

Examining the Relationship Between Quasi-Static Testing and Dynamic Crash Response of Heavy Truck Rear Impact Guards through Simulation

Alex J. Kalmar-Gonzalo, Berkan Guleyupoglu, Derek A. Jones

SAE Government-Industry Meeting, 2024



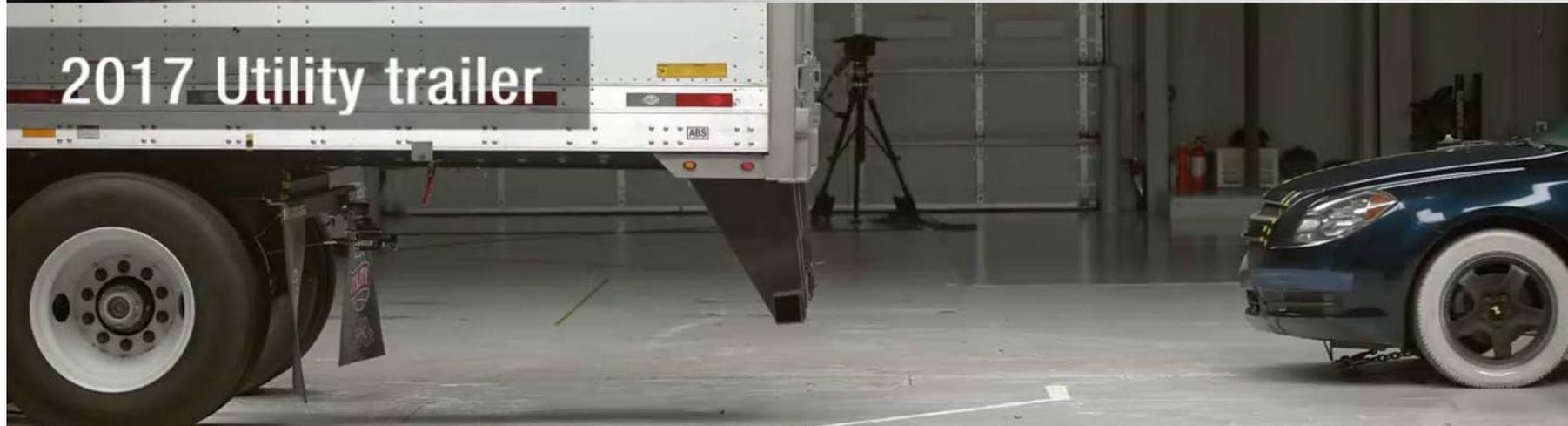
5,788 deaths in traffic crashes involving large trucks in USA 2021¹

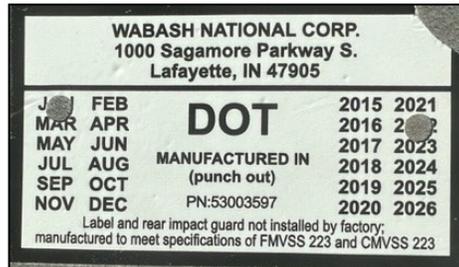
- Increased 17% compared to 2020
- Account for 13% of all motor vehicle traffic fatalities
- 72% of these traffic fatalities were occupants of vehicles other than the large truck

Between 2008-2009, 977 fatalities from rear-end strikes²

¹FARS 2021 Annual Report

²DOT HS 811 725, March 2023





1996 – FMVSS
223 & 224
Established

2021 – IIHS
Semitrailer
Underride Testing
Updated



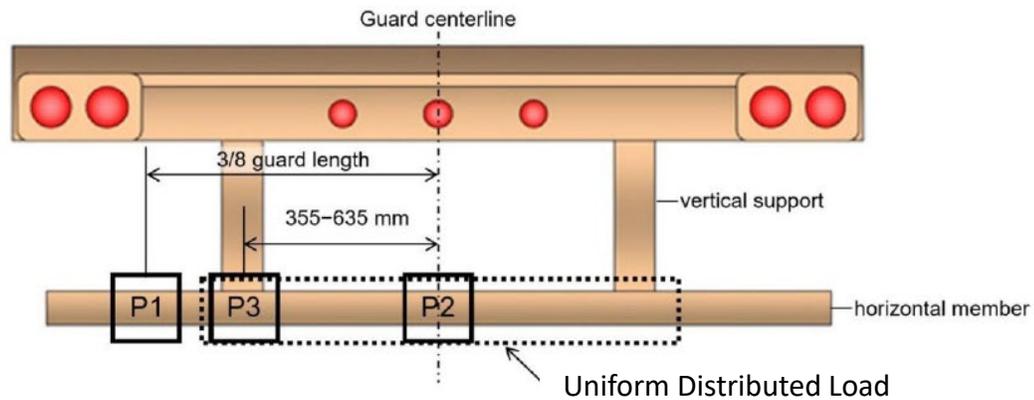
2016 – IIHS
Semitrailer
Underride Testing
Introduced

2022 FMVSS 223
& 224 Upgraded



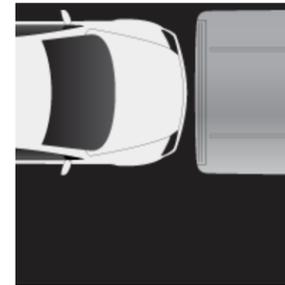
DEPARTMENT OF TRANSPORTATION
National Highway Traffic Safety
Administration
49 CFR Part 571
[Docket No. NHTSA-2022-0053]
RIN 2127-AL58
Federal Motor Vehicle Safety
Standards; Rear Impact Guards, Rear
Impact Protection
AGENCY: National Highway Traffic
Safety Administration (NHTSA),
Department of Transportation (DOT).
ACTION: Final rule.

Quasi-Static Loading per 2022 Final Rule:

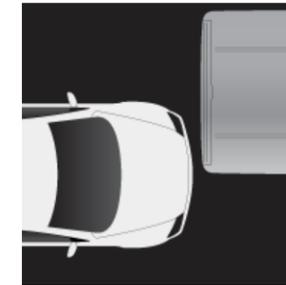


Regulation	Force within 125 mm			Energy Absorption
	P1	P2	UDL	
FMVSS No. 223 (2022)	50 kN	50 kN	350 kN	20 kJ in UDL

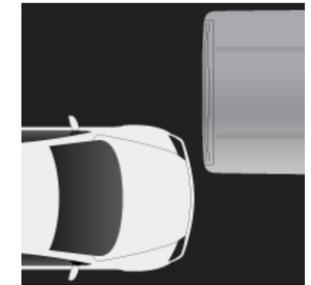
Dynamic Testing per IIHS Toughguard award:



FULL WIDTH
The car crashes into the center of the truck's rear.



