## Measurement of School Bus Pedal Dimensions

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| 16. Abstract <br> The National Transportation Safety Board (NTSB) investigated four crashes of school buses and one of a fire truck, all of which occurred from 2005 to 2009 and concluded that these accidents were consistent with pedal misapplication. Among the NTSB recommendations was that NHTSA analyze pedal configurations in heavy vehicles to determine the effect of pedal design on the driver's task. This research was performed at NHTSA's Vehicle Research and Test Center (VRTC), in East Liberty, Ohio, to provide an overview of the range of typical pedal dimensions in school buses. However, analysis to determine the effect of pedal design on the driver's task was beyond the scope of this study. NHTSA identified 21 dimensions based on the SAE J1100 standard and also developed a procedure capable of determining pedal position. Two additional dimensions were used for the analysis of the transit style buses to account for the steering column position. <br> The dimensions for 24 Type C (conventional style) buses and 8 Type D (transit style) buses were measured and compared. Only the stepover distance, the seat cushion width, and the steering wheel width and height were not significantly different between the two types. The Type C buses measured were assembled by three different manufacturers, Bluebird Corporation, Fort Valley, GA; IC Corporation, Warrenville, IL (a subsidiary of Navistar); and Thomas Built Corporation, High Point, NC (a subsidiary of Daimler Trucks, N.A.). The Bluebird and Thomas Built buses were the most similar, but they had statistically significant differences in the brake pedal width and the stepover distance from the face planes of the pedals, as well as some differences in seating position. The IC buses were statistically different in 11 and 12 of 21 measurements from the Bluebird and Thomas Built buses, respectively. <br> The dimensions for six Type D buses manufactured by Bluebird and two by Thomas were measured. The dimensions were statistically different in only 8 of the 23 dimension measured. Most of the differences were smaller distances from the pedals to the "tunnel" on the right side of the pedals for the Bluebird buses. <br> The measurements for the 32 buses were compared to the dimensions of 101 passenger vehicles. Seventeen of the 21 dimensions were statistically different. Even though the means were different, the distributions of values had considerable overlap. The variables that had little overlap were that the bus accelerator and brake pedals had a shorter overall travel to the floor, and the steering wheel was farther from the floor and pedals for buses than for the passenger vehicles. The dimensions of both the Type C and Type D buses were compared to the average dimensions of the passenger cars. The measurements of Type D buses differed from passenger cars in nearly every dimension. Only the distance from the accelerator to the tunnel and the seat cushion width were not significantly different, and for 14 of the dimensions there was no overlap between the outliers of the 2 distributions. The Type C buses were more similar to passenger car dimensions, differing in 10 of the 21 dimensions measured, with only the height and size of the steering wheel having no overlap between the distributions. |  |  |  |
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## 1. Executive Summary

The National Transportation Safety Board (NTSB) investigated four crashes of school buses and one of a fire truck, all of which occurred from 2005 to 2009 and concluded that these accidents were consistent with pedal misapplication. ${ }^{1}$ One NTSB recommendation was that NHTSA analyze pedal configurations in heavy vehicles to determine the effect of pedal design on the driver's task. This research was performed at NHTSA's Vehicle Research and Test Center (VRTC), in East Liberty, Ohio, to provide an overview of the range of typical pedal dimensions in school buses. However, analysis to determine the effect of pedal design on the driver's task was beyond the scope of this study.

Recently, NHTSA completed a study to analyze possible relationships in a limited number of cases between pedal design factors and the rate of pedal misapplication in passenger vehicles, specifically occurring when drivers intend to apply the brake but instead apply the accelerator. ${ }^{2}$ In that study, NHTSA identified 21 dimensions based on the SAE J1100 standard and also developed a procedure capable of determining precise pedal positions. Two additional dimensions were added to the current study to accommodate the Type D buses for a total of 23 different dimensions. These dimensions include pedal placement dimensions as well as dimensions such as the distance from the steering wheel to the floor plane that help define the driver's orientation to the pedals.

The dimensions for 24 Type C (conventional style) buses and 8 Type D (transit style) buses were measured. All the horizontal pedal dimensions were significantly different between the two types of buses. For the other pedal dimensions, only the perpendicular stepover distance was not significantly different. The driver position dimensions of seat cushion width and steering wheel width and height were not different.

[^0]The Type C buses measured were assembled by three different manufacturers, Bluebird Corporation, Fort Valley, GA; IC Corporation, Warrenville, IL (a subsidiary of Navistar); and Thomas Built Corporation, High Point, NC (a subsidiary of Daimler Trucks, N.A.). The Bluebird and Thomas Built buses were the most similar, but they had statistically significant differences in the brake pedal width and stepover in plane, (that is the perpendicular distance between the planes of the brake and accelerator pedal faces) as well as some differences in seating position. The IC buses were statistically different in 11 and 12 of 21 measurements from the Bluebird and Thomas Built buses, respectively.

The dimensions for six Type D buses manufactured by Bluebird and two by Thomas were measured. The dimensions were statistically different in only 8 of the 23 dimensions measured. Most of the differences were smaller distances from the pedals to the "tunnel" on the right side of the pedals for the Bluebird buses.

The measurements for the 32 buses were compared to the dimensions of 101 passenger vehicles previously reported by NHTSA. Seventeen of the 21 dimensions were statistically different on average. From inspection of the distributions, even though the means were different, the distributions of values had considerable overlap for most values. The variables that had little overlap were that the bus accelerator and brake pedals had a shorter overall travel to the floor and the steering wheel was farther from the floor and pedals for buses than for the passenger vehicles.

The dimensions of both the Type C and Type D buses were compared to the average dimensions of the passenger cars. The measurements of Type D buses differed from passenger cars in nearly every dimension. Only the distance from the accelerator to the tunnel (A) and seat cushion width (L) were not significantly different, and for 14 of the dimensions there was no overlap between the outliers of the 2 distributions. The Type C buses were more similar to passenger car dimensions, differing in 10 of the 21 dimensions measured, with only the height and size of the steering wheel having no overlap between the distributions.

## 2. Background

After the initial investigation of a school bus crash in May 2005 suggested that the cause may have been pedal misapplication, the National Transportation Safety Board carried out a special investigation into pedal misapplication in heavy vehicles. The NTSB investigated four crashes of school buses and one of a fire truck, all of which occurred from 2005 to 2009. The NTSB also reviewed work done by NHTSA in the 1980s after receiving claims of sudden unintended acceleration for certain passenger vehicles. ${ }^{3}$ The NTSB investigators found no mechanical failures of the braking system in the vehicles, no contributing medical conditions of the drivers, and no outside interference with the driver. The absence of these factors, along with other evidence, led the NTSB to conclude that these accidents were consistent with pedal misapplication. The NTSB recommended that national and State associations of pupil transportation include the risk of pedal misapplication in literature and training sessions.

The NTSB also made several specific recommendations to NHTSA:

- NHTSA should require the installation of brake transmission shift interlocks (BTSI) in heavy vehicles. ${ }^{4}$ Based on the documented success of brake transmission shift interlocks in preventing sudden unintended acceleration of light passenger vehicles during initial movement, (3) the NTSB concluded that the installation of BTSI on heavy vehicles would have prevented three of the five incidents they investigated.
- NHTSA should develop and implement industrial standards for onboard recording of bus crash data. ${ }^{5}$
- NHTSA should analze pedal configurations in heavy vehicles, including innovative designs, to determine the effect of pedal design on the driver's task. ${ }^{6}$
- Ultimately, NHTSA should publish pedal design guidelines for designers and manufacturers. ${ }^{7}$

[^1]This report is not intended to fully respond to the NTSB recommendation that NHTSA analyze pedal configurations in heavy vehicles, including innovative designs, to determine the effect of pedal design on the driver's task. Rather, the data compiled in this report analyzes pedal configurations in certain heavy vehicles.

Recently, NHTSA completed a study to analyze possible relationships between pedal design factors and the rate of pedal misapplication in passenger vehicles, specifically occurring when drivers intend to apply the brake but instead apply the accelerator, which can result in unintended acceleration (UA) of a vehicle. ${ }^{2,8}$ An example of a design factor is "lateral separation," the horizontal gap between the brake and accelerator pedals. Another example is "stepover," the distance between the surface plane of the brake pedal and the surface plane of the accelerator pedal. Previous research efforts into UA events hypothesized that pedal design factors may contribute to driver pedal error. The previous study used data from a North Carolina State Crash Database, ${ }^{9}$ selected because it offered detailed police accident report records with sufficiently specific vehicle make and model information for 2,411 UA events. This database was also recently used to study demographic information. ${ }^{10}$ The records covered a 5 -year period from 2004 to 2008.

A UA event is defined as any unintended powered acceleration of a motor vehicle. That is, acceleration powered by the engine and not intentionally commanded by the operator via the vehicle's controls. UA events included, but were not limited to, stuck throttle, engine surging, high idle speed, and sudden acceleration incidents (SAI).

An SAI is defined in the report "An Examination of Sudden Acceleration" ${ }^{11}$ as any "unintended, unexpected, high-power accelerations from a stationary position or very low initial speed accompanied by an apparent loss of braking effectiveness." The report was the result of a study conducted in the late 1980's to identify and evaluate factors that contribute to the occurrence of SAI. It also identified vehicle design factors such as pedal placement and pedal feedback as important variables in events that involve the unintentional misapplication of vehicle control pedals.

[^2]Currently, there is no globally accepted standard to regulate pedal placement. The human factors science needed to better determine optimal locations of pedals has historically been limited and difficult to obtain. As a result, significant variation can be found in the locations of pedal controls among vehicle manufacturers. Overall variability has been asserted to be a contributing design factor in cases of UA events. In a memorandum report for NHTSA's Office of Defects Investigation (ODI) of activities in response to a request from the Minnesota State Patrol, the vehicle defects investigator noted that a "lack of consistency between the pedal cluster positions in the vehicle primarily operated by the driver and the subject vehicle may have contributed to the subject crash." ${ }^{12}$ It has been theorized that the variation in pedal placement may be a factor in the higher observed rate of pedal misapplication by drivers who were unfamiliar with the vehicle.

Another relevant design factor is stepover height, defined as the difference in height between the plane of the brake pedal face and the plane of the accelerator pedal face. Vehicles with little stepover height may cause the driver to inadvertently depress both pedals at the same time or to more likely confuse the pedal location. In 1983, Audi recalled 117,000 Model 5000 passenger cars (Recall $83 \mathrm{~V}-095^{13}$ ) due to insufficient stepover height and installed a brake pedal plate to increase the height of the pedal face.

There are two main types of pedal designs among the measured school buses: one is pedals that are mounted to the vertical firewall under the instrument panel, and the other is pedals that are mounted to and hinged at the floor.

The research program described in this report was performed at NHTSA's Vehicle Research and Test Center to provide an overview of the range of typical pedal dimensions in school buses.

[^3]
## 3. Three Dimensional (3D) Laser Scanning

The driver's seat was positioned in the full rearward position. If the vehicle was equipped with a tilt steering column, it was set to the position closest to the center of the arc of travel.

A hand-held 3D laser scanner was used to record the locations of the control pedals, driver's seat, and steering wheel. The scanner operated while tethered to a computer, and the data gathered was stored in a standard stereo lithography (*.stl) file format. A typical session of data being recorded is shown in Figure 1. The operator scanned the vehicle surfaces until the computer rendering showed that all required surfaces had been adequately covered. The accelerator pedal was scanned in three positions. The first was the static position, the second was the fully depressed wide open throttle position, and the third was a point of travel at the approximate center of the first two positions.


Figure 1 - Typical Scanning Session

## 4. Control Location Measurements

Twenty-one variables were identified, shown in Table 1, for which dimensional measurements were collected for analysis. Eighteen of these were identified in SAE J1100. ${ }^{14}$ Three other measurements were defined and appear in the table as variables M, Arc, Chord, Left and Wall. In addition to the measurements of pedal position in the vehicle, several variables were identified that were important for the orientation of the driver to the position of the pedals.

Table 1 - List of Dimensions Analyzed

| Letter Identifier | SAE Variable | Description |
| :---: | :---: | :---: |
| A | PW-17 | Accelerator to tunnel |
| B | PW-21 | Lateral spacing right edge of brake to left edge accelerator (arc) |
| C | PW-27 | Right edge of brake to tunnel - horizontal |
| D | PW-42 | Left edge of brake to vertical panel on left |
| E | PW-82 | Brake centerline to accelerator centerline |
| F | PW-92 | Driver centerline to right edge of brake |
| G | PW-98 | Driver centerline to accelerator horizontal centerline |
| H | PL-52 | Stepover - brake to accelerator - shortest arc distance |
| I | PH-26 | Bottom edge of undepressed brake pedal to floor |
| J | PH-16 | Bottom edge of undepressed accelerator pedal to floor |
| L | SW-16 | Seat cushion width |
| M | (not identified) | Steering centerline to brake pedal center |
| N | PL-1 | Distance between the planes of brake and accelerator pedal faces |
| 0 | PW-47 | Overall width of floorpan @ 150 mm above floor |
| P | H-17 | Height of steering wheel from floor |
| Q | W-9 | Width of steering wheel |
| R | L-6 | Ball of foot accelerator pedal to front center of steering wheel |
| S | PW-22 | Brake pedal width |
| T | PW-11 | Accelerator pedal width |
| Are | (not identified) | Arc length of accelerator pedal |
| Chord | (not identified) | Chord length of accelerator pedal |
| Left* | (not identified) | Distance from left edge of brake pedal to steering column |
| Wall* | (not identified) | Distance from left edge of brake pedal to wall on left |
| * Dimensions added for Type D buses |  |  |

[^4]The data acquired by the 3D laser scan of the vehicle's driver controls was analyzed in a computer aided design (CAD) software program. The program allowed the 3D rendering of the vehicle to be rotated to the optimal viewing angle and measurements taken. A table of all measurement results can be found in Appendix A. Five views displaying the measurement results for each vehicle were identified, and examples are shown in Figure 2 to Figure 6. Images for each vehicle can be found in Appendix G.


Figure 2 - Dimensions A, B, C, D


Figure 3 - Dimensions E, F, G


Figure 4 - Dimensions H, J, N, P, R, Pedal Arcs


Figure 5 - Dimensions L, Q


Figure 6 - Dimensions M, O, S, T

## 5. Pedal Dimensions Analysis

## Dimensions by Bus Type

The dimensions for 24 Type C (conventional style) buses and 8 Type D (transit style) buses were measured. The average dimensions are shown in Table 2. All the horizontal pedal dimensions were significantly different between the two types of buses. For the other pedal dimensions, only the stepover distance was not significantly different. The driver position dimensions of seat cushion width and steering wheel width and height were not different. A $t$ test comparison of the measurements and the distributions are shown in Appendix B.