50 PERCENT OVERLAP
Half of the car's width overlaps the rear of the truck.



30 PERCENT OVERLAP
Thirty percent of the car's width overlaps the rear of the truck.

Study Goal: Examine the relationship between quasi-static rear impact guard requirements and dynamic crash structural performance, including occupant response

- Aim 1: Develop Model of 3 Rear Impact Guards and Validate Against Quasi-Static Testing
- Aim 2: Modify guard models to minimally pass FMVSS regulations. Evaluate performance in simulated full crash tests. Strengthen guards to prevent PCI in 30% overlap and re-test in quasi-static conditions
- Aim 3: Investigate the effectiveness of guards at higher velocity crash modes

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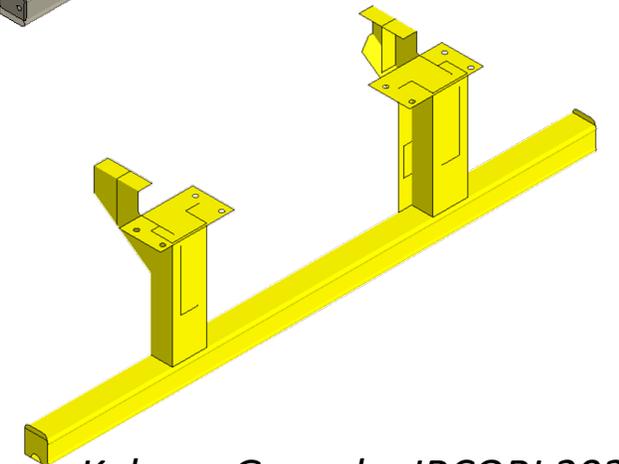
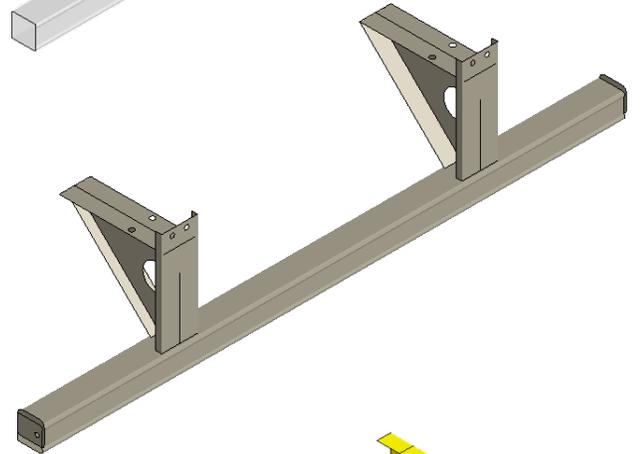
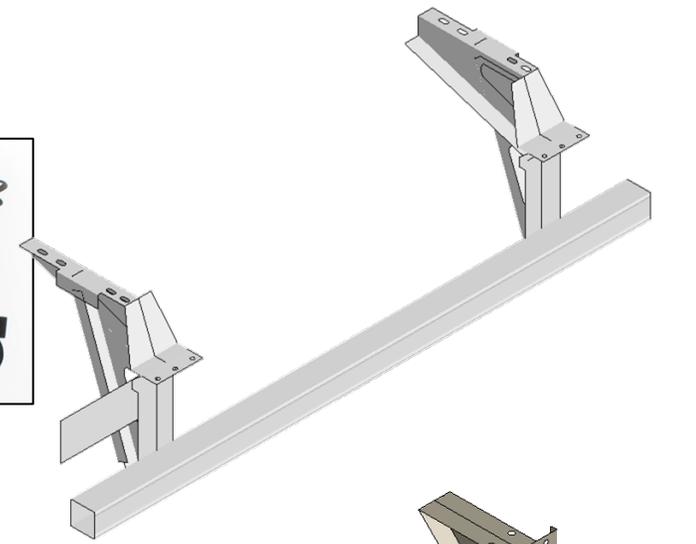
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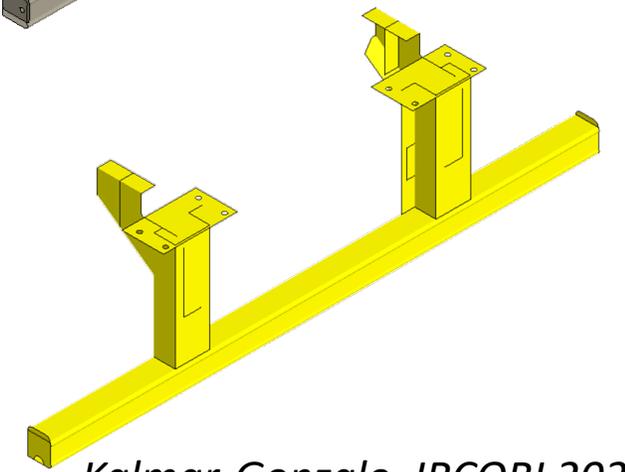
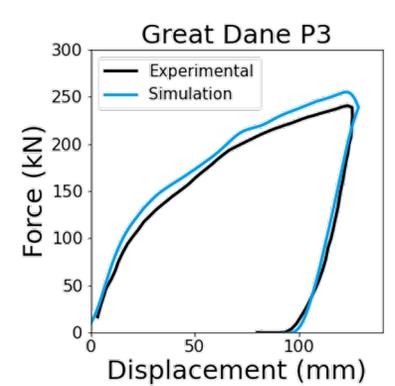
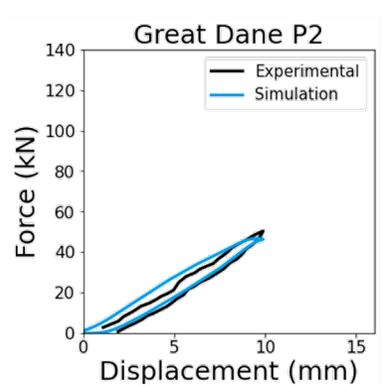
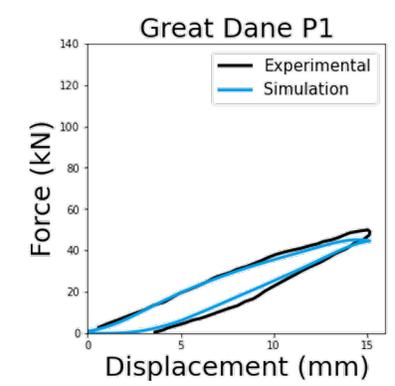
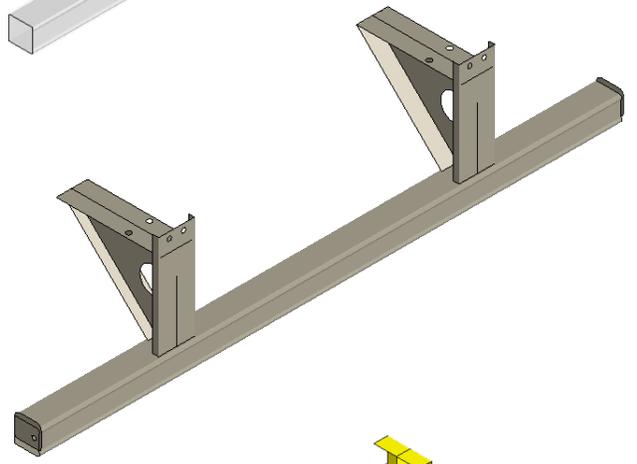
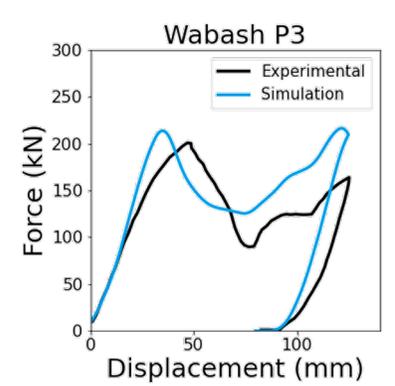
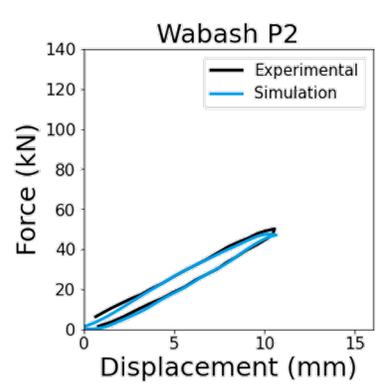
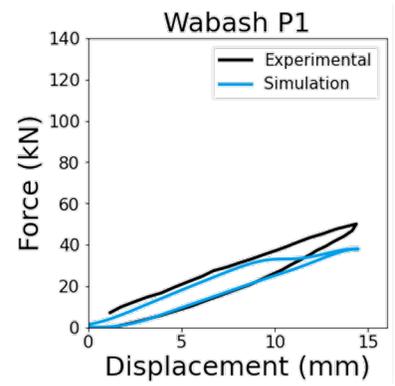
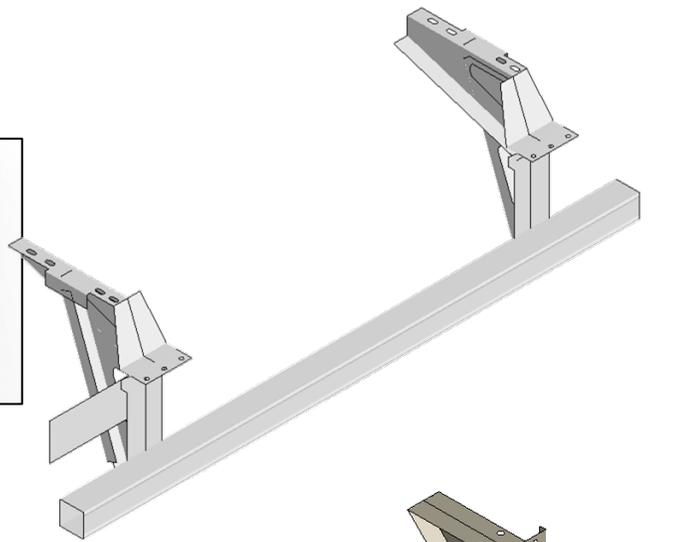
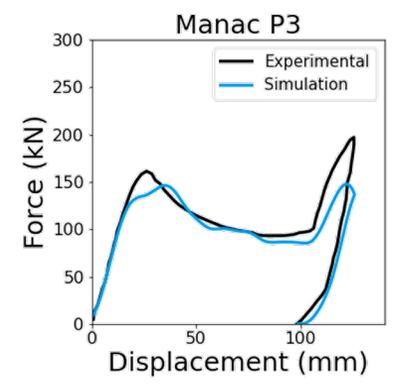
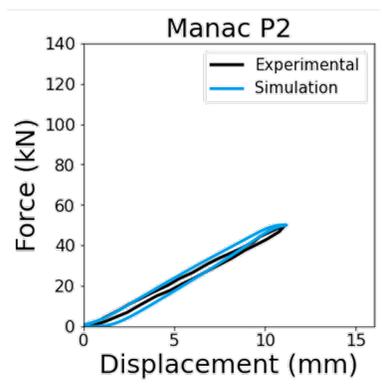
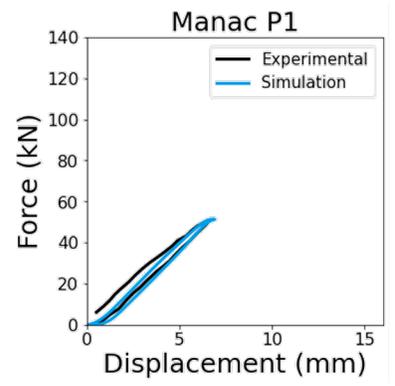
- Meets FMVSS 223 and report is available
- Has been tested in IIHS full vehicle crash tests
- Prevalent on US roadways
- Still available new from manufacturer

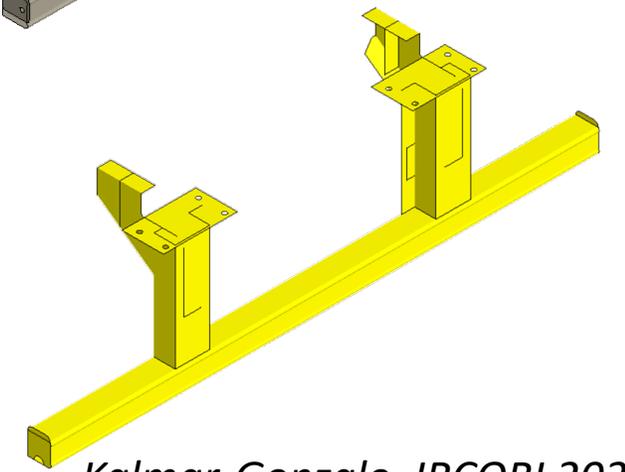
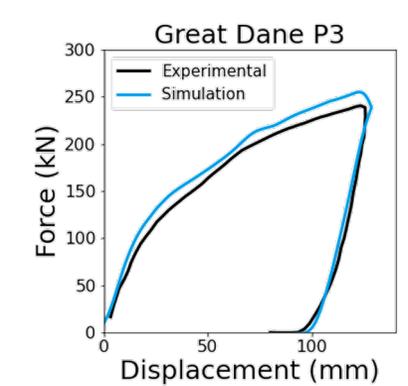
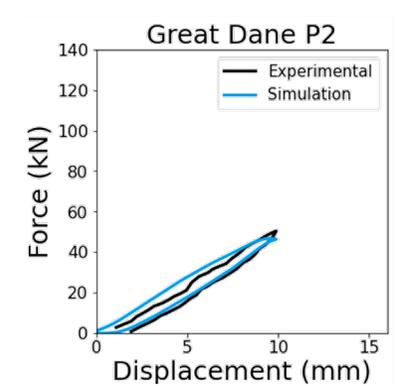
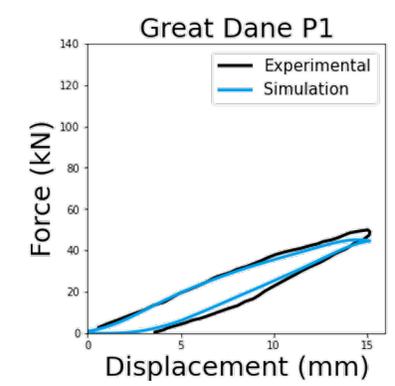
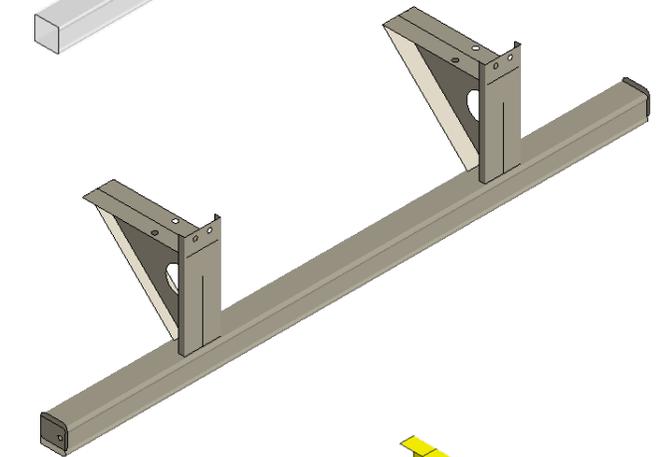
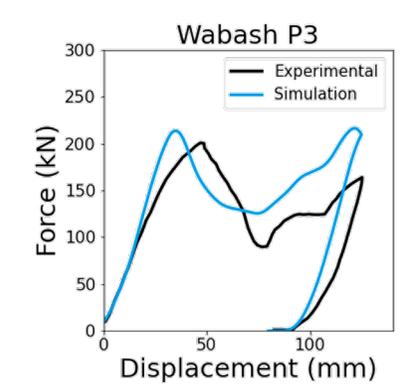
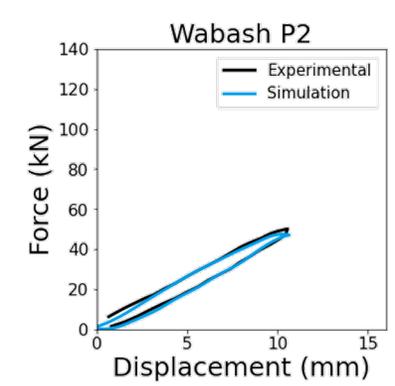
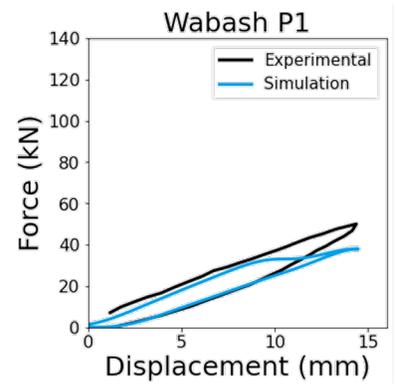
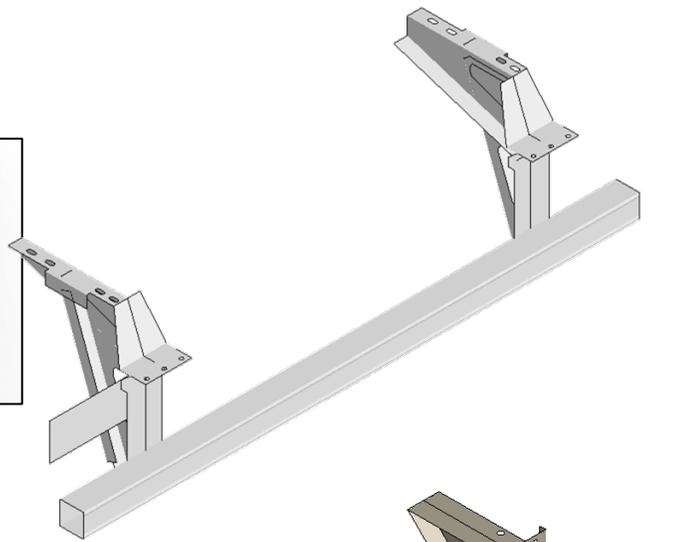
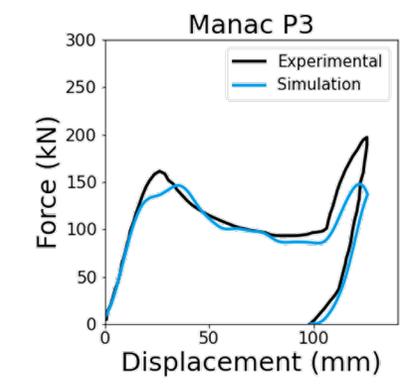
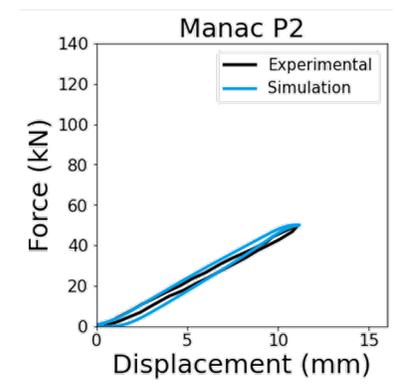
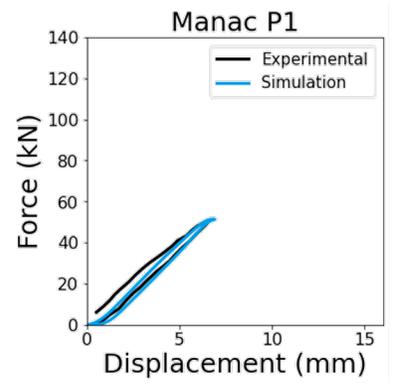