Table 2 - Average Dimensions of Bus Types C (Conventional Style) and Type D (Transit Style)

|  | Type C Buses |  |  | Type D Buses |  |  | Significantly <br> Dimension |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Number <br> of <br> Vehicles | Average <br> Dimension, <br> $\mathbf{m m}$ | Standard <br> Deviation, <br> $\mathbf{m m}$ | Number <br> of <br> Vehicles | Average <br> Dimension, <br> $\mathbf{m m}$ | Standard <br> Deviation, <br> $\mathbf{m m}$ | Different, $\boldsymbol{(} \boldsymbol{t}$ <br> test $\mathbf{0}$ <br> $\mathbf{0}=\mathbf{0 . 0 5})$ |
| A | 24 | 58.1 | 22.2 | 8 | 41.2 | 12.5 | Yes |
| B | 24 | 89.4 | 18.2 | 8 | 30.4 | 11 | Yes |
| C | 24 | 197 | 22.6 | 8 | 139.4 | 11.5 | Yes |
| D | 24 | 234.9 | 51.2 | 8 | 396.3 | 32.4 | Yes |
| E | 24 | 157.3 | 16.6 | 8 | 108.6 | 5.7 | Yes |
| F | 24 | 63.2 | 34.8 | 8 | 185.5 | 25 | Yes |
| G | 24 | 170.5 | 33.6 | 8 | 256 | 21.1 | Yes |
| H | 24 | 30.5 | 22.5 | 8 | 18.7 | 16.8 | No |
| I | 24 | 106.4 | 17.7 | 8 | 22.8 | 3 | Yes |
| J | 24 | 76.3 | 15.6 | 8 | 25.7 | 7.8 | Yes |
| L | 24 | 502.5 | 18.9 | 8 | 501.7 | 29.2 | No |
| M | 24 | 19 | 18.5 | 8 | 135.4 | 36.1 | Yes |
| N | 24 | 35.4 | 23.8 | 8 | 26.3 | 19.9 | No |
| O | 24 | 515.7 | 54 | 8 | 625.2 | 32.6 | Yes |
| P | 24 | 808 | 41.2 | 8 | 795.5 | 21.5 | No |
| Q | 24 | 453.6 | 8 | 8 | 468.3 | 20.3 | No |
| R | 24 | 386.7 | 42.3 | 8 | 275.5 | 40.8 | Yes |
| S | 24 | 99.8 | 3.8 | 8 | 71.3 | 1.2 | Yes |
| T | 24 | 53.3 | 3.4 | 8 | 67.1 | 5.5 | Yes |
| ARC | 24 | 253.6 | 89.8 | 8 | 203.4 | 105.5 | No |
| CHORD | 24 | 65.4 | 16 | 8 | 80.5 | 18 | No |
| WALL | 0 | $\cdot$ | $\cdot$ | 8 | 39.9 | 18.6 | NA |
| LEFT | 0 | $\cdot$ | $\cdot$ | 8 | 249.4 | 32 | NA |

## Type C Buses by Manufacturer

The Type C buses measured were assembled by three different manufacturers, Bluebird , IC, and Thomas Built. The average dimensions are shown in Table 3. The Bluebird and Thomas Built buses were the most similar, but they had statistically significant differences in the brake pedal width and stepover in plane, as well as some differences in seating position. The IC buses were statistically different in 11 and 12 of 21 measurements from the Bluebird and Thomas Built buses, respectively. All comparisons are shown in Appendix C.

Table 3 - Average Dimensions of Type C Buses by Manufacturer

| Variable | Manufacturer |  |  |  |  |  |  |  |  | Statistical Differences* |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | BlueBird |  |  | IC |  |  | Thomas |  |  | $\begin{aligned} & \text { BB } \\ & \text { vs. } \\ & \text { IC } \end{aligned}$ | $\begin{gathered} \text { BB } \\ \text { vs. } \\ \text { Th. } \end{gathered}$ | $\begin{aligned} & \text { IC } \\ & \text { vs. } \\ & \text { Th. } \end{aligned}$ |
|  | N | Mean, mm | Std. <br> Dev., <br> mm | N | Mean, mm | Std. Dev., mm | N | Mean, mm | Std. Dev., mm |  |  |  |
| A | 13 | 64.3 | 27.5 | 9 | 45.9 | 2.4 | 2 | 71.9 | 1.7 |  |  |  |
| B | 13 | 77.8 | 9.2 | 9 | 110.3 | 5.3 | 2 | 71.2 | 2.7 | $\checkmark$ |  | $\checkmark$ |
| C | 13 | 189.1 | 27.5 | 9 | 210.1 | 5 | 2 | 188.9 | 3.8 |  |  |  |
| D | 13 | 265.5 | 35.1 | 9 | 179.9 | 12.9 | 2 | 282.8 | 13.7 | $\checkmark$ |  | $\checkmark$ |
| E | 13 | 146.9 | 7.4 | 9 | 176.8 | 2.4 | 2 | 137.2 | 0.9 | $\checkmark$ |  | $\checkmark$ |
| F | 13 | 56 | 31.1 | 9 | 55 | 10.7 | 2 | 147.1 | 0.5 |  | $\checkmark$ | $\checkmark$ |
| G | 13 | 151.8 | 29.4 | 9 | 182.7 | 9.6 | 2 | 237.2 | 2.5 | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| H | 13 | 16.9 | 14.1 | 9 | 55.5 | 1.5 | 2 | 6.5 | 3.5 | $\checkmark$ |  | $\checkmark$ |
| I | 13 | 99.1 | 17.3 | 9 | 121.3 | 4.6 | 2 | 86.9 | 0.4 | $\checkmark$ |  | $\checkmark$ |
| J | 13 | 76.9 | 14.1 | 9 | 83.4 | 3.7 | 2 | 40.2 | 1.2 |  | $\checkmark$ | $\checkmark$ |
| L | 13 | 491.3 | 18.2 | 9 | 516.1 | 8.9 | 2 | 514.8 | 1.8 | $\checkmark$ |  |  |
| M | 13 | 20.9 | 11.4 | 9 | 5.7 | 4 | 2 | 66.1 | 11.9 | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| N | 13 | 19.9 | 17.1 | 9 | 60.9 | 3.8 | 2 | 21.4 | 2.4 | $\sqrt{ }$ | $\sqrt{ }$ | $\sqrt{ }$ |
| 0 | 13 | 540.4 | 56.3 | 9 | 472.2 | 13.4 | 2 | 551.3 | 15.4 | $\checkmark$ |  |  |
| P | 13 | 801.2 | 51.8 | 9 | 823.8 | 17.7 | 2 | 781.7 | 0.8 |  |  |  |
| Q | 13 | 454.9 | 2.3 | 9 | 447 | 3.5 | 2 | 474.8 | 0.6 | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| R | 13 | 399.6 | 52.7 | 9 | 371 | 17 | 2 | 374.2 | 28.8 |  |  |  |
| S | 13 | 101.5 | 3.3 | 9 | 99.3 | 0.9 | 2 | 91 | 1.7 |  | $\checkmark$ | $\checkmark$ |
| T | 13 | 52.6 | 3.1 | 9 | 53.2 | 1.4 | 2 | 58.4 | 9 |  |  |  |
| ARC | 13 | 263.6 | 114.2 | 9 | 231.3 | 51.1 | 2 | 289.3 | 10 |  |  |  |
| CHORD | 13 | 62.3 | 18.2 | 9 | 74 | 1.3 | 2 | 47.3 | 21.1 |  |  |  |
| * Statistically significant differences at $\alpha=0.05$ using Scheffe's test were indicated by a check $(\sqrt{ })$ |  |  |  |  |  |  |  |  |  |  |  |  |

## Type D Buses by Manufacturer

The dimensions for six Type D buses manufactured by Bluebird and two by Thomas were measured. The average dimensions are shown in Table 4. The dimensions were statistically different in only 8 of the 23 dimension measured. Most of the differences were smaller distances from the pedals to the "tunnel" on the right side of the pedals for the Bluebird buses. All comparisons are shown in Appendix D.

Table 4 - Average Dimensions of Type D Buses by Manufacturer

| Dimension | Bluebird |  |  | Thomas |  |  | Significantly Different, ( $t$ test $\alpha=0.05$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { Number } \\ \text { of } \\ \text { Vehicles } \end{gathered}$ | Average Dimension, mm | Standard Deviation, mm | $\begin{aligned} & \text { Number } \\ & \text { of } \\ & \text { Vehicles } \end{aligned}$ | Average Dimension, mm | Standard Deviation, mm |  |
| A | 6 | 37.0 | 11.7 | 2 | 53.6 | 0.4 | Yes |
| B | 6 | 25.9 | 8.4 | 2 | 43.9 | 2.6 | Yes |
| C | 6 | 133.5 | 4.8 | 2 | 156.9 | 0.2 | Yes |
| D | 6 | 410.9 | 19.5 | 2 | 352.6 | 19.4 | Yes |
| E | 6 | 108.1 | 2.3 | 2 | 110.4 | 13.9 | No |
| F | 6 | 184.6 | 25.4 | 2 | 188.4 | 33.6 | No |
| G | 6 | 254.4 | 23.4 | 2 | 260.8 | 17.5 | No |
| H | 6 | 13.3 | 13.0 | 2 | 34.8 | 21.1 | No |
| I | 6 | 22.5 | 3.0 | 2 | 23.9 | 4.0 | No |
| J | 6 | 25.0 | 7.8 | 2 | 28.0 | 10.3 | No |
| L | 6 | 499.7 | 33.3 | 2 | 507.7 | 18.2 | No |
| M | 6 | 130.4 | 41.2 | 2 | 150.6 | 7.2 | No |
| N | 6 | 18.8 | 13.5 | 2 | 48.5 | 23.3 | No |
| 0 | 6 | 633.6 | 33.8 | 2 | 600.1 | 5.9 | No |
| P | 6 | 792.4 | 24.4 | 2 | 804.8 | 7.0 | No |
| Q | 6 | 457.4 | 1.6 | 2 | 501.2 | 0.6 | Yes |
| R | 6 | 291.1 | 32.5 | 2 | 228.7 | 22.8 | Yes |
| S | 6 | 71.5 | 1.3 | 2 | 70.9 | 0.5 | No |
| T | 6 | 69.5 | 3.8 | 2 | 60.1 | 1.1 | Yes |
| ARC | 6 | 173.4 | 86.7 | 2 | 293.5 | 136.8 | No |
| CHORD | 6 | 74.7 | 16.8 | 2 | 98.1 | 5.7 | No |
| WALL | 6 | 34.1 | 18.0 | 2 | 57.4 | 0.4 | Yes |
| LEFT | 6 | 266.3 | 9.9 | 2 | 198 | 11.2 | No |

## Buses Versus Passenger Vehicles

The measurements for the 32 buses were compared to the dimensions of 101 passenger vehicles previously reported by NHTSA. ${ }^{2}$ The averages are shown in Table 5 and all comparisons are shown in Appendix E. Seventeen of the 21 dimensions were statistically different on average. The $T$ test comparisons of the values and distributions are shown in Appendix E. From inspection of the distributions, even though the means were different, the distributions of values had considerable overlap for most values. The variables that had little overlap were that the bus accelerator and brake pedals had a shorter overall travel to the floor, and the steering wheel was farther from the floor and pedals for buses than for passenger vehicles.

Table 5 - Average Dimensions of Buses and Passenger Vehicles

| Dimension | Buses |  |  | Passenger Vehicles |  |  | Significantly Different, ( $t$ test $\alpha=0.05$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Number of Vehicles | Average Dimension, mm | Standard <br> Deviation, mm | Number of Vehicles | Average Dimension, mm | Standard <br> Deviation, mm |  |
| A | 32 | 53.8 | 21.4 | 101 | 41.5 | 15.8 | Yes |
| B | 32 | 74.7 | 30.8 | 101 | 75.4 | 10.7 | No |
| C | 32 | 182.6 | 32.4 | 101 | 167.1 | 14.8 | Yes |
| D | 32 | 275.2 | 85.0 | 101 | 236.1 | 25.9 | Yes |
| E | 32 | 145.1 | 25.9 | 101 | 154.1 | 11.8 | No |
| F | 32 | 93.8 | 62.7 | 101 | 61.9 | 26.9 | Yes |
| G | 32 | 191.9 | 48.5 | 101 | 152.7 | 33.5 | Yes |
| H | 32 | 27.6 | 21.6 | 101 | 50.2 | 11.5 | Yes |
| I | 32 | 85.5 | 39.8 | 101 | 154.5 | 13.9 | Yes |
| J | 32 | 63.7 | 26.2 | 101 | 113.4 | 13.2 | Yes |
| L | 32 | 502.3 | 21.4 | 101 | 527.8 | 41.1 | Yes |
| M | 32 | 48.1 | 56.3 | 101 | 25.6 | 20.7 | Yes |
| N | 32 | 33.1 | 22.9 | 101 | 51.5 | 12.9 | Yes |
| O | 32 | 543.1 | 68.8 | 101 | 526.6 | 41.9 | No |
| P | 32 | 804.9 | 37.3 | 101 | 628.2 | 28.5 | Yes |
| Q | 32 | 457.2 | 13.5 | 101 | 381.6 | 8.0 | Yes |
| R | 32 | 358.9 | 64.0 | 101 | 561.8 | 33.8 | Yes |
| S | 32 | 92.7 | 13.0 | 101 | 120.7 | 16.2 | Yes |
| T | 32 | 56.8 | 7.2 | 101 | 46.5 | 8.6 | Yes |
| ARC | 32 | 241.1 | 94.8 | 101 | 205.1 | 83.9 | No |
| CHORD | 32 | 69.2 | 17.5 | 101 | 62.4 | 12.3 | Yes |

## Buses Versus Passenger Vehicles by Type

The dimensions of both the Type C and Type D buses were compared to the average dimensions of the passenger cars previously measured by NHTSA. The average values and comparisons are shown in Table 6 and the comparisons are shown in Appendix F. The measurements of Type D buses differed from passenger cars in nearly every dimension. Only the distance from the accelerator to the tunnel (A) and seat cushion width (L) were not significantly different, and for 14 of the dimensions there was no overlap between the outliers of the 2 distributions. The Type C buses were more similar to passenger car dimensions, differing in 10 of the 21 dimensions measured, with only the height and size of the steering wheel having no overlap between the distributions.