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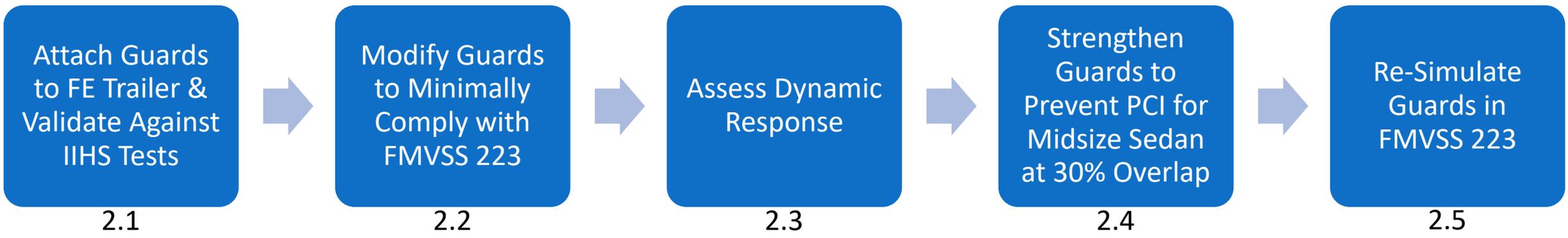




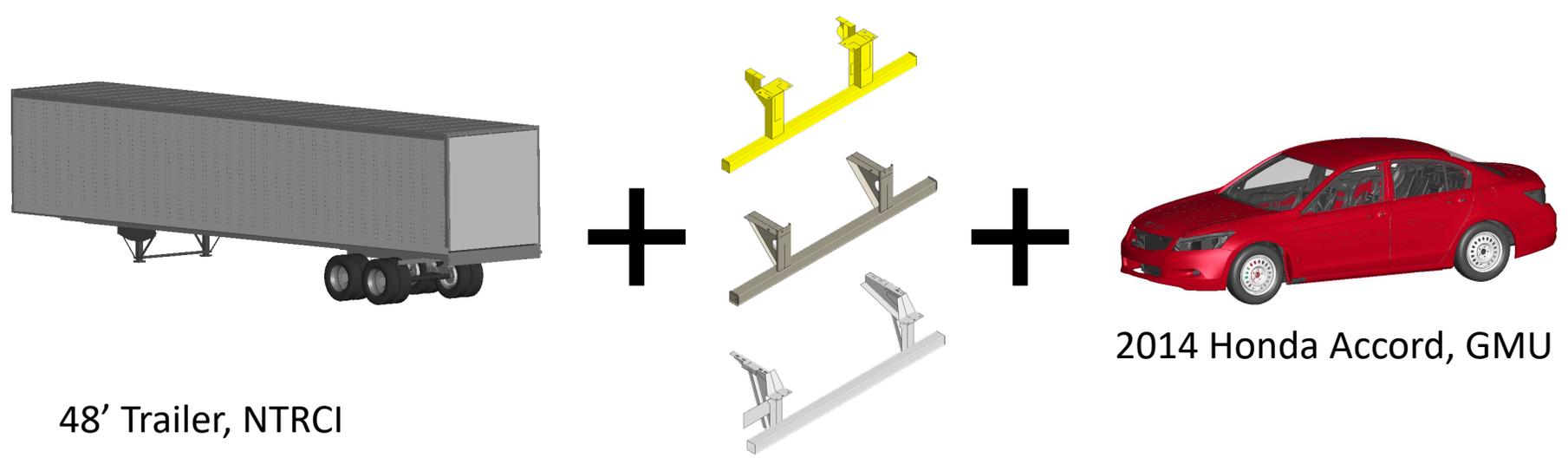
Average CORA Score = 0.942

Study Goal: Examine the relationship between quasi-static rear impact guard requirements and dynamic crash structural performance, including occupant response