Table 6 - Comparison of Dimensions for Passenger Cars and Type C and D Buses

| Variable | Vehicle Category |  |  |  |  |  |  |  |  | Statistical Differences* |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Type C Bus |  |  | Type D Bus |  |  | Passenger Car |  |  | $\begin{gathered} \text { C } \\ \text { vs. } \\ \text { D } \end{gathered}$ | $\begin{gathered} \text { C } \\ \text { vs. } \\ \text { Car } \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { vs. } \\ \text { Car } \end{gathered}$ |
|  | N | Mean, mm | Std. Dev., mm | N | Mean, mm | Std. Dev., mm | N | Mean, mm | Std. Dev., mm |  |  |  |
| A | 24 | 58.1 | 22.2 | 8 | 41.2 | 12.5 | 101 | 41.5 | 15.8 |  | $\checkmark$ |  |
| B | 24 | 89.4 | 18.2 | 8 | 30.4 | 11.0 | 101 | 75.4 | 10.7 | $\sqrt{ }$ | $\checkmark$ | $\checkmark$ |
| C | 24 | 197.0 | 22.6 | 8 | 139.4 | 11.5 | 101 | 167.1 | 14.8 | $\sqrt{ }$ |  | $\checkmark$ |
| D | 24 | 234.9 | 51.2 | 8 | 396.3 | 32.4 | 101 | 236.1 | 25.9 | $\checkmark$ |  | $\checkmark$ |
| E | 24 | 157.3 | 16.6 | 8 | 108.6 | 5.7 | 101 | 154.1 | 11.8 | $\sqrt{ }$ |  | $\checkmark$ |
| F | 24 | 63.2 | 34.8 | 8 | 185.5 | 25.0 | 101 | 61.9 | 26.9 | $\sqrt{ }$ |  | $\sqrt{ }$ |
| G | 24 | 170.5 | 33.6 | 8 | 256.0 | 21.1 | 101 | 152.7 | 33.5 | $\checkmark$ |  | $\checkmark$ |
| H | 24 | 30.5 | 22.5 | 8 | 18.7 | 16.8 | 101 | 50.2 | 11.5 |  | $\checkmark$ | $\checkmark$ |
| I | 24 | 106.4 | 17.7 | 8 | 22.8 | 3.0 | 101 | 154.5 | 13.9 | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| J | 24 | 76.3 | 15.6 | 8 | 25.7 | 7.8 | 101 | 113.4 | 13.2 | $\sqrt{ }$ | $\checkmark$ | $\sqrt{ }$ |
| L | 24 | 502.5 | 18.9 | 8 | 501.7 | 29.2 | 101 | 527.8 | 41.1 |  | $\checkmark$ |  |
| M | 24 | 19.0 | 18.5 | 8 | 135.4 | 36.1 | 101 | 25.6 | 20.7 | $\checkmark$ |  | $\checkmark$ |
| N | 24 | 35.4 | 23.8 | 8 | 26.3 | 19.9 | 101 | 51.5 | 12.9 |  | $\checkmark$ | $\checkmark$ |
| 0 | 24 | 515.7 | 54.0 | 8 | 625.2 | 32.6 | 101 | 526.6 | 41.9 | $\checkmark$ |  | $\checkmark$ |
| P | 24 | 808.0 | 41.2 | 8 | 795.5 | 21.5 | 101 | 628.2 | 28.5 |  | $\checkmark$ | $\checkmark$ |
| Q | 24 | 453.6 | 8.0 | 8 | 468.3 | 20.3 | 101 | 381.6 | 8.0 | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| R | 24 | 386.7 | 42.3 | 8 | 275.5 | 40.8 | 101 | 561.8 | 33.8 | $\sqrt{ }$ | $\checkmark$ | $\checkmark$ |
| S | 24 | 99.8 | 3.8 | 8 | 71.3 | 1.2 | 101 | 120.7 | 16.2 | $\sqrt{ }$ | $\checkmark$ | $\checkmark$ |
| T | 24 | 53.3 | 3.4 | 8 | 67.1 | 5.5 | 101 | 46.5 | 8.6 | $\sqrt{ }$ | $\checkmark$ | $\checkmark$ |
| ARC | 24 | 253.6 | 89.8 | 8 | 203.4 | 105.5 | 101 | 205.1 | 83.9 |  |  |  |
| CHORD | 24 | 65.4 | 16.0 | 8 | 80.5 | 18.0 | 101 | 62.4 | 12.3 | $\sqrt{ }$ |  | $\checkmark$ |
| * Statistically significant differences at $\alpha=0.05$ using Scheffe's test were indicated by a check ( $\sqrt{ }$ ) |  |  |  |  |  |  |  |  |  |  |  |  |

## Summary

All of the horizontal pedal dimensions were significantly different between Type C and Type D buses. Only the stepover distance, seat cushion width, steering wheel width, and height were not different for Type C and Type D buses.

For Type C buses, the Bluebird and Thomas Built buses were the most similar, but they had statistically significant differences in the brake pedal width and stepover distance between the face planes of the pedals, as well as some differences in seating position. The IC buses were statistically different in 11 and 12 of 21 measurements from the Bluebird and Thomas Built buses, respectively.

The dimensions for Type D buses manufactured by Bluebird and by Thomas were statistically different in only 8 of the 23 dimension measured. Most of the differences were smaller distances from the pedals to the "tunnel" on the right side of the pedals for the Bluebird buses.

The measurements for the 32 buses were compared to the dimensions of 101 passenger vehicles. Seventeen of the 21 dimensions were statistically different on average. Even though the means were different, most of the distributions of values had considerable overlap. The variables that had little overlap were that the bus accelerator and brake pedals had a shorter overall travel to the floor, and the steering wheel was farther from the floor and pedals for buses than for the passenger vehicles.

The dimensions of both the Type C and Type D buses were compared to the average dimensions of the passenger cars. The measurements of Type D buses differed from passenger cars in nearly every dimension. Only the distances from the accelerator to the tunnel and seat cushion width were not significantly different, and for 14 of the dimensions there was no overlap between the outliers of the 2 distributions. The Type C buses were more similar to passenger car dimensions, differing in 10 of the 21 dimensions measured, with only the height and size of the steering wheel having no overlap between the distributions.
6. Appendix A - Bus Measurements

| Type | A | B | C | D | E | F | G | H | I | J | L | M | N | 0 | P | Q | R | S | T | ARC | CHORD | ALL LEFT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 70.7 | 73.1 | 186.2 | 292.5 | 137.8 | 147.4 | 238.9 | 4 | 86.6 | 39.3 | 513.5 | 74.5 | 23.1 | 562.2 | 781.1 | 475.2 | 353.8 | 92.2 | 52 | 296.3 | 32.4 |  |
| C | 73.1 | 69.3 | 191.6 | 273.1 | 136.5 | 146.7 | 235.4 | 8.9 | 87.1 | 41 | 516 | 57.7 | 19.7 | 540.4 | 472.3 | 474.3 | 394.5 | 89.8 | 64.7 | 282.2 | 62.3 |  |
| C | 31 | 80.3 | 160.8 | 265.1 | 147.2 | 54 | 153.6 | 16.2 | 116.1 | 76.8 | 486.4 | 24.7 | 11.8 | 513 | 804.1 | 454.5 | 352.5 | 98.6 | 51.6 | 223.8 | 37.2 |  |
| C | 53.7 | 77.6 | 173.3 | 243.3 | 149.9 | 34.5 | 134.3 | 13 | 117 | 77.9 | 485.1 | 30 | 11.1 | 501 | 775.3 | 453.5 | 392.5 | 99.6 | 52.2 | 253.5 | 81.4 |  |
| C | 35 | 84 | 163.9 | 232.1 | 153.4 | 42 | 144.6 | 15.7 | 107.3 | 50.6 | 473.8 | 21.3 | 22.3 | 481.4 | 4668.6 | 454.7 | 485.7 | 99.4 | 51 | 260.2 | 33 |  |
| C | 99.8 | 74.3 | 217.9 | 260.5 | 144.5 | 67.7 | 159 | 8.3 | 73.8 | 90.3 | 471.9 | 4.5 | 19.6 | 564.9 | 9818.6 | 458 | 423.8 | 105.8 | 84.4 | 289.9 | 56.9 | . . |
| C | 87.5 | 82.9 | 219.3 | 254.9 | 145.4 | 83.7 | 175.1 | 3.5 | 73.6 | 94 | 471.5 | 2.4 | 11.4 | 559.2 | 258 | 457.5 | 473.2 | 106.8 | 53.8 | 302.9 | 43.9 | . . |
| C | 83.6 | 80.3 | 214.7 | 253.1 | 145.8 | 43.4 | 137.5 | 7.8 | 83.2 | 87.1 | 481.4 | 2.6 | 4.7 | 560.8 | 850.5 | 457.2 | 461.8 | 105.2 | 25.6 | 281.2 | 65.5 | . |
| C | 101.7 | 80.3 | 230 | 340.1 | 145.2 | 135.7 | 228.5 | 19.6 | 77.4 | 68 | 527.7 | 37.6 | 24.3 | 652.3 | 332.2 | 457.4 | 410.4 | 104.7 | 49.3 | 208.7 | 74.6 | . |
| C | 104.9 | 74.1 | 228 | 339.6 | 143.3 | 92.2 | 179.8 | 31.5 | 86.9 | 70.8 | 527.1 | 17 | 34.2 | 651.7 | 730.7 | 451.2 | 385.8 | 103.8 | 80.6 | 185.6 | 72.7 | . . |
| C | 37.8 | 92.4 | 171.6 | 236.7 | 162.6 | 36.1 | 148.3 | 0.3 | 110.8 | 89.8 | 484.2 | 29 | 0.5 | 495.6 | 6826.9 | 457.2 | 305.3 | 99 | 51.5 | 259.1 | 56.8 | . . |
| C | 36.9 | 86.5 | 171. | 236.9 | 156.4 | 37 | 143.2 | 7 | 110.7 | 90.6 | 491.2 | 31.5 | 2.5 | 495.8 | 8830.7 | 453.9 | 347.4 | 99.4 | 60.2 | 254.4 | 56.9 | . . |
| C | 48.4 | 78 | 170.8 | 271.9 | 143.6 | 30.4 | 125.6 | 10.4 | 119.3 | 84.3 | 498.9 | 21.2 | 11.6 | 527.4 | 4809.8 | 453.8 | 360.6 | 99.7 | 52.2 | 248 | 61.3 | . |
| C | 54.9 | 57.5 | 170.2 | 263.7 | 138.1 | 33.2 | 121.5 | 45.1 | 106.8 | 58.1 | 491 | 25.9 | 54.5 | 517.1 | 1820.2 | 452.6 | 386.4 | 97.1 | 53.3 | 588.3 | 99.3 | . |
| C | 60.9 | 63.5 | 166.3 | 254 | 134.6 | 38.5 | 122.2 | 41.2 | 104.9 | 61.5 | 496.7 | 24.4 | 49.9 | 504.8 | 789.8 | 451.8 | 409.3 | 100.2 | 57.1 | 70.6 | 70 | . . |
| C | 46.9 | 100.3 | 203.7 | 192.9 | 172.9 | 66.5 | 189 | 57.1 | 120.5 | 85.1 | 518.8 | 9.5 | 56.9 | 478.6 | 825.1 | 444.7 | 370.1 | 99.5 | 54 | 247.7 | 75 | . . |
| C | 45.6 | 119.5 | 214.1 | 165.7 | 180.9 | 48.9 | 182.2 | 53.1 | 125 | 82.9 | 525.3 | 7.2 | 64.3 | 460.5 | 5814.6 | 450 | 382 | 98.1 | 51.4 | 191 | 72.5 | . . |


| Type | A | B | C | D | E | F | G | H | I | J | L | M | N | 0 | P | Q |  |  |  |  | HORD | WALL | EFT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C | 47.9 | 114.4 | 213.6 | 178 | 179.6 | 38.6 | 168.3 | 55 | 121.5 | 80.5 | 5519.6 | 61.5 | 62.3 | 473.4 | 4817.4 | 450.4 | 4380.9 | 100 | 54.9 | 214.5 | 71.9 |  |  |
| C | 47.8 | 109.1 | 208.2 | 189.1 | 174.2 | 55.5 | 182.3 | 57.5 | 122.5 | 83.2 | 2516 | 10.6 | 62.2 | 481.7 | 7850.6 | 449.5 | 5342.7 | 100.1 | 151.5 | 160.9 | 73 |  |  |
| C | 46.4 | 108. | 209.9 | 186.6 | 176.9 | 64.5 | 191.1 | 54.7 | 109.9 | 75.7 | 7498.9 | 99.8 | 54.9 | 479.1 | 1796.1 | 442.9 | 386.4 | 99.8 | 52.5 | 218.7 | 74.1 |  |  |
| C | 45.8 | 110 | 208.5 | 185 | 177.2 | 41.1 | 168.2 | 55.6 | 124.4 | 88.8 | 8519.9 | $9 \quad 0.4$ | 57.9 | 473.1 | 1813.9 | 444 | 389.8 | 99.5 | 53.2 | 207.2 | 74.7 |  |  |
| C | 43.6 | 110 | 206.9 | 189.2 | 176.8 | 56.8 | 184.3 | 53.9 | 124.9 | 84.6 | 6503.3 | 31.4 | 60.4 | 480 | 851.6 | 441.7 | 7344.7 | 97.7 | 53.2 | 337.6 | 76.1 |  | . |
| C | 48.5 | 107.4 | 219.9 | 179.8 | 176.3 | 68.5 | 197 | 55.7 | 122.4 | 84.4 | 4519.9 | 96.7 | 67.2 | 482.2 | 2825.3 | 449.6 | 6369.5 | 100.1 | 155.5 | 231.6 | 74.2 |  | . |
| C | 40.8 | 113. | 205.8 | 153 | 176.4 | 54.5 | 181.8 | 57.1 | 120.6 | 85.7 | 7522.9 | 94 | 61 | . 4 | 4819.7 | 449.8 | 8372.5 | 99 | 53 | 272.7 | 74.2 |  | . |
| D | 37.9 | 20.2 | 128.2 | 434. | 10 | 195.1 | 263.2 | 10.7 | 23.3 | 16.4 | 4459.5 | 5201.2 | 4.3 | 673.1 | 1824.7 | 458.4 | 4260.8 | 69.5 | 73.1 | 243.3 | 72.9 | 58.5 | 263.6 |
| D | 49.7 | 17.5 | 134.6 | 394.5 | 107.1 | 178.9 | 249.8 | 2.6 | 24.9 | 24.2 | 2513.5 | 5105.6 | 17.2 | 608.8 | 8795 | 457.9 | 307.4 | 71.6 | 66.6 | 6240.5 | 63.3 | 21.5 | 258.4 |
| D | 50 | 21.8 | 141 | 396.1 | 110.3 | 193.6 | 263 | 7.4 | 23.6 | 25.4 | 4475.7 | 7108.4 | 16.4 | 615.5 | 5813.6 | 456.2 | 250.9 | 73.1 | 68.5 | 5239.9 | 64.7 | 26.1 | 258.5 |
| D | 19.3 | 41.1 | 128.4 | 437.3 | 110.3 | 224. | 291 | 38.8 | 20.1 | 20 | 477.5 | 5160 | 44.4 | 681.1 | 1758.9 | 458.9 | 9277.9 | 70.5 | 63.8 | 54.1 | 108 | 55.9 | 283.8 |
| D | 33.1 | 27.6 | 134.2 | 403.2 | 106.9 | 155.5 | 228.3 | 7.5 | 17.6 | 39.2 | 2531.3 | 399 | 13 | 611.5 | 5774.4 | 458 | 328.4 | 71.5 | 72.8 | 76.4 | 67.6 | 22.8 | 271.8 |
| D | 32.2 | 27.2 | 134.8 | 400 | 109.3 | 160.3 | 231.2 | 13 | 25.3 | 24.7 | 7540.4 | 4108.1 | 17.5 | 611.8 | 8787.9 | 454.8 | 321.3 | 72.7 | 72.2 | 2186.3 | 71.4 | 19.9 | 261.7 |
| D | 53.3 | 42 | 157 | 366.3 | 100.6 | 212.1 | 273.2 | 19.9 | 26.7 | 35.3 | 3494.8 | 8155.7 | 32 | 604.2 | 2799.8 | 500.7 | 7212.5 | 71.2 | 60.8 | 390.2 | 94 | 57.1 | 206.5 |
| D | 53.8 | 45.7 | 156.7 | 338.9 | 120.2 | 164.6 | 248 | 49.7 | 21.1 | 20.7 | 7520.5 | 5145.5 | 65 | 595.9 | 9809.7 | 501.6 | 6244.8 | 70.5 | 59.3 | 3196.8 | 102.1 | 57.6 | 190.6 |