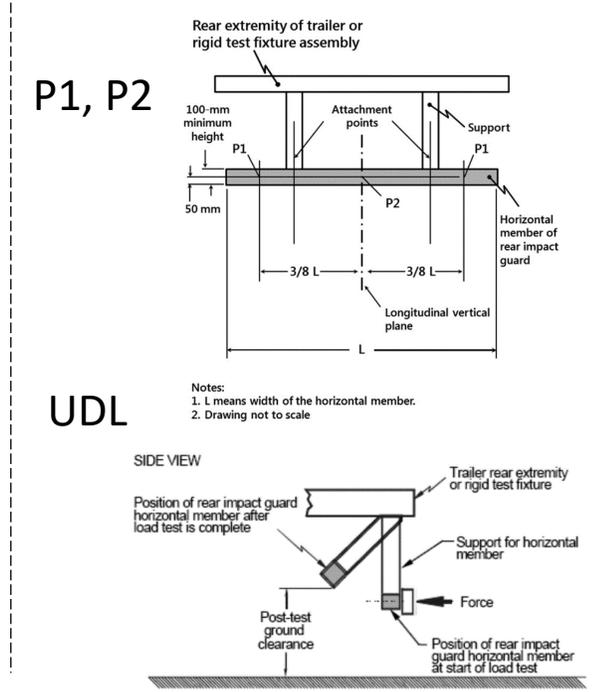
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Dynamic Simulations