## 7. Appendix B - T Test Comparisons of Dimensions by Bus Type

Variable: A

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 58.0500 | 22.2351 | 4.5387 | 31.0000 | 104.9 |
| Type D | 8 | 41.1625 | 12.4898 | 4.4158 | 19.3000 | 53.8000 |
| Diff (1-2) | 16.8875 | 20.3823 | 8.3210 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | 2.03 | 0.0514 |
| Satterthwaite | Unequal | 22.097 | 2.67 | 0.0141 |



Variable: B

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 89.4458 | 18.1528 | 3.7054 | 57.5000 | 119.5 |
| Type D | 8 | 30.3875 | 10.9911 | 3.8859 | 17.5000 | 45.7000 |
| Diff (1-2) | 59.0583 | 16.7578 | 6.8413 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 30 | 8.63 | $<.0001$ |
| Satterthwaite | Unequal | 20.387 | 11.00 | $<.0001$ |



Variable: C

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 197.0 | 22.6314 | 4.6196 | 160.8 | 230.0 |
| Type D | 8 | 139.4 | 11.5219 | 4.0736 | 128.2 | 157.0 |
| Diff (1-2) | 57.5917 | 20.5827 | 8.4028 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | 6.85 | $<.0001$ |
| Satterthwaite | Unequal | 24.333 | 9.35 | $<.0001$ |



Variable: D

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 234.9 | 51.2014 | 10.4515 | 153.0 | 340.1 |
| Type D | 8 | 396.3 | 32.4460 | 11.4714 | 338.9 | 437.3 |
| Diff (1-2) | -161.4 | 47.4924 | 19.3887 |  |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 30 | -8.33 | $<.0001$ |
| Satterthwaite | Unequal | 19.38 | -10.40 | $<.0001$ |



Variable: E

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 157.3 | 16.5962 | 3.3877 | 134.6 | 180.9 |
| Type D | 8 | 108.6 | 5.7021 | 2.0160 | 100.6 | 120.2 |
| Diff (1-2) | 48.6750 | 14.7903 | 6.0381 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 30 | 8.06 | $<.0001$ |
| Satterthwaite | Unequal | 29.867 | 12.35 | $<.0001$ |



Variable: F

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 63.2250 | 34.8106 | 7.1057 | 30.4000 | 147.4 |
| Type D | 8 | 185.5 | 24.9877 | 8.8345 | 155.5 | 224.1 |
| Diff (1-2) |  | -122.3 | 32.7829 | 13.3836 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 30 | -9.14 | $<.0001$ |
| Satterthwaite | Unequal | 16.841 | -10.79 | $<.0001$ |



Variable: G

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 170.5 | 33.5647 | 6.8514 | 121.5 | 238.9 |
| Type D | 8 | 256.0 | 21.0686 | 7.4489 | 228.3 | 291.1 |
| Diff (1-2) | -85.5375 | 31.1014 | 12.6971 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 30 | -6.74 | $<.0001$ |
| Satterthwaite | Unequal | 19.587 | -8.45 | $<.0001$ |



Variable: H

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 30.5083 | 22.4624 | 4.5851 | 0.3000 | 57.5000 |
| Type D | 8 | 18.7000 | 16.7983 | 5.9391 | 2.6000 | 49.7000 |
| Diff (1-2) | 11.8083 | 21.2761 | 8.6859 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | 1.36 | 0.1841 |
| Satterthwaite | Unequal | 16.091 | 1.57 | 0.1350 |



Variable: I

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 106.4 | 17.7478 | 3.6228 | 73.6000 | 125.0 |
| Type D | 8 | 22.8250 | 3.0231 | 1.0688 | 17.6000 | 26.7000 |
| Diff (1-2) | 83.5583 | 15.6084 | 6.3721 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | 13.11 | $<.0001$ |
| Satterthwaite | Unequal | 26.518 | 22.12 | $<.0001$ |



Variable: J

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 76.2917 | 15.5622 | 3.1766 | 39.3000 | 94.0000 |
| Type D | 8 | 25.7375 | 7.7618 | 2.7442 | 16.4000 | 39.2000 |
| Diff (1-2) | 50.5542 | 14.1326 | 5.7696 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 30 | 8.76 | $<.0001$ |
| Satterthwaite | Unequal | 24.784 | 12.04 | $<.0001$ |



Variable: L

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 502.5 | 18.8916 | 3.8562 | 471.5 | 527.7 |
| Type D | 8 | 501.7 | 29.1709 | 10.3135 | 459.5 | 540.4 |
| Diff (1-2) | 0.8917 | 21.7295 | 8.8710 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | 0.10 | 0.9206 |
| Satterthwaite | Unequal | 9.0403 | 0.08 | 0.9372 |



Variable: M

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 18.9750 | 18.5358 | 3.7836 | 0.4000 | 74.5000 |
| Type D | 8 | 135.4 | 36.1271 | 12.7729 | 99.0000 | 201.2 |
| Diff (1-2) | -116.5 | 23.8316 | 9.7292 |  |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | -11.97 | $<.0001$ |
| Satterthwaite | Unequal | 8.263 | -8.74 | $<.0001$ |



Variable: N

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 35.3750 | 23.7791 | 4.8539 | 0.5000 | 67.2000 |
| Type D | 8 | 26.2500 | 19.8985 | 7.0352 | 4.3000 | 65.0000 |
| Diff (1-2) | 9.1250 | 22.9324 | 9.3621 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | 0.97 | 0.3375 |
| Satterthwaite | Unequal | 14.267 | 1.07 | 0.3034 |



Variable: O

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 515.7 | 54.0421 | 11.0313 | 441.4 | 652.3 |
| Type D | 8 | 625.2 | 32.6212 | 11.5333 | 595.9 | 681.1 |
| Diff (1-2) | -109.5 | 49.8737 | 20.3609 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 30 | -5.38 | $<.0001$ |
| Satterthwaite | Unequal | 20.456 | -6.86 | $<.0001$ |



Variable: P

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 808.0 | 41.1724 | 8.4043 | 668.6 | 858.0 |
| Type D | 8 | 795.5 | 21.5246 | 7.6101 | 758.9 | 824.7 |
| Diff (1-2) | 12.5458 | 37.5198 | 15.3174 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | 0.82 | 0.4192 |
| Satterthwaite | Unequal | 23.74 | 1.11 | 0.2796 |



Variable: Q

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Type C | 24 | 453.6 | 8.0218 | 1.6374 | 441.7 | 475.2 |
| Type D | 8 | 468.3 | 20.3116 | 7.1812 | 454.8 | 501.6 |
| Diff (1-2) |  | -14.7542 | 12.0664 | 4.9261 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | -3.00 | 0.0055 |
| Satterthwaite | Unequal | 7.7404 | -2.00 | 0.0813 |



Variable: R

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 386.7 | 42.2774 | 8.6298 | 305.3 | 485.7 |
| Type D | 8 | 275.5 | 40.7994 | 14.4248 | 212.5 | 328.4 |
| Diff (1-2) | 111.2 | 41.9372 | 17.1208 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | 6.50 | $<.0001$ |
| Satterthwaite | Unequal | 12.423 | 6.62 | $<.0001$ |



Variable: S

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 99.7958 | 3.7888 | 0.7734 | 89.8000 | 106.8 |
| Type D | 8 | 71.3250 | 1.1865 | 0.4195 | 69.5000 | 73.1000 |
| Diff (1-2) | 28.4708 | 3.3666 | 1.3744 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 30 | 20.71 | $<.0001$ |
| Satterthwaite | Unequal | 29.994 | 32.36 | $<.0001$ |



Variable: T

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 53.3208 | 3.4330 | 0.7007 | 48.4000 | 64.7000 |
| Type D | 8 | 67.1375 | 5.4526 | 1.9278 | 59.3000 | 73.1000 |
| Diff (1-2) | -13.8167 | 3.9966 | 1.6316 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | -8.47 | $<.0001$ |
| Satterthwaite | Unequal | 8.9246 | -6.74 | $<.0001$ |



Variable: ARC

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 253.6 | 89.8428 | 18.3391 | 70.6000 | 588.3 |
| Type D | 8 | 203.4 | 105.5 | 37.3091 | 54.1000 | 390.2 |
| Diff (1-2) | 50.1708 | 93.7372 | 38.2681 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | 1.31 | 0.1998 |
| Satterthwaite | Unequal | 10.603 | 1.21 | 0.2537 |



Variable: CHORD

| style | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Type C | 24 | 65.4125 | 15.9885 | 3.2636 | 32.4000 | 99.3000 |
| Type D | 8 | 80.5000 | 17.9584 | 6.3492 | 63.3000 | 108.0 |
| Diff (1-2) | -15.0875 | 16.4693 | 6.7235 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 30 | -2.24 | 0.0324 |
| Satterthwaite | Unequal | 10.955 | -2.11 | 0.0583 |


8. Appendix C-Comparison of Type C Bus Measurements by Manufacturer
Dependent Variable: A

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 2217.70752 | 1108.85376 | 2.54 | 0.1025 |
| Error | 21 | 9153.47248 | 435.87964 |  |  |
| Corrected Total | 23 | 11371.18000 |  |  |  |

R-Square Coeff Var Root MSE A Mean
$\begin{array}{llll}0.195029 & 35.96508 & 20.87773 & 58.05000\end{array}$


Scheffe's Test for A

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 435.8796 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |
| :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 95 Lim | fidence |
| Thomas - BB | 7.585 | -34.172 | 49.341 |
| Thomas - IC | 25.978 | -16.998 | 68.953 |
| BB - Thomas | -7.585 | -49.341 | 34.172 |
| BB - IC | 18.393 | -5.445 | 42.232 |
| IC - Thomas | -25.978 | -68.953 | 16.998 |
| IC - BB | -18.393 | -42.232 | 5.445 |

Dependent Variable: B

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 6331.867618 | 3165.933809 | $53.31<.0001$ |  |
| Error | 21 | 1247.191966 | 59.390094 |  |  |
| Corrected Total | 23 | 7579.059583 |  |  |  |


| R-Square | Coeff Var | Root MSE | B Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.835442 | 8.615825 | 7.706497 | 89.44583 |

Distribution of B


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 59.39009 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 9 Lim | nfidence |  |
| IC - BB | 32.466 | 23.666 | 41.265 | *** |
| IC - Thomas | 39.089 | 23.225 | 54.952 | *** |
| BB-IC | -32.466 | -41.265 | -23.666 | *** |
| BB - Thomas | 6.623 | -8.790 | 22.036 |  |
| Thomas - IC | -39.089 | -54.952 | -23.225 | *** |
| Thomas - BB | -6.623 | -22.036 | 8.790 |  |

Dependent Variable: C

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 2475.98266 | 1237.99133 | 2.79 | 0.0840 |
| Error | 21 | 9304.13692 | 443.05414 |  |  |
| Corrected Total | 23 | 11780.11958 |  |  |  |

R-Square Coeff Var Root MSE C Mean
$\begin{array}{lllll}0.210183 & 10.68718 & 21.04885 & 196.9542\end{array}$


## Scheffe's Test for C

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 443.0541 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$ <br> $\mathbf{m f g}$ <br> Comparison | Difference <br> Between <br> Means | Simultaneous 95\% Confidence <br> Limits |  |
| :---: | :---: | :---: | ---: |
| IC - BB | 20.951 | -3.083 | 44.985 |
| IC - Thomas | 21.167 | -22.161 | 64.495 |
| BB - IC | -20.951 | -44.985 | 3.083 |
| BB - Thomas | 0.215 | -41.883 | 42.314 |
| Thomas - IC | -21.167 | -64.495 | 22.161 |
| Thomas - BB | -0.215 | -42.314 | 41.883 |

Dependent Variable: D

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 43988.97009 | 21994.48504 | 28.32 | $<.0001$ |
| Error | 21 | 16307.56325 | 776.55063 |  |  |
| Corrected Total | 23 | 60296.53333 |  |  |  |

R-Square Coeff Var Root MSE D Mean
$\begin{array}{llll}0.729544 & 11.86488 & 27.86666 & 234.8667\end{array}$


## Scheffe's Test for D

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 776.5506 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | ---: | ---: | ---: | :--- |
| mfg <br> Comparison | Difference <br> Between <br> Means | Simultaneous 95\% Confidence <br> Limits |  |  |
| Thomas - BB | 17.27 | -38.47 | 73.00 |  |
| Thomas - IC | 102.88 | 45.52 | 160.24 | $* * *$ |
| BB - Thomas | -17.27 | -73.00 | 38.47 |  |
| BB - IC | 85.61 | 53.79 | 117.43 | $* * *$ |
| IC - Thomas | -102.88 | -160.24 | -45.52 | $* * *$ |
| IC - BB | -85.61 | -117.43 | -53.79 | $* * *$ |
|  |  |  |  |  |

Dependent Variable: E

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 5634.138173 | 2817.069087 | $84.41<.0001$ |  |
| Error | 21 | 700.808077 | 33.371813 |  |  |
| Corrected Total | 23 | 6334.946250 |  |  |  |

R-Square Coeff Var Root MSE E Mean
$\begin{array}{llll}0.889374 & 3.672203 & 5.776834 & 157.3125\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 33.37181 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 9 Lim | nfidence |  |
| IC - BB | 29.877 | 23.281 | 36.473 | *** |
| IC - Thomas | 39.650 | 27.759 | 51.541 | *** |
| BB-IC | -29.877 | -36.473 | -23.281 | * |
| BB - Thomas | 9.773 | -1.781 | 21.327 |  |
| Thomas - IC | -39.650 | -51.541 | -27.759 | *** |
| Thomas - BB | -9.773 | -21.327 | 1.781 |  |