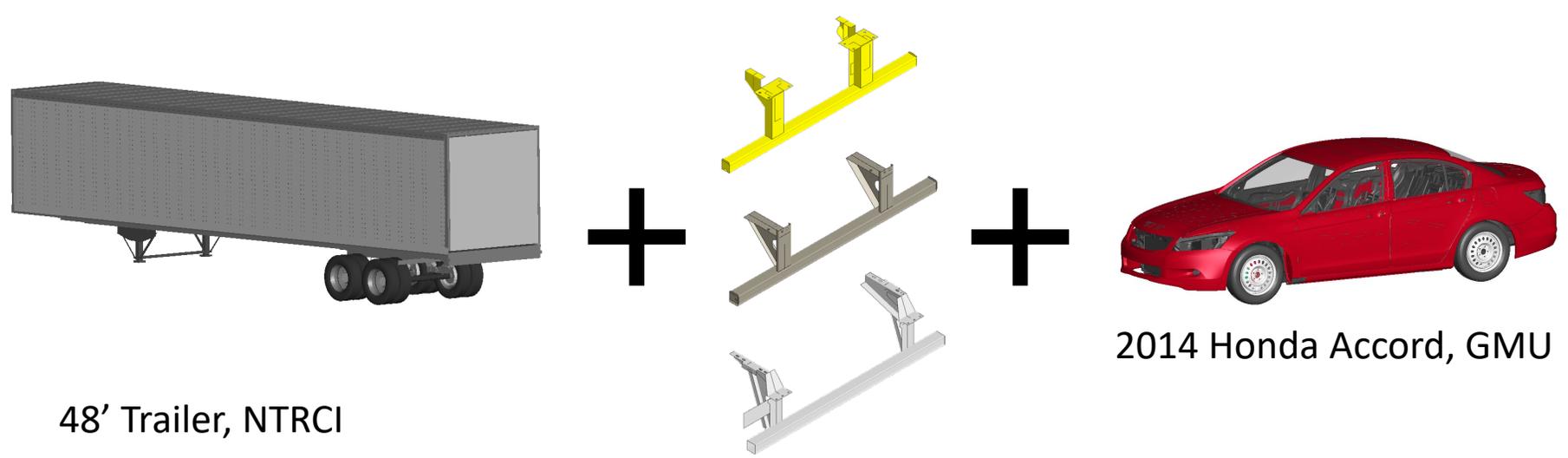


Quasi-Static Simulations

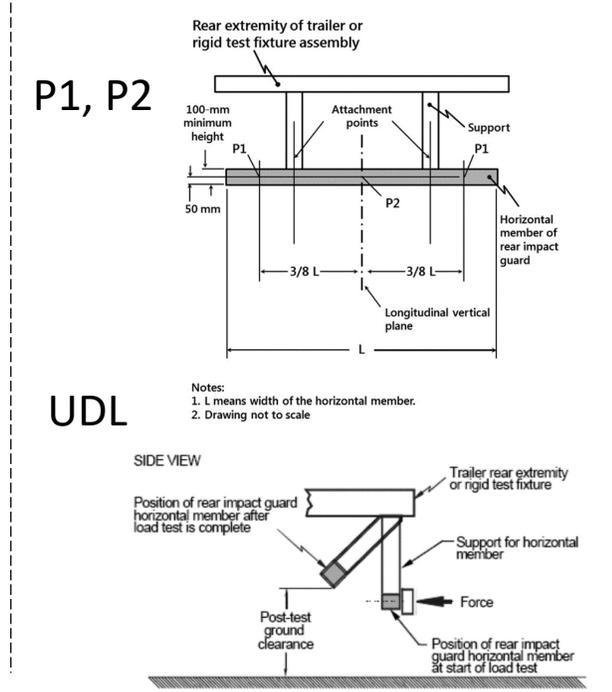


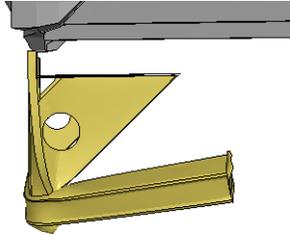


Dynamic Simulations

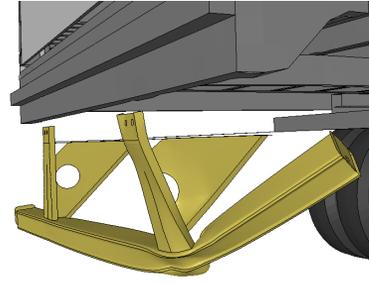


Quasi-Static Simulations





30% Overlap



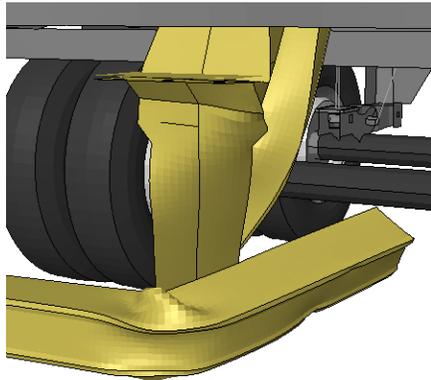
50% Overlap



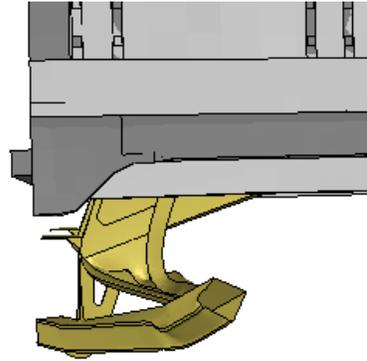
Full Overlap



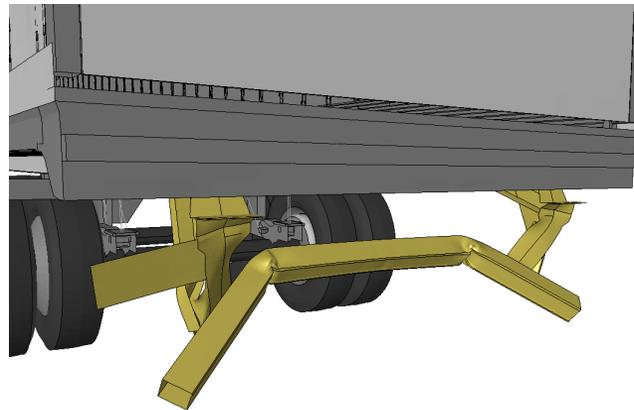
Full Overlap:
Physical vs Simulation



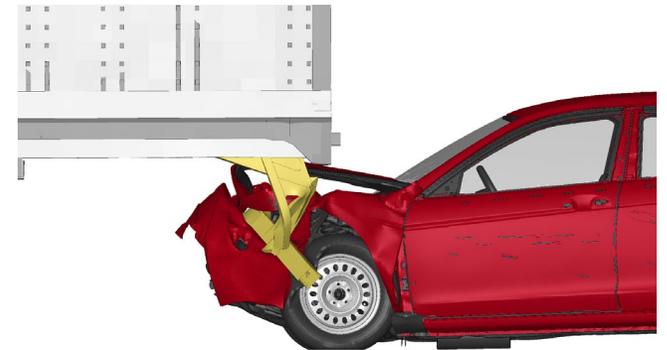
30% Overlap



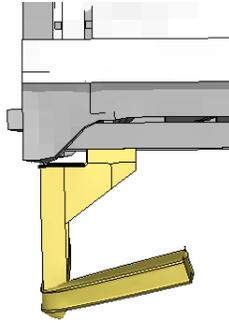
50% Overlap



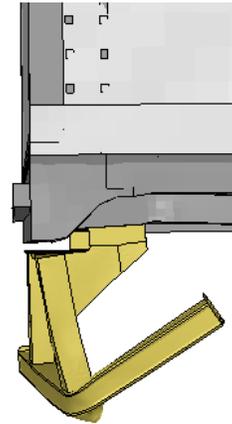
Full Overlap



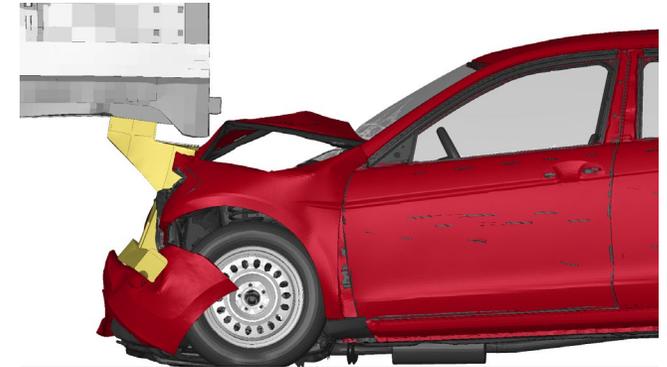
Full Overlap:
Physical vs Simulation



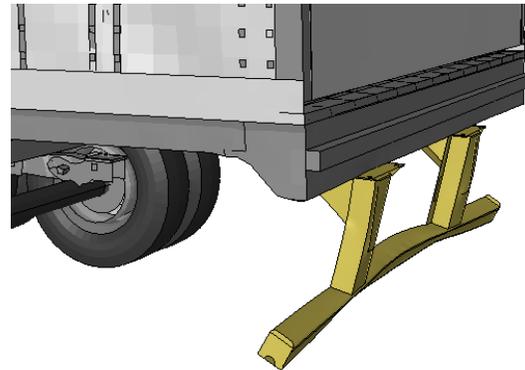
30% Overlap



50% Overlap



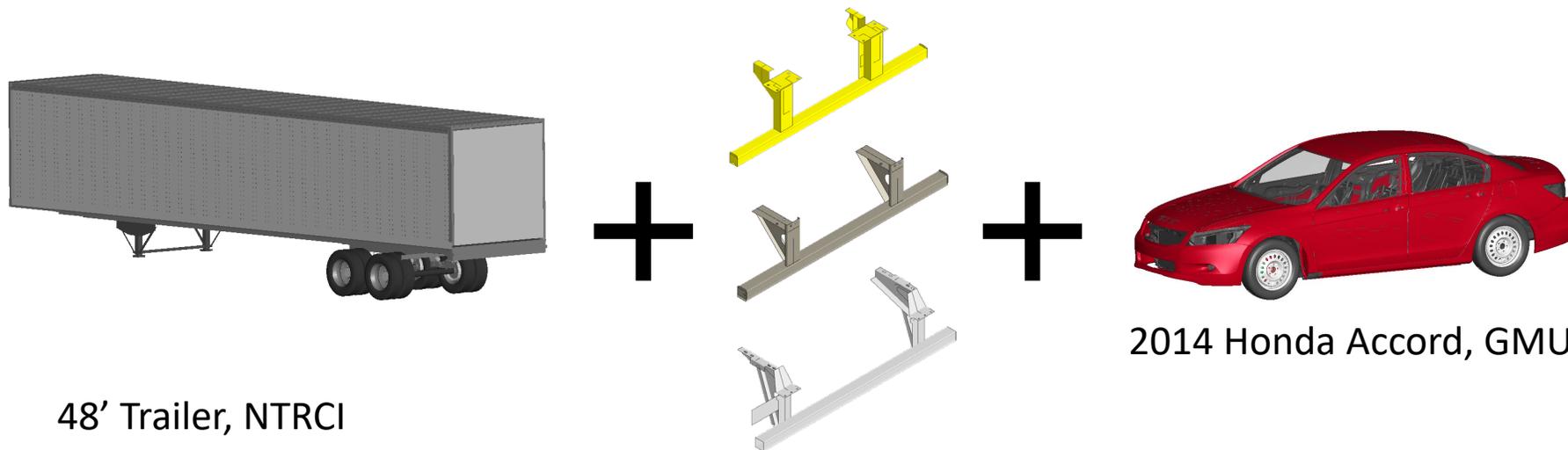
Full Overlap:
Physical vs Simulation



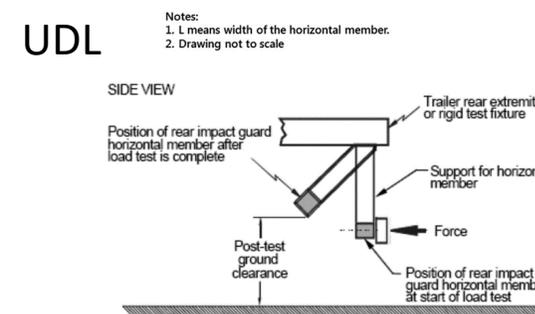
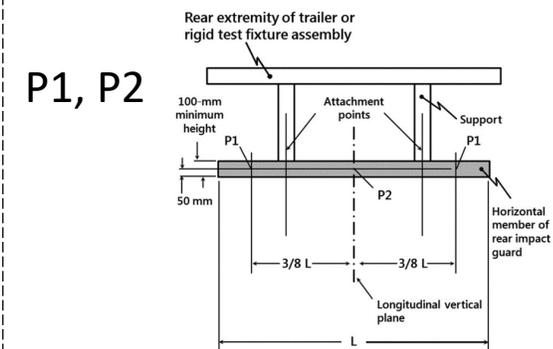
Full Overlap