Dependent Variable: F

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 15336.60342 | 7668.30171 | 12.85 | 0.0002 |  |
| Error | 21 | 12534.28158 | 596.87055 |  |  |  |
|  | Corrected Total | 23 | 27870.88500 |  |  |  |


| R-Square | Coeff Var | Root MSE | F Mean |
| ---: | ---: | ---: | ---: |
| 0.550273 | 38.64126 | 24.43093 | 63.22500 |



Scheffe's Test for F

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 596.8706 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 95 Lim | nfidence |  |
| Thomas-BB | 91.019 | 42.156 | 139.882 | *** |
| Thomas - IC | 92.061 | 41.771 | 142.351 | ** |
| BB - Thomas | -91.019 | -139.882 | -42.156 | *** |
| BB-IC | 1.042 | -26.854 | 28.938 |  |
| IC - Thomas | -92.061 | -142.351 | -41.771 | *** |
| IC - BB | -1.042 | -28.938 | 26.854 |  |

Dependent Variable: G

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 14775.01544 | 7387.50772 | 13.93 | 0.0001 |
| Error | 21 | 11136.59081 | 530.31385 |  |  |
| Corrected Total | 23 | 25911.60625 |  |  |  |


| R-Square | Coeff Var | Root MSE | G Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.570208 | 13.50747 | 23.02854 | 170.4875 |



Scheffe's Test for G

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 530.3138 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg | Difference | Simultaneous 95 | nfidence |  |
| Comparison | Between <br> Means | Lim |  |  |
| Thomas - IC | 54.461 | 7.058 | 101.864 | ** |
| Thomas - BB | 85.365 | 39.307 | 131.423 | *** |
| IC - Thomas | -54.461 | -101.864 | -7.058 | *** |
| IC - BB | 30.904 | 4.610 | 57.199 | *** |
| BB - Thomas | -85.365 | -131.423 | -39.307 | ** |
| BB-IC | -30.904 | -57.199 | -4.610 | *** |

Dependent Variable: H

\[\)|  Source  |  DF  |  Sum of Squares  |  Mean Square  |  F Value  |  Pr $>\text { F }$ |
| :--- | ---: | ---: | ---: | ---: | ---: |
|  Model  | 2 | 9199.00855 | 4599.50427 | 40.15 | $<.0001$ |
|  Error  | 21 | 2405.84979 | 114.56428 |  |  |
|  Corrected Total  | 23 | 11604.85833 |  |  |  |

\]

| R-Square | Coeff Var | Root MSE | H Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.792686 | 35.08376 | 10.70347 | 30.50833 |



Scheffe's Test for H

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 114.5643 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 9 Lin | nfidence |  |
| IC - BB | 38.630 | 26.408 | 50.851 | *** |
| IC - Thomas | 49.072 | 27.040 | 71.105 | *** |
| BB - IC | -38.630 | -50.851 | -26.408 | *** |
| BB - Thomas | 10.442 | -10.965 | 31.850 |  |
| Thomas - IC | -49.072 | -71.105 | -27.040 | *** |
| Thomas - BB | -10.442 | -31.850 | 10.965 |  |

Dependent Variable: I

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 3462.577564 | 1731.288782 | 9.61 | 0.0011 |
| Error | 21 | 3782.095769 | 180.099799 |  |  |
| Corrected Total | 23 | 7244.673333 |  |  |  |

$$
\begin{array}{rrrr}
\text { R-Square } & \text { Coeff Var } & \text { Root MSE } & \text { I Mean } \\
0.477948 & 12.61488 & 13.42013 & 106.3833
\end{array}
$$



Scheffe's Test for I

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 180.0998 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg | Difference | Simultaneous 95 | fidence |  |
| Comparison | Between Means | Lim |  |  |
| IC - BB | 22.238 | 6.915 | 37.562 | * |
| IC - Thomas | 34.450 | 6.825 | 62.075 | * |
| BB-IC | -22.238 | -37.562 | -6.915 | ** |
| BB - Thomas | 12.212 | -14.629 | 39.052 |  |
| Thomas - IC | -34.450 | -62.075 | -6.825 | *** |
| Thomas - BB | -12.212 | -39.052 | 14.629 |  |

Dependent Variable: J

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 3076.404103 | 1538.202051 | 12.95 | 0.0002 |
| Error | 21 | 2493.794231 | 118.752106 |  |  |
| Corrected Total | 23 | 5570.198333 |  |  |  |

R-Square Coeff Var Root MSE J Mean<br>$\begin{array}{llll}0.552297 & 14.28379 & 10.89734 & 76.29167\end{array}$



## Scheffe's Test for J

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 118.7521 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 9 Lim | fidence |  |
| IC - BB | 6.526 | -5.917 | 18.968 |  |
| IC - Thomas | 43.283 | 20.852 | 65.715 | *** |
| BB - IC | -6.526 | -18.968 | 5.917 |  |
| BB - Thomas | 36.758 | 14.963 | 58.553 | *** |
| Thomas - IC | -43.283 | -65.715 | -20.852 | *** |
| Thomas - BB | -36.758 | -58.553 | -14.963 | *** |

Dependent Variable: L

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 3587.293333 | 1793.646667 | 8.15 | 0.0024 |
| Error | 21 | 4621.245000 | 220.059286 |  |  |
| Corrected Total | 23 | 8208.538333 |  |  |  |

R-Square Coeff Var Root MSE L Mean
$\begin{array}{llll}0.437020 & 2.951874 & 14.83440 & 502.5417\end{array}$


Scheffe's Test for L

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 220.0593 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 95 Lim | fidence |  |
| IC - Thomas | 1.317 | -29.219 | 31.852 |  |
| IC - BB | 24.767 | 7.828 | 41.705 | *** |
| Thomas - IC | -1.317 | -31.852 | 29.219 |  |
| Thomas - BB | 23.450 | -6.219 | 53.119 |  |
| BB-IC | -24.767 | -41.705 | -7.828 | *** |
| BB - Thomas | -23.450 | -53.119 | 6.219 |  |

Dependent Variable: M

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 6082.601752 | 3041.300876 | 35.10 | $<.0001$ |
| Error | 21 | 1819.643248 | 86.649678 |  |  |
| Corrected Total | 23 | 7902.245000 |  |  |  |

R-Square Coeff Var Root MSE M Mean
$\begin{array}{llll}0.769731 & 49.05708 & 9.308581 & 18.97500\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 86.64968 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 9 Lim | nfidence |  |
| Thomas - BB | 45.169 | 26.552 | 63.787 | *** |
| Thomas - IC | 60.422 | 41.261 | 79.583 | *** |
| BB - Thomas | -45.169 | -63.787 | -26.552 | *** |
| BB - IC | 15.253 | 4.624 | 25.882 | * |
| IC - Thomas | -60.422 | -79.583 | -41.261 | *** |
| IC - BB | -15.253 | -25.882 | -4.624 | *** |

Dependent Variable: N

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 9361.50192 | 4680.75096 | 26.98 | $<.0001$ |
| Error | 21 | 3643.76308 | 173.51253 |  |  |
| Corrected Total | 23 | 13005.26500 |  |  |  |

R-Square Coeff Var Root MSE N Mean
$\begin{array}{llll}0.719824 & 37.23651 & 13.17242 & 35.37500\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 173.5125 |
| Critical Value of F | 3.46680 |



Dependent Variable: O

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 27468.84085 | 13734.42043 | 7.26 | 0.0040 |
| Error | 21 | 39703.77248 | 1890.65583 |  |  |
| Corrected Total | 23 | 67172.61333 |  |  |  |

R-Square Coeff Var Root MSE O Mean
$\begin{array}{llll}0.408929 & 8.431038 & 43.48167 & 515.7333\end{array}$



Dependent Variable: P

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 4237.09377 | 2118.54689 | 1.28 | 0.2988 |
| Error | 21 | 34751.82581 | 1654.84885 |  |  |
| Corrected Total | 23 | 38988.91958 |  |  |  |

R-Square Coeff Var Root MSE P Mean
$\begin{array}{lllll}0.108674 & 5.034347 & 40.67983 & 808.0458\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 1654.849 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |
| :---: | :---: | :---: | ---: |
| mfg <br> Comparison | Difference <br> Between <br> Means | Simultaneous 95\% Confidence <br> Limits |  |
| IC - BB | 22.63 | -23.82 | 69.08 |
| IC - Thomas | 42.11 | -41.63 | 125.85 |
| BB - IC | -22.63 | -69.08 | 23.82 |
| BB - Thomas | 19.48 | -61.88 | 100.85 |
| Thomas - IC | -42.11 | -125.85 | 41.63 |
| Thomas - BB | -19.48 | -100.85 | 61.88 |

Dependent Variable: Q

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 1312.883419 | 656.441709 | 82.48 | $<.0001$ |
| Error | 21 | 167.134915 | 7.958805 |  |  |
| Corrected Total | 23 | 1480.018333 |  |  |  |

R-Square Coeff Var Root MSE Q Mean<br>$\begin{array}{lllll}0.887072 & 0.622001 & 2.821135 & 453.5583\end{array}$



| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 7.958805 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the 0.05 level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 9 Lim | nfidence |  |
| Thomas - BB | 19.881 | 14.238 | 25.523 | *** |
| Thomas - IC | 27.794 | 21.987 | 33.602 | * |
| BB - Thomas | -19.881 | -25.523 | -14.238 | * |
| BB-IC | 7.914 | 4.692 | 11.135 | * |
| IC - Thomas | -27.794 | -33.602 | -21.987 | * |
| IC - BB | -7.914 | -11.135 | -4.692 | *** |

Dependent Variable: R

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 4706.71688 | 2353.35844 | 1.36 | 0.2789 |
| Error | 21 | 36402.93645 | 1733.47316 |  |  |
| Corrected Total | 23 | 41109.65333 |  |  |  |

$$
\begin{array}{rrrrr}
\text { R-Square } & \text { Coeff Var } & \text { Root MSE } & \text { R Mean } \\
0.114492 & 10.76582 & 41.63500 & 386.7333
\end{array}
$$



| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 1733.473 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |
| :---: | :---: | :---: | ---: |
| mfg <br> Comparison | Difference <br> Between <br> Means | Simultaneous 95\% Confidence <br> Limits |  |
| BB - Thomas | 25.44 | -57.83 | 108.71 |
| BB - IC | 28.64 | -18.90 | 76.18 |
| Thomas - BB | -25.44 | -108.71 | 57.83 |
| Thomas - IC | 3.19 | -82.51 | 88.90 |
| IC - BB | -28.64 | -76.18 | 18.90 |
| IC - Thomas | -3.19 | -88.90 | 82.51 |

Dependent Variable: S

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 193.9237714 | 96.9618857 | $14.95<.0001$ |  |
| Error | 21 | 136.2458120 | 6.4878958 |  |  |
| Corrected Total | 23 | 330.1695833 |  |  |  |

R-Square Coeff Var Root MSE S Mean
$\begin{array}{llll}0.587346 & 2.552346 & 2.547135 & 99.79583\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 6.487896 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| mfg <br> Comparison | Difference Between Means | Simultaneous 9 Lim | nfidence |  |
| BB-IC | 2.1735 | -0.7349 | 5.0819 |  |
| BB - Thomas | 10.4846 | 5.3902 | 15.5790 | * |
| IC - BB | -2.1735 | -5.0819 | 0.7349 |  |
| IC - Thomas | 8.3111 | 3.0680 | 13.5543 | *** |
| Thomas - BB | -10.4846 | -15.5790 | -5.3902 | *** |
| Thomas - IC | -8.3111 | -13.5543 | -3.0680 | *** |

Dependent Variable: T

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 57.3923611 | 28.6961806 | 2.82 | 0.0822 |
| Error | 21 | 213.6672222 | 10.1746296 |  |  |
| Corrected Total | 23 | 271.0595833 |  |  |  |

R-Square Coeff Var Root MSE T Mean
$\begin{array}{lllll}0.211733 & 5.982220 & 3.189770 & 53.32083\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 10.17463 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the 0.05 level were indicated by ***. |  |  |  |
| :---: | :---: | :---: | :---: |
| mfg Comparison | Difference Between Means | Simultaneous 95 Lim | fidence |
| Thomas - IC | 5.106 | -1.460 | 11.672 |
| Thomas - BB | 5.750 | -0.630 | 12.130 |
| IC - Thomas | -5.106 | -11.672 | 1.460 |
| IC - BB | 0.644 | -2.998 | 4.287 |
| BB - Thomas | -5.750 | -12.130 | 0.630 |
| BB - IC | -0.644 | -4.287 | 2.998 |

Dependent Variable: ARC

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 8296.5655 | 4148.2827 | 0.49 | 0.6188 |
| Error | 21 | 177353.0329 | 8445.3825 |  |  |
| Corrected Total | 23 | 185649.5983 |  |  |  |

R-Square Coeff Var Root MSE ARC Mean
$\begin{array}{llll}0.044689 & 36.23649 & 91.89876 & 253.6083\end{array}$


Scheffe's Test for ARC

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 8445.383 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$ <br> $\mathbf{m f g}$ <br> Comparison | Difference <br> Between <br> Means | Simultaneous 95\% Confidence <br> Limits |  |
| :---: | ---: | :---: | ---: |
| Thomas - BB | 25.70 | -158.10 | 209.50 |
| Thomas - IC | 57.93 | -131.24 | 247.10 |
| BB - Thomas | -25.70 | -209.50 | 158.10 |
| BB - IC | 32.23 | -72.70 | 137.16 |
| IC - Thomas | -57.93 | -247.10 | 131.24 |
| IC - BB | -32.23 | -137.16 | 72.70 |

Dependent Variable: CHORD

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Model | 2 | 1439.513558 | 719.756779 | 3.40 | 0.0524 |
| Error | 21 | 4440.052692 | 211.431081 |  |  |
| Corrected Total | 23 | 5879.566250 |  |  |  |

R-Square Coeff Var Root MSE CHORD Mean

| 0.244833 | 22.22919 | 14.54067 | 65.41250 |
| :--- | :--- | :--- | :--- |



| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 21 |
| Error Mean Square | 211.4311 |
| Critical Value of F | 3.46680 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$ |  |  |  |
| :---: | :---: | :---: | ---: |
| mfg <br> Comparison | Difference <br> Between <br> Means | Simultaneous 95\% Confidence <br> Limits |  |
| IC - BB | 11.697 | -4.905 | 28.300 |
| IC - Thomas | 26.617 | -3.315 | 56.548 |
| BB - IC | -11.697 | -28.300 | 4.905 |
| BB - Thomas | 14.919 | -14.163 | 44.001 |
| Thomas - IC | -26.617 | -56.548 | 3.315 |
| Thomas - BB | -14.919 | -44.001 | 14.163 |

9. Appendix D-T Test Comparison of Type D Buses by Manufacturer

Variable: A

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 37.0333 | 11.6845 | 4.7702 | 19.3000 | 50.0000 |
| Thomas | 2 | 53.5500 | 0.3536 | 0.2500 | 53.3000 | 53.8000 |
| Diff (1-2) | -16.5167 | 10.6674 | 8.7099 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -1.90 | 0.1067 |
| Satterthwaite | Unequal | 5.0273 | -3.46 | 0.0179 |



Variable: B

| $\boldsymbol{m f g}$ | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 25.9000 | 8.4318 | 3.4423 | 17.5000 | 41.1000 |
| Thomas | 2 | 43.8500 | 2.6163 | 1.8500 | 42.0000 | 45.7000 |
| Diff (1-2) | -17.9500 | 7.7709 | 6.3449 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 6 | -2.83 | 0.0300 |
| Satterthwaite | Unequal | 5.8608 | -4.59 | 0.0039 |



Variable: C

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 133.5 | 4.7693 | 1.9471 | 128.2 | 141.0 |
| Thomas | 2 | 156.9 | 0.2121 | 0.1500 | 156.7 | 157.0 |
| Diff (1-2) | -23.3167 | 4.3547 | 3.5556 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -6.56 | 0.0006 |
| Satterthwaite | Unequal | 5.0586 | -11.94 | $<.0001$ |



Variable: D

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 410.9 | 19.5002 | 7.9609 | 394.5 | 437.3 |
| Thomas | 2 | 352.6 | 19.3747 | 13.7000 | 338.9 | 366.3 |
| Diff (1-2) | 58.2667 | 19.4794 | 15.9048 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | 3.66 | 0.0105 |
| Satterthwaite | Unequal | 1.7495 | 3.68 | 0.0813 |



Variable: E

|  | mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 108.1 | 2.3339 | 0.9528 | 104.4 | 110.3 |  |
| Thomas | 2 | 110.4 | 13.8593 | 9.8000 | 100.6 | 120.2 |  |
| Diff (1-2) | -2.3500 | 6.0459 | 4.9364 |  |  |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -0.48 | 0.6509 |
| Satterthwaite | Unequal | 1.019 | -0.24 | 0.8503 |



Variable: F

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 184.6 | 25.3822 | 10.3623 | 155.5 | 224.1 |
| Thomas | 2 | 188.4 | 33.5876 | 23.7500 | 164.6 | 212.1 |
| Diff (1-2) | -3.7667 | 26.9240 | 21.9834 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -0.17 | 0.8696 |
| Satterthwaite | Unequal | 1.4068 | -0.15 | 0.9025 |



Variable: G

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 254.4 | 23.4047 | 9.5549 | 228.3 | 291.1 |
| Thomas | 2 | 260.8 | 17.5362 | 12.4000 | 248.4 | 273.2 |
| Diff (1-2) | -6.3667 | 22.5330 | 18.3981 |  |  |  |


| Method | Variances | DF | $\boldsymbol{t}$ Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 6 | -0.35 | 0.7411 |
| Satterthwaite | Unequal | 2.3728 | -0.41 | 0.7180 |



Variable: H

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 13.3333 | 12.9617 | 5.2916 | 2.6000 | 38.8000 |
| Thomas | 2 | 34.8000 | 21.0718 | 14.9000 | 19.9000 | 49.7000 |
| Diff (1-2) | -21.4667 | 14.6290 | 11.9446 |  |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -1.80 | 0.1224 |
| Satterthwaite | Unequal | 1.2641 | -1.36 | 0.3674 |



Variable: I

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 22.4667 | 3.0071 | 1.2276 | 17.6000 | 25.3000 |
| Thomas | 2 | 23.9000 | 3.9598 | 2.8000 | 21.1000 | 26.7000 |
| Diff (1-2) |  | -1.4333 | 3.1857 | 2.6011 |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -0.55 | 0.6015 |
| Satterthwaite | Unequal | 1.411 | -0.47 | 0.7014 |



Variable: J

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 24.9833 | 7.7652 | 3.1701 | 16.4000 | 39.2000 |
| Thomas | 2 | 28.0000 | 10.3238 | 7.3000 | 20.7000 | 35.3000 |
| Diff (1-2) | -3.0167 | 8.2469 | 6.7336 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 6 | -0.45 | 0.6699 |
| Satterthwaite | Unequal | 1.4028 | -0.38 | 0.7541 |



Variable: L

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 499.7 | 33.2576 | 13.5774 | 459.5 | 540.4 |
| Thomas | 2 | 507.7 | 18.1726 | 12.8500 | 494.8 | 520.5 |
| Diff (1-2) | -8.0000 | 31.2533 | 25.5182 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -0.31 | 0.7645 |
| Satterthwaite | Unequal | 3.5854 | -0.43 | 0.6931 |



Variable: M

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 130.4 | 41.1609 | 16.8039 | 99.0000 | 201.2 |
| Thomas | 2 | 150.6 | 7.2125 | 5.1000 | 145.5 | 155.7 |
| Diff (1-2) | -20.2167 | 37.6898 | 30.7736 |  |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -0.66 | 0.5356 |
| Satterthwaite | Unequal | 5.7209 | -1.15 | 0.2955 |



Variable: N

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 18.8333 | 13.4683 | 5.4984 | 4.3000 | 44.4000 |
| Thomas | 2 | 48.5000 | 23.3345 | 16.5000 | 32.0000 | 65.0000 |
| Diff (1-2) | -29.6667 | 15.5535 | 12.6994 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -2.34 | 0.0582 |
| Satterthwaite | Unequal | 1.2314 | -1.71 | 0.3010 |



Variable: O

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 633.6 | 33.8313 | 13.8116 | 608.8 | 681.1 |
| Thomas | 2 | 600.1 | 5.8690 | 4.1500 | 595.9 | 604.2 |
| Diff (1-2) | 33.5833 | 30.9764 | 25.2922 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | 1.33 | 0.2325 |
| Satterthwaite | Unequal | 5.7108 | 2.33 | 0.0609 |



Variable: P

| mfg | N | Mean |  |  |  | Std Dev |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Std Err | Minimum | Maximum |  |  |  |  |
| BlueBird | 6 | 792.4 | 24.3556 | 9.9432 | 758.9 | 824.7 |
| Thomas | 2 | 804.8 | 7.0004 | 4.9500 | 799.8 | 809.7 |
| Diff (1-2) | -12.3333 | 22.4165 | 18.3030 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 6 | -0.67 | 0.5255 |
| Satterthwaite | Unequal | 5.9562 | -1.11 | 0.3096 |



Variable: Q

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BlueBird | 6 | 457.4 | 1.5526 | 0.6339 | 454.8 | 458.9 |
| Thomas | 2 | 501.2 | 0.6364 | 0.4500 | 500.7 | 501.6 |
| Diff (1-2) |  | -43.7833 | 1.4410 | 1.1765 |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 6 | -37.21 | $<.0001$ |
| Satterthwaite | Unequal | 4.9822 | -56.32 | $<.0001$ |



Variable: R

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 291.1 | 32.4881 | 13.2632 | 250.9 | 328.4 |
| Thomas | 2 | 228.7 | 22.8395 | 16.1500 | 212.5 | 244.8 |
| Diff (1-2) | 62.4667 | 31.0887 | 25.3838 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | 2.46 | 0.0491 |
| Satterthwaite | Unequal | 2.57 | 2.99 | 0.0707 |



Variable: S

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 71.4833 | 1.3423 | 0.5480 | 69.5000 | 73.1000 |
| Thomas | 2 | 70.8500 | 0.4950 | 0.3500 | 70.5000 | 71.2000 |
| Diff (1-2) |  | 0.6333 | 1.2419 | 1.0140 |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | 0.62 | 0.5552 |
| Satterthwaite | Unequal | 5.4099 | 0.97 | 0.3716 |



Variable: T

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 69.5000 | 3.8220 | 1.5603 | 63.8000 | 73.1000 |
| Thomas | 2 | 60.0500 | 1.0607 | 0.7500 | 59.3000 | 60.8000 |
| Diff (1-2) |  | 9.4500 | 3.5158 | 2.8706 |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | 3.29 | 0.0166 |
| Satterthwaite | Unequal | 5.981 | 5.46 | 0.0016 |



Variable: ARC

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 173.4 | 86.7393 | 35.4112 | 54.1000 | 243.3 |
| Thomas | 2 | 293.5 | 136.8 | 96.7000 | 196.8 | 390.2 |
| Diff (1-2) | -120.1 | 96.8851 | 79.1064 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -1.52 | 0.1798 |
| Satterthwaite | Unequal | 1.2816 | -1.17 | 0.4162 |



Variable: CHORD

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 74.6500 | 16.7534 | 6.8395 | 63.3000 | 108.0 |
| Thomas | 2 | 98.0500 | 5.7276 | 4.0500 | 94.0000 | 102.1 |
| Diff (1-2) | -23.4000 | 15.4714 | 12.6323 |  |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -1.85 | 0.1134 |
| Satterthwaite | Unequal | 5.6487 | -2.94 | 0.0277 |



Variable: LEFT

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 266.3 | 9.8813 | 4.0340 | 258.4 | 283.8 |
| Thomas | 2 | 198.6 | 11.2430 | 7.9500 | 190.6 | 206.5 |
| Diff (1-2) | 67.7500 | 10.1210 | 8.2637 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | 8.20 | 0.0002 |
| Satterthwaite | Unequal | 1.5606 | 7.60 | 0.0323 |



Variable: WALL

| mfg | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| BlueBird | 6 | 34.1167 | 18.0149 | 7.3546 | 19.9000 | 58.5000 |
| Thomas | 2 | 57.3500 | 0.3536 | 0.2500 | 57.1000 | 57.6000 |
| Diff (1-2) | -23.2333 | 16.4459 | 13.4281 |  |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 6 | -1.73 | 0.1343 |
| Satterthwaite | Unequal | 5.0115 | -3.16 | 0.0251 |


10. Appendix E-T Test Comparison of Passenger Car and Bus Dimensions

Variable: A

| vehtype | $\mathbf{N}$ | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 53.8281 | 21.3830 | 3.7800 | 19.3000 | 104.9 |
| Pas | 101 | 41.5327 | 15.7795 | 1.5701 | 4.5000 | 83.8000 |
| Diff (1-2) | 12.2955 | 17.2706 | 3.5035 |  |  |  |


| Method | Variances | DF | $\mathbf{t}$ Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 3.51 | 0.0006 |
| Satterthwaite | Unequal | 42.23 | 3.00 | 0.0045 |



Variable: B

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 74.6813 | 30.7707 | 5.4396 | 17.5000 | 119.5 |
| Pas | 101 | 75.4129 | 10.7408 | 1.0688 | 49.6000 | 97.1000 |
| Diff (1-2) |  | -0.7316 | 17.6671 | 3.5839 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | -0.20 | 0.8386 |
| Satterthwaite | Unequal | 33.424 | -0.13 | 0.8958 |



Variable: C

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 182.6 | 32.4337 | 5.7335 | 128.2 | 230.0 |
| Pas | 101 | 167.1 | 14.8079 | 1.4734 | 129.7 | 200.4 |
| Diff (1-2) |  | 15.4810 | 20.4039 | 4.1391 |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 3.74 | 0.0003 |
| Satterthwaite | Unequal | 35.182 | 2.62 | 0.0130 |



Variable: D

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 275.2 | 85.0104 | 15.0279 | 153.0 | 437.3 |
| Pas | 101 | 236.1 | 25.9236 | 2.5795 | 188.5 | 313.2 |
| Diff (1-2) |  | 39.1181 | 47.1504 | 9.5648 |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 4.09 | $<.0001$ |
| Satterthwaite | Unequal | 32.845 | 2.57 | 0.0151 |



Variable: E

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 145.1 | 25.8894 | 4.5766 | 100.6 | 180.9 |
| Pas | 101 | 154.1 | 11.8187 | 1.1760 | 121.2 | 181.8 |
| Diff (1-2) | -8.9315 | 16.2862 | 3.3038 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | -2.70 | 0.0078 |
| Satterthwaite | Unequal | 35.181 | -1.89 | 0.0670 |



Variable: F

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 93.8000 | 62.7297 | 11.0891 | 30.4000 | 224.1 |
| Pas | 101 | 61.9356 | 26.9239 | 2.6790 | 0.8000 | 126.0 |
| Diff (1-2) | 31.8644 | 38.5298 | 7.8160 |  |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 4.08 | $<.0001$ |
| Satterthwaite | Unequal | 34.688 | 2.79 | 0.0084 |



Variable: G

| vehtype | $\mathbf{N}$ | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 191.9 | 48.4997 | 8.5736 | 121.5 | 291.1 |
| Pas | 101 | 152.7 | 33.5422 | 3.3376 | 32.0000 | 211.1 |
| Diff (1-2) |  | 39.1798 | 37.6228 | 7.6320 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 5.13 | $<.0001$ |
| Satterthwaite | Unequal | 40.817 | 4.26 | 0.0001 |



Variable: H

| vehtype | $\mathbf{N}$ | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 27.5563 | 21.5652 | 3.8122 | 0.3000 | 57.5000 |
| Pas | 101 | 50.2495 | 11.5284 | 1.1471 | 22.0000 | 77.6000 |
| Diff (1-2) |  | -22.6933 | 14.5432 | 2.9502 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | -7.69 | $<.0001$ |
| Satterthwaite | Unequal | 36.774 | -5.70 | $<.0001$ |



Variable: I

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 85.4938 | 39.8386 | 7.0425 | 17.6000 | 125.0 |
| Pas | 101 | 154.5 | 13.9274 | 1.3858 | 103.8 | 188.5 |
| Diff (1-2) |  | -68.9944 | 22.8833 | 4.6420 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | -14.86 | $<.0001$ |
| Satterthwaite | Unequal | 33.432 | -9.61 | $<.0001$ |



Variable: J

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 63.6531 | 26.2287 | 4.6366 | 16.4000 | 94.0000 |
| Pas | 101 | 113.4 | 13.2135 | 1.3148 | 76.9000 | 167.3 |
| Diff (1-2) |  | -49.7192 | 17.2068 | 3.4905 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 131 | -14.24 | $<.0001$ |
| Satterthwaite | Unequal | 36.113 | -10.32 | $<.0001$ |



Variable: L

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 502.3 | 21.3798 | 3.7794 | 459.5 | 540.4 |
| Pas | 101 | 527.8 | 41.1022 | 4.0898 | 458.3 | 716.6 |
| Diff (1-2) |  | -25.4525 | 37.3868 | 7.5842 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | -3.36 | 0.0010 |
| Satterthwaite | Unequal | 102.53 | -4.57 | $<.0001$ |