Dynamic Simulations

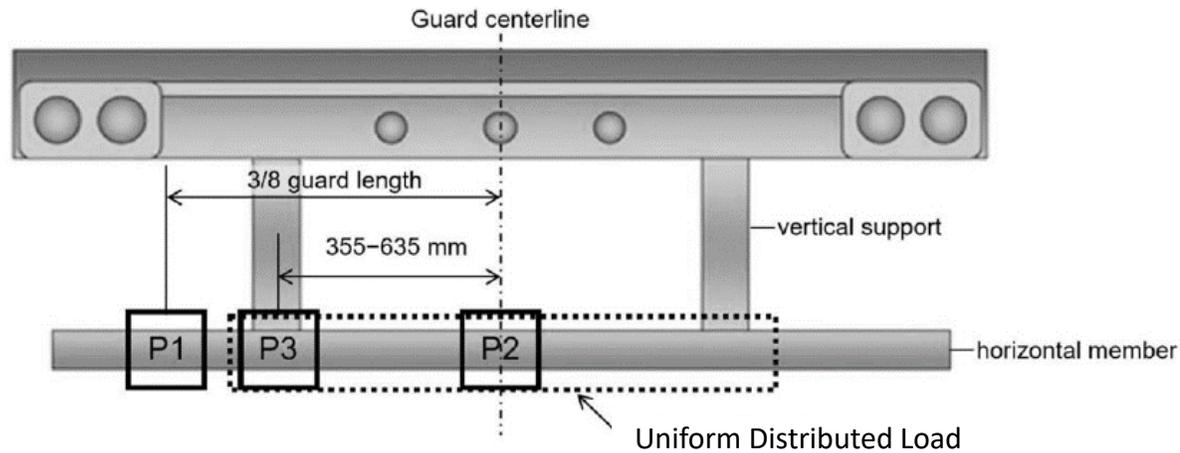


Quasi-Static Simulations



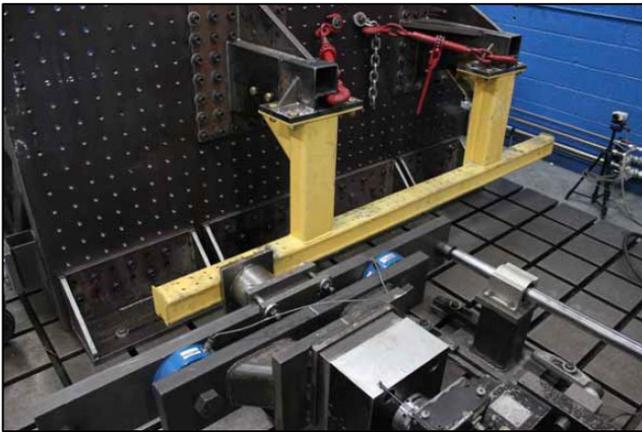


Aim 2.2: Modify Guards to minimally comply with FMVSS 223



FMVSS No. 223 (2022):

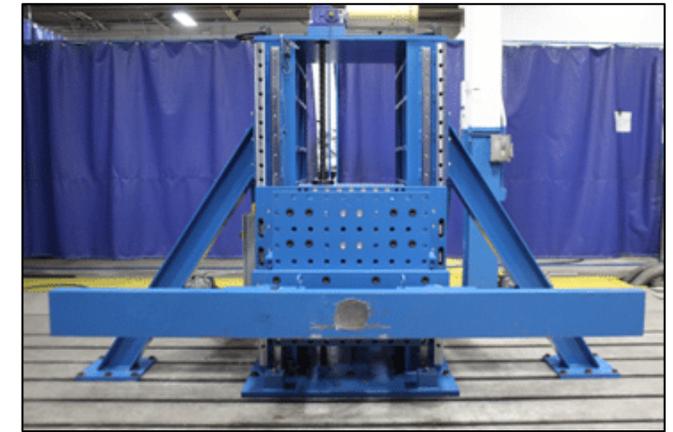
- P1, P2 must resist 50 kN before 125 mm
- UDL must resist 350 kN before 125mm & absorb 20 kJ of energy through plastic deformation
- Final Ground Clearance ≤ 22 in