Variable: M

| vehtype | $\mathbf{N}$ | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 48.0906 | 56.3456 | 9.9606 | 0.4000 | 201.2 |
| Pas | 101 | 25.5970 | 20.7130 | 2.0610 | 0.7000 | 79.6000 |
| Diff (1-2) | 22.4936 | 32.8451 | 6.6629 |  |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 3.38 | 0.0010 |
| Satterthwaite | Unequal | 33.692 | 2.21 | 0.0339 |



Variable: N

| vehtype | $\mathbf{N}$ | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 33.0938 | 22.9139 | 4.0506 | 0.5000 | 67.2000 |
| Pas | 101 | 51.4941 | 12.8654 | 1.2802 | 17.4000 | 79.6000 |
| Diff (1-2) |  | -18.4003 | 15.8303 | 3.2113 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | -5.73 | $<.0001$ |
| Satterthwaite | Unequal | 37.386 | -4.33 | 0.0001 |



Variable: O

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 543.1 | 68.7606 | 12.1553 | 441.4 | 681.1 |
| Pas | 101 | 526.6 | 41.9284 | 4.1720 | 451.2 | 627.9 |
| Diff (1-2) |  | 16.4787 | 49.6067 | 10.0631 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 1.64 | 0.1039 |
| Satterthwaite | Unequal | 38.568 | 1.28 | 0.2074 |



Variable: P

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 804.9 | 37.3201 | 6.5973 | 668.6 | 858.0 |
| Pas | 101 | 628.2 | 28.5108 | 2.8369 | 561.1 | 689.2 |
| Diff (1-2) |  | 176.7 | 30.8237 | 6.2528 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 28.26 | $<.0001$ |
| Satterthwaite | Unequal | 43.068 | 24.61 | $<.0001$ |



Variable: Q

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 457.2 | 13.5290 | 2.3916 | 441.7 | 501.6 |
| Pas | 101 | 381.6 | 8.0037 | 0.7964 | 339.3 | 399.9 |
| Diff (1-2) |  | 75.6320 | 9.6028 | 1.9480 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 38.83 | $<.0001$ |
| Satterthwaite | Unequal | 38.111 | 30.00 | $<.0001$ |



Variable: R

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 358.9 | 64.0058 | 11.3147 | 212.5 | 485.7 |
| Pas | 101 | 561.8 | 33.7973 | 3.3630 | 474.3 | 645.6 |
| Diff (1-2) |  | -202.8 | 42.9117 | 8.7049 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | -23.30 | $<.0001$ |
| Satterthwaite | Unequal | 36.63 | -17.18 | $<.0001$ |



Variable: S

| vehtype | $\mathbf{N}$ | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 92.6781 | 12.9559 | 2.2903 | 69.5000 | 106.8 |
| Pas | 101 | 120.7 | 16.2191 | 1.6139 | 81.8000 | 150.0 |
| Diff (1-2) |  | -27.9981 | 15.5090 | 3.1461 |  |  |


| Method | Variances | DF | t Value | $\operatorname{Pr}>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | :--- |
| Pooled | Equal | 131 | -8.90 | $<.0001$ |
| Satterthwaite | Unequal | 64.498 | -9.99 | $<.0001$ |



Variable: T

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 56.7750 | 7.2392 | 1.2797 | 48.4000 | 73.1000 |
| Pas | 101 | 46.5198 | 8.5872 | 0.8545 | 27.2000 | 75.3000 |
| Diff (1-2) |  | 10.2552 | 8.2881 | 1.6813 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 6.10 | $<.0001$ |
| Satterthwaite | Unequal | 61.041 | 6.66 | $<.0001$ |



Variable: ARC

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 241.1 | 94.8178 | 16.7616 | 54.1000 | 588.3 |
| Pas | 100 | 205.1 | 83.9152 | 8.3915 | 18.1000 | 438.0 |
| Diff (1-2) |  | 36.0146 | 86.6397 | 17.5966 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 130 | 2.05 | 0.0427 |
| Satterthwaite | Unequal | 47.552 | 1.92 | 0.0607 |



Variable: CHORD

| vehtype | N | Mean | Std Dev | Std Err | Minimum | Maximum |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Bus | 32 | 69.1844 | 17.5084 | 3.0951 | 32.4000 | 108.0 |
| Pas | 101 | 62.3535 | 12.3307 | 1.2269 | 23.5000 | 92.3000 |
| Diff (1-2) |  | 6.8309 | 13.7334 | 2.7859 |  |  |


| Method | Variances | DF | t Value | Pr $>\|\mathbf{t}\|$ |
| :--- | :--- | ---: | ---: | ---: |
| Pooled | Equal | 131 | 2.45 | 0.0155 |
| Satterthwaite | Unequal | 41.193 | 2.05 | 0.0466 |


11. Appendix F - Comparison of Passenger Car Dimensions to Type C and D Buses

Dependent Variable: A

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 268651.3291 | 89550.4430 | 311.58 | $<.0001$ |
| Error | 130 | 37362.5009 | 287.4039 |  |  |
| Uncorrected Total | 133 | 306013.8300 |  |  |  |

R-Square Coeff Var Root MSE A Mean
$\begin{array}{llll}0.125970 & 38.10433 & 16.95299 & 44.49098\end{array}$


## Scheffe's Test for A

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 287.4039 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type C Bus - Pass. Car | 16.517 | 6.984 | 26.050 | * |
| Type C Bus - Type D Bus | 16.887 | -0.251 | 34.026 |  |
| Pass. Car - Type C Bus | -16.517 | -26.050 | -6.984 | ** |
| Pass. Car - Type D Bus | 0.370 | -15.048 | 15.789 |  |
| Type D Bus - Type C Bus | -16.887 | -34.026 | 0.251 |  |
| Type D Bus - Pass. Car | -0.370 | -15.789 | 15.048 |  |

Dependent Variable: B

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 773797.7884 | 257932.5961 | 1679.82 | $<.0001$ |
| Error | 130 | 19961.2416 | 153.5480 |  |  |
| Uncorrected Total | 133 | 793759.0300 |  |  |  |

R-Square Coeff Var Root MSE B Mean
$\begin{array}{lllll}0.511969 & 16.46992 & 12.39145 & 75.23684\end{array}$



Dependent Variable: C

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 3905685.874 | 1301895.291 | 4886.30 | $<.0001$ |
| Error | 130 | 34636.906 | 266.438 |  |  |
| Uncorrected Total | 133 | 3940322.780 |  |  |  |


| R-Square | Coeff V | Root <br> MSE | C Mean |
| :--- | :--- | ---: | ---: | ---: |
| 0.426177 | 9.556745 | 16.32292 | 170.8000 |



## Scheffe's Test for C

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 266.4377 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type C Bus - Pass. Car | 29.879 | 20.700 | 39.058 | * |
| Type C Bus - Type D Bus | 57.592 | 41.091 | 74.093 | *** |
| Pass. Car - Type C Bus | -29.879 | -39.058 | -20.700 | * |
| Pass. Car - Type D Bus | 27.713 | 12.867 | 42.558 | *** |
| Type D Bus - Type C Bus | -57.592 | -74.093 | -41.091 | *** |
| Type D Bus - Pass. Car | -27.713 | -42.558 | -12.867 | *** |

Dependent Variable: D

\[\)|  Source  |  DF  |  Sum of Squares  |  Mean Square  |  F Value  |  Pr $>\text { F }$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
|  Model  | 3 | 8210720.702 | 2736906.901 | 2638.10 | $<.0001$ |
|  Error  | 130 | 134869.158 | 1037.455 |  |  |
|  Uncorrected Total  | 133 | 8345589.860 |  |  |  |

\]

## R-Square Coeff Var Root MSE D Mean

$\begin{array}{llll}0.589338 & 13.11897 & 32.20955 & 245.5188\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 1037.455 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type D Bus - Pass. Car | 160.193 | 130.899 | 189.487 | * |
| Type D Bus - Type C Bus | 161.433 | 128.872 | 193.994 | *** |
| Pass. Car - Type D Bus | -160.193 | -189.487 | -130.899 | * |
| Pass. Car - Type C Bus | 1.240 | -16.872 | 19.352 |  |
| Type C Bus - Type D Bus | -161.433 | -193.994 | -128.872 | *** |
| Type C Bus - Pass. Car | -1.240 | -19.352 | 16.872 |  |

Dependent Variable: E

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Model | 3 | 3086007.567 | 1028669.189 | 6513.50 | $<.0001$ |
| Error | 130 | 20530.753 | 157.929 |  |  |
| Uncorrected Total | 133 | 3106538.320 |  |  |  |


| R-Square | Coeff Var | Root MSE | E Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.440347 | 8.271757 | 12.56698 | 151.9263 |



| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 157.9289 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the 0.05 level were indicated by $* * *$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type C Bus - Pass. Car | 3.237 | -3.829 | 10.304 |  |
| Type C Bus - Type D Bus | 48.675 | 35.971 | 61.379 | *** |
| Pass. Car - Type C Bus | -3.237 | -10.304 | 3.829 |  |
| Pass. Car - Type D Bus | 45.438 | 34.008 | 56.867 | *** |
| Type D Bus - Type C Bus | -48.675 | -61.379 | -35.971 | *** |
| Type D Bus - Pass. Car | -45.438 | -56.867 | -34.008 | *** |

Dependent Variable: F

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 758732.2383 | 252910.7461 | 313.93 | $<.0001$ |
| Error | 130 | 104731.4317 | 805.6264 |  |  |
| Uncorrected Total | 133 | 863463.6700 |  |  |  |
|  |  |  |  |  |  |


| R-Square | Coeff Var | Root MSE | F Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.522099 | 40.77965 | 28.38356 | 69.60226 |



## Scheffe's Test for F

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 805.6264 |
| Critical Value of F | 3.06584 |

Comparisons significant at the 0.05 level were indicated by $* * *$. vehtype Difference Simultaneous 95\% Confidence Comparison Between

Limits
Means

| Type D Bus - Type C Bus | 122.300 | 93.607 | 150.993 | $* * *$ |
| :--- | ---: | ---: | ---: | :--- |
| Type D Bus - Pass. Car | 123.589 | 97.775 | 149.404 | $* * *$ |
| Type C Bus - Type D Bus | -122.300 | -150.993 | -93.607 | $* * *$ |
| Type C Bus - Pass. Car | 1.289 | -14.671 | 17.250 |  |
| Pass. Car - Type D Bus | -123.589 | -149.404 | -97.775 | $* * *$ |
| Pass. Car - Type C Bus | -1.289 | -17.250 | 14.671 |  |

Dependent Variable: G

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 3576776.085 | 1192258.695 | 1095.15 | $<.0001$ |
| Error | 130 | 141527.055 | 1088.670 |  |  |
| Uncorrected Total | 133 | 3718303.140 |  |  |  |


| R-Square | Coeff Var | Root MSE | G Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.364580 | 20.35236 | 32.99499 | 162.1188 |



## Scheffe's Test for G

|  | Alpha |  | 0.05 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Error | Degrees of Fr | reedom 130 |  |  |
|  | Error | Mean Square | 1088.67 |  |  |
|  | Critic | Value of $F$ | 3.06584 |  |  |
| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |  |
| vehtype Comparison |  | Difference Simultaneous 95\% Confidence Between Limits Means |  |  |  |
| Type D Bus - Type C Bus |  | 85.538 | 52.182 | 118.893 | ** |
| Type D Bus - Pass. Car |  | 103.333 | 73.324 | 133.341 | ** |
| Type C Bus - Type D Bus |  | -85.538 | -118.893 | -52.182 | *** |
| Type C Bus - Pass. Car |  | 17.795 | -0.758 | 36.349 |  |
| Pass. Car - Type D Bus |  | -103.333 | -133.341 | -73.324 | *** |
| Pass. Car - Type C Bus |  | -17.795 | -36.349 | 0.758 |  |

Dependent Variable: H

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 280162.0092 | 93387.3364 | $451.81<.0001$ |  |
| Error | 130 | 26870.4508 | 206.6958 |  |  |
| Uncorrected Total | 133 | 307032.4600 |  |  |  |


| R-Square | Coeff Var | Root MSE | H Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.331939 | 32.09888 | 14.37692 | 44.78947 |



| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 206.6958 |
| Critical Value of F | 3.06584 |

Comparisons significant at the 0.05 level were indicated by ***. vehtype
Comparison

| Pass. Car - Type C Bus | 19.741 | 11.657 | 27.826 | $* * *$ |
| :---: | ---: | ---: | ---: | ---: |
| Pass. Car - Type D Bus | 31.550 | 18.474 | 44.625 | $* * *$ |
| Type C Bus - Pass. Car | -19.741 | -27.826 | -11.657 | $* * *$ |
| Type C Bus - Type D Bus | 11.808 | -2.725 | 26.342 |  |
| Type D Bus - Pass. Car | -31.550 | -44.625 | -18.474 | $* * *$ |
| Type D Bus - Type C Bus | -11.808 | -26.342 | 2.725 |  |

Dependent Variable: I

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 2686310.236 | 895436.745 | 4358.85 | $<.0001$ |
| Error | 130 | 26705.874 | 205.430 |  |  |
| Uncorrected Total | 133 | 2713016.110 |  |  |  |


| R-Square | Coeff Var | Root MSE | I Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.855076 | 10.39454 | 14.33282 | 137.8880 |



## Scheffe's Test for I

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 205.4298 |
| Critical Value of F | 3.06584 |


| Comparisons signifi vehtype Comparison | ant at the 0 Difference Between Means | 05 level were in Simultaneous Li | by ***. <br> onfidence |  |
| :---: | :---: | :---: | :---: | :---: |
| Pass. Car - Type C Bus | 48.105 | 40.045 | 56.164 | *** |
| Pass. Car - Type D Bus | 131.663 | 118.628 | 144.699 | *** |
| Type C Bus - Pass. Car | -48.105 | -56.164 | -40.045 | *** |
| Type C Bus - Type D Bus | 83.558 | 69.069 | 98.048 | *** |
| Type D Bus - Pass. Car | -131.663 | -144.699 | -118.628 | ** |
| Type D Bus - Type C Bus | -83.558 | -98.048 | -69.069 | *** |

Dependent Variable: J

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- |
| Model | 3 | 1443169.991 | 481056.664 | 2666.67 | $<.0001$ |
| Error | 130 | 23451.499 | 180.396 |  |  |
| Uncorrected Total | 133 | 1466621.490 |  |  |  |


| R-Square | Coeff Var | Root MSE | J Mean |
| ---: | ---: | ---: | ---: |
| 0.762774 | 13.24445 | 13.43116 | 101.4098 |



## Scheffe's Test for J

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 180.3961 |
| Critical Value of F | 3.06584 |

Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***.
vehtype
Comparison

Pass. Car - Type C Bus
Pass. Car - Type D Bus
Type C Bus - Pass. Car
Type C Bus - Type D Bus
Type D Bus - Pass. Car
Type D Bus - Type C Bus

Difference Simultaneous 95\% Confidence Between Limits Means

| 37.081 | 29.528 | $44.633^{* * *}$ |  |
| ---: | ---: | ---: | ---: |
| 87.635 | 75.419 | $99.850^{* * *}$ |  |
| -37.081 | -44.633 | $-29.528^{* * *}$ |  |
| 50.554 | 36.976 | $64.132^{* * *}$ |  |
| -87.635 | -99.850 | -75.419 | *** |
| -50.554 | -64.132 | -36.976 | *** |

Dependent Variable: L

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- |
| Model | 3 | 36207172.50 | 12069057.50 | 8568.78 | $<.0001$ |
| Error | 130 | 183103.87 | 1408.49 |  |  |
| Uncorrected Total | 133 | 36390276.37 |  |  |  |

R-Square Coeff Var Root MSE L Mean
$\begin{array}{llll}0.079193 & 7.194491 & 37.52987 & 521.6474\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 1408.491 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| vehtype Difference Simultaneous 95\% Confidence <br> Comparison Between Limits |  |  |  |  |
|  |  |  |  |  |
| Pass. Car - Type C Bus | 25.230 | 4.126 | 46.333 | *** |
| Pass. Car - Type D Bus | 26.121 | -8.012 | 60.254 |  |
| Type C Bus - Pass. Car | -25.230 | -46.333 | -4.126 | *** |
| Type C Bus - Type D Bus | 0.892 | -37.048 | 38.831 |  |
| Type D Bus - Pass. Car | -26.121 | -60.254 | 8.012 |  |
| Type D Bus - Type C Bus | -0.892 | -38.831 | 37.048 |  |

Dependent Variable: M

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 221563.7471 | 73854.5824 | 160.17 | $<.0001$ |
| Error | 130 | 59941.4529 | 461.0881 |  |  |
| Uncorrected Total | 133 | 281505.2000 |  |  |  |

R-Square Coeff Var Root MSE M Mean<br>$\begin{array}{llll}0.609801 & 69.24747 & 21.47296 & 31.00902\end{array}$




Dependent Variable: N

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 303361.3286 | 101120.4429 | 406.63 | $<.0001$ |
| Error | 130 | 32328.6414 | 248.6819 |  |  |
| Uncorrected Total | 133 | 335689.9700 |  |  |  |

R-Square Coeff Var Root MSE N Mean
$\begin{array}{llll}0.212568 & 33.50474 & 15.76965 & 47.06692\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 248.6819 |
| Critical Value of F | 3.06584 |

Comparisons significant at the 0.05 level were indicated by ***. vehtype
Comparison

| Pass. Car - Type C Bus | 16.119 | 7.252 | 24.987 | $* * *$ |
| :---: | ---: | ---: | ---: | ---: |
| Pass. Car - Type D Bus | 25.244 | 10.902 | 39.586 | $* * *$ |
| Type C Bus - Pass. Car | -16.119 | -24.987 | -7.252 | $* * *$ |
| Type C Bus - Type D Bus | 9.125 | -6.817 | 25.067 |  |
| Type D Bus - Pass. Car | -25.244 | -39.586 | -10.902 | $* * *$ |
| Type D Bus - Type C Bus | -9.125 | -25.067 | 6.817 |  |

Dependent Variable: O

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 37522244.93 | 12507414.98 | 6492.93 | $<.0001$ |
| Error | 130 | 250420.87 | 1926.31 |  |  |
| Uncorrected Total | 133 | 37772665.80 |  |  |  |


| R-Square | Coeff Var | Root MSE | O Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.238765 | 8.271800 | 43.88980 | 530.5955 |



| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 1926.314 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the 0.05 level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type D Bus - Pass. Car | 98.607 | 58.690 | 138.524 | *** |
| Type D Bus - Type C Bus | 109.504 | 65.135 | 153.873 |  |
| Pass. Car - Type D Bus | -98.607 | -138.524 | -58.690 | *** |
| Pass. Car - Type C Bus | 10.897 | -13.782 | 35.577 |  |
| Type C Bus - Type D Bus | -109.504 | -153.873 | -65.135 | *** |
| Type C Bus - Pass. Car | -10.897 | -35.577 | 13.782 |  |

Dependent Variable: P

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- |
| Model | 3 | 60590355.42 | 20196785.14 | 21256.6 | $<.0001$ |
| Error | 130 | 123518.64 | 950.14 |  |  |
| Uncorrected Total | 133 | 60713874.06 |  |  |  |


| R-Square | Coeff Var | Root MSE | P Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.860169 | 4.595777 | 30.82440 | 670.7113 |



| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 950.1434 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the 0.05 level were indicated by ***. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type C Bus - Type D Bus | 12.546 | -18.615 | 43.707 |  |
| Type C Bus - Pass. Car | 179.853 | 162.520 | 197.186 | *** |
| Type D Bus - Type C Bus | -12.546 | -43.707 | 18.615 |  |
| Type D Bus - Pass. Car | 167.307 | 139.272 | 195.341 | *** |
| Pass. Car - Type C Bus | -179.853 | -197.186 | -162.520 | *** |
| Pass. Car - Type D Bus | -167.307 | -195.341 | -139.272 | *** |

Dependent Variable: Q

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 21400316.05 | 7133438.68 | 86073.7 | $<.0001$ |
| Error | 130 | 10773.87 | 82.88 |  |  |
| Uncorrected Total | 133 | 21411089.92 |  |  |  |


| R-Square | Coeff Var | Root MSE | Q Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.928690 | 2.276976 | 9.103623 | 399.8120 |

## Distribution of Q



```
Scheffe's Test for Q
```

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 82.87596 |
| Critical Value of F | 3.06584 |

Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***.
vehtype
Comparison

Difference Simultaneous 95\% Confidence Between

Limits Means

| Type D Bus - Type C Bus | 14.754 | 5.551 | 23.957 | $* * *$ |
| :--- | ---: | ---: | ---: | :--- |
| Type D Bus - Pass. Car | 86.698 | 78.418 | 94.977 | $* * *$ |
| Type C Bus - Type D Bus | -14.754 | -23.957 | -5.551 | $* * *$ |
| Type C Bus - Pass. Car | 71.943 | 66.824 | 77.063 | $* * *$ |
| Pass. Car - Type D Bus | -86.698 | -94.977 | -78.418 | $* * *$ |
| Pass. Car - Type C Bus | -71.943 | -77.063 | -66.824 | $* * *$ |

Dependent Variable: R

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Model | 3 | 36069305.70 | 12023101.90 | 9359.99 | $<.0001$ |
| Error | 130 | 166987.72 | 1284.52 |  |  |
| Uncorrected Total | 133 | 36236293.42 |  |  |  |

\author{

R-Square Coeff Var Root MSE R Mean <br> | 0.865438 | 6.987011 | 35.84021 | 512.9549 |
| :--- | :--- | :--- | :--- |

}


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 1284.521 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Pass. Car - Type C Bus | 175.023 | 154.870 | 195.177 | * |
| Pass. Car - Type D Bus | 286.256 | 253.660 | 318.853 | *** |
| Type C Bus - Pass. Car | -175.023 | -195.177 | -154.870 |  |
| Type C Bus - Type D Bus | 111.233 | 75.002 | 147.465 | *** |
| Type D Bus - Pass. Car | -286.256 | -318.853 | -253.660 | * |
| Type D Bus - Type C Bus | -111.233 | -147.465 | -75.002 | * |

Dependent Variable: S

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Model | 3 | 1750557.232 | 583519.077 | 2846.88 | $<.0001$ |
| Error | 130 | 26645.828 | 204.968 |  |  |
| Uncorrected Total | 133 | 1777203.060 |  |  |  |


| R-Square | Coeff Var | Root MSE | S Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.472971 | 12.56514 | 14.31670 | 113.9398 |



| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 204.9679 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the 0.05 level were indicated by ***. |  |  |
| :---: | :---: | :---: |
| vehtype | Difference | Simultaneous 95\% Confidence |
| Comparison | Between | Limits |
|  | Means |  |


| Pass. Car - Type C Bus | 20.880 | 12.830 | 28.931 | $* * *$ |
| :---: | ---: | ---: | ---: | ---: |
| Pass. Car - Type D Bus | 49.351 | 36.330 | 62.372 | $* * *$ |
| Type C Bus - Pass. Car | -20.880 | -28.931 | -12.830 | $* * *$ |
| Type C Bus - Type D Bus | 28.471 | 13.998 | 42.944 | $* * *$ |
| Type D Bus - Pass. Car | -49.351 | -62.372 | -36.330 | $* * *$ |
| Type D Bus - Type C Bus | -28.471 | -42.944 | -13.998 | $* * *$ |

Dependent Variable: T

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 322867.5113 | 107622.5038 | 1781.55 | $<.0001$ |
| Error | 130 | 7853.2387 | 60.4095 |  |  |
| Uncorrected Total | 133 | 330720.7500 |  |  |  |


| R-Square | Coeff Var | Root MSE | T Mean |
| ---: | ---: | ---: | ---: | ---: |
| 0.320321 | 15.86609 | 7.772357 | 48.98722 |



## Scheffe's Test for T

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 60.40953 |
| Critical Value of F | 3.06584 |

Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. vehtype Difference Simultaneous 95\% Confidence Comparison Between Limits Means

| Type D Bus - Type C Bus | 13.817 | 5.959 | 21.674 | $* * *$ |
| :---: | ---: | ---: | ---: | :--- |
| Type D Bus - Pass. Car | 20.618 | 13.549 | 27.687 | $* * *$ |
| Type C Bus - Type D Bus | -13.817 | -21.674 | -5.959 | $* * *$ |
| Type C Bus - Pass. Car | 6.801 | 2.431 | 11.172 | $* * *$ |
| Pass. Car - Type D Bus | -20.618 | -27.687 | -13.549 | $* * *$ |
| Pass. Car - Type C Bus | -6.801 | -11.172 | -2.431 | $* * *$ |

Dependent Variable: ARC

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 6079298.273 | 2026432.758 | 272.09 | $<.0001$ |
| Error | 129 | 960734.567 | 7447.555 |  |  |
| Uncorrected Total | 132 | 7040032.840 |  |  |  |

R-Square Coeff Var Root MSE ARC Mean
$\begin{array}{llll}0.046210 & 40.36789 & 86.29922 & 213.7818\end{array}$


| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 129 |
| Error Mean Square | 7447.555 |
| Critical Value of F | 3.06639 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by ***. |  |  |  |
| :---: | ---: | :---: | ---: |
| vehtype <br> Comparison | Difference <br> Between <br> Means | Simultaneous 95\% Confidence <br> Limits |  |
| Type C Bus - Pass. Car | 48.56 | -0.02 | 97.14 |
| Type C Bus - Type D Bus | 50.17 | -37.08 | 137.42 |
| Pass. Car - Type C Bus | -48.56 | -97.14 | 0.02 |
| Pass. Car - Type D Bus | 1.61 | -76.91 | 80.14 |
| Type D Bus - Type C Bus | -50.17 | -137.42 | 37.08 |
| Type D Bus - Pass. Car | -1.61 | -80.14 | 76.91 |

Dependent Variable: CHORD

| Source | DF | Sum of Squares | Mean Square | F Value | Pr $>$ F |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Model | 3 | 547216.5025 | 182405.5008 | 1015.90 | $<.0001$ |
| Error | 130 | 23341.6775 | 179.5514 |  |  |
| Uncorrected Total | 133 | 570558.1800 |  |  |  |

R-Square Coeff Var Root MSE CHORD Mean

| 0.096733 | 20.93798 | 13.39968 | 63.99699 |
| :--- | :--- | :--- | :--- |

Distribution of CHORD


## Scheffe's Test for CHORD

| Alpha | 0.05 |
| :--- | ---: |
| Error Degrees of Freedom | 130 |
| Error Mean Square | 179.5514 |
| Critical Value of F | 3.06584 |


| Comparisons significant at the $\mathbf{0 . 0 5}$ level were indicated by $* * *$. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type D Bus - Type C Bus | 15.088 | 1.542 | 28.633 | * |
| Type D Bus - Pass. Car | 18.147 | 5.960 | 30.333 | * |
| Type C Bus - Type D Bus | -15.088 | -28.633 | -1.542 | * |
| Type C Bus - Pass. Car | 3.059 | -4.476 | 10.594 |  |
| Pass. Car - Type D Bus | -18.147 | -30.333 | -5.960 | *** |
| Pass. Car - Type C Bus | -3.059 | -10.594 | 4.476 |  |



U.S. Department of Transportation National Highway Traffic Safety Administration


[^0]:    ${ }^{1}$ National Transportation Safety Board. (2009, September 1). Pedal misapplcations in heavy vehicles. (Special Investigation Report. Report No. NTSB/ST-0902 PB2009-917003, Notation 1841A). Washington, DC: Author. Available at www.ntsb.gov/doclib/safetystudies/SIR0902.pdf
    ${ }^{2}$ Collins, W., Evans, L., \& Hughes, R.. (n.a.) An analysis of the relationship between driver brake and accelerator controls and reported pedal misapplication rates in North Carolina. (Unpublished NHTSA report). Washington, DC: National Highway Traffic Safety Administration.

[^1]:    ${ }^{3}$ Pollard, J., \& Sussman, E. D. (1989, January). An examination of sudden acceleration. (Report No. DOT HS 807 367). Washington, DC: National Highway Traffic Safety Administration. Available at www.autosafety.org/sites/default/files/1989\%20NHTSA\%20SA\%20Study\%20Report\%20\&\%20Appendices\%20AD(1).pdf
    ${ }^{4}$ Recommendation H-09-01, page 37and H-99-53, page 38
    ${ }^{5}$ Recommendation H-99-54, page 38
    ${ }^{6}$ Recommendation H-09-12, page 37
    ${ }^{7}$ Recommendation $\mathrm{H}=09-13$, page 37

[^2]:    ${ }^{8}$ Collins, Evans, \& Hughes (n.a.)
    ${ }^{9}$ Lococo, K. H., Staplin, L., Martell, C. A., \& Sifrit, K. J. (March 2012). Pedal Application Errors. (Report No. DOT HS 811 597). Washington, DC: National Highway Traffic Safety Administration.
    ${ }^{10}$ Ibid.
    ${ }^{11}$ Pollard, \& Sussman (1989.

[^3]:    ${ }^{12}$ National Highway Traffic Safety Administration. (1999, January). Investigation of Sudden Acceleration Incident in Minneapolis, MN, by Bob Young. (Office of Defect Investigation, Memorandum Report MF99-002, pp 8).
    Washington, DC: Author.
    ${ }^{13}$ NHTSA Campaign ID Number:83V095000.

[^4]:    ${ }^{14}$ Society of Automotive Engineers. (2009). SAE J1 100 surface vehicle recommended practice, (R) Motor Vehicle Dimensions, Rev. 2009. Warrendale, PA: Author.