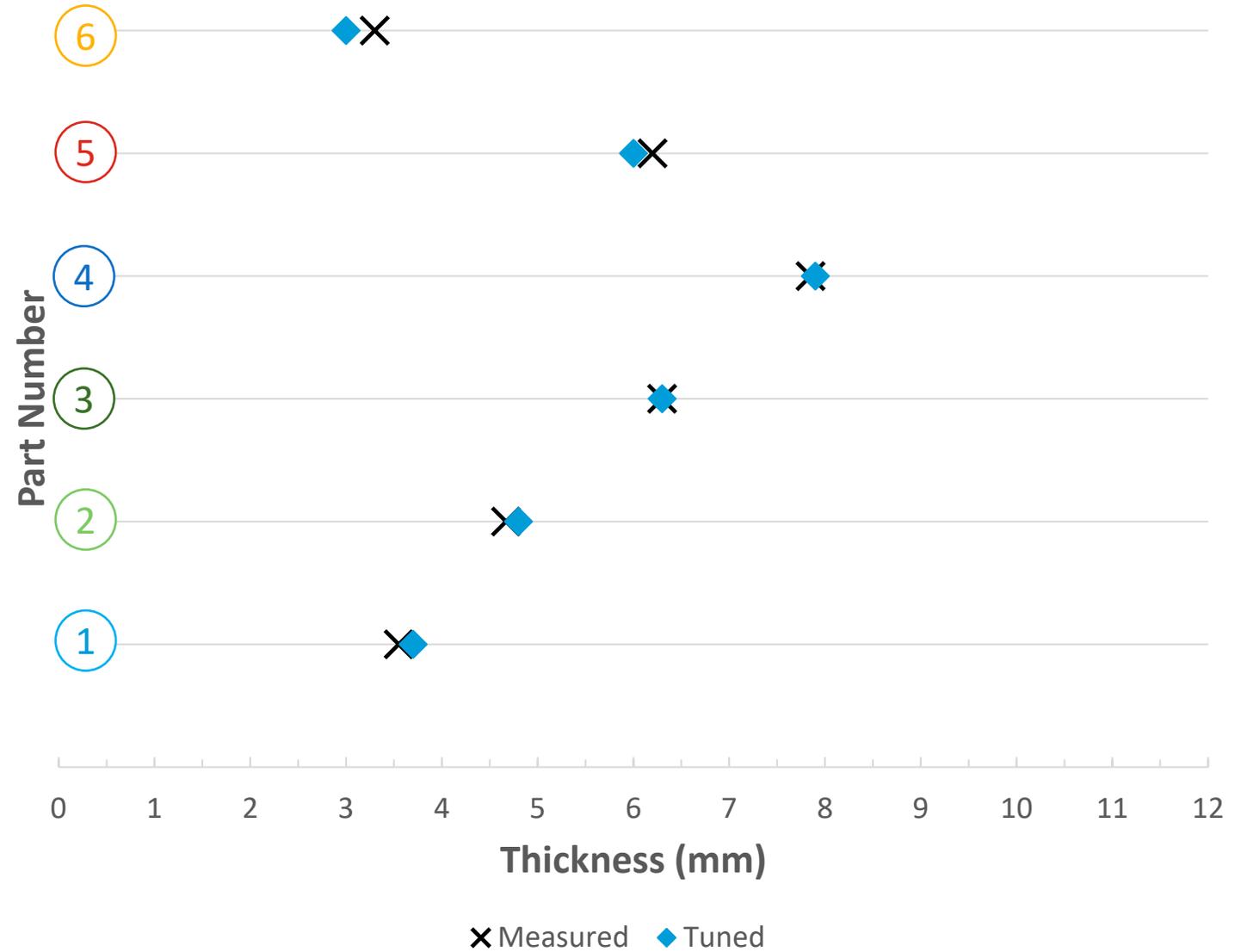
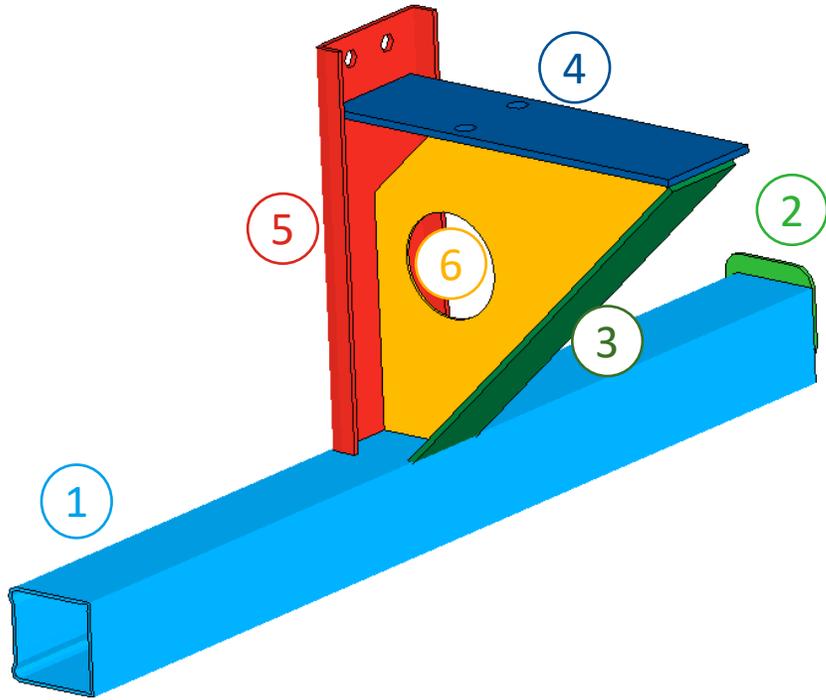
P1

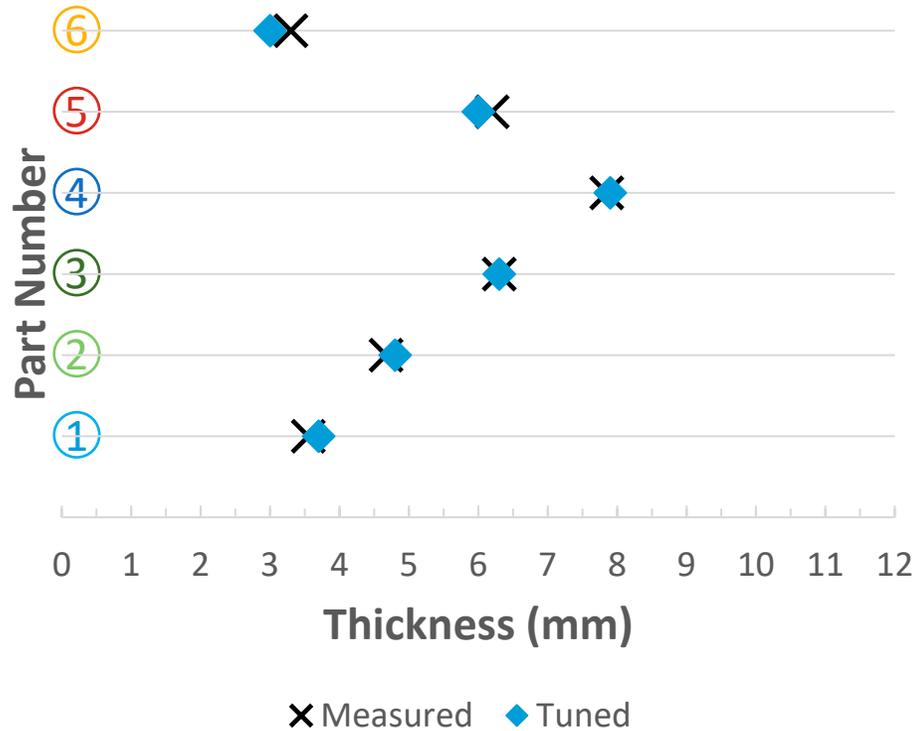
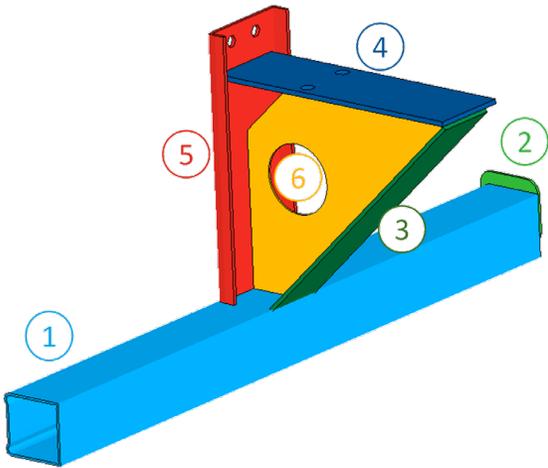


P2

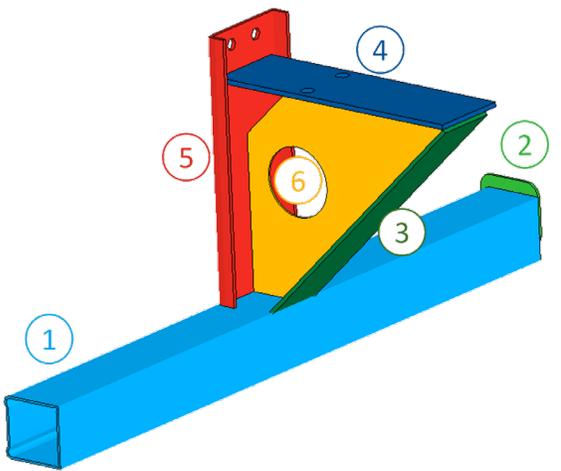


UDL

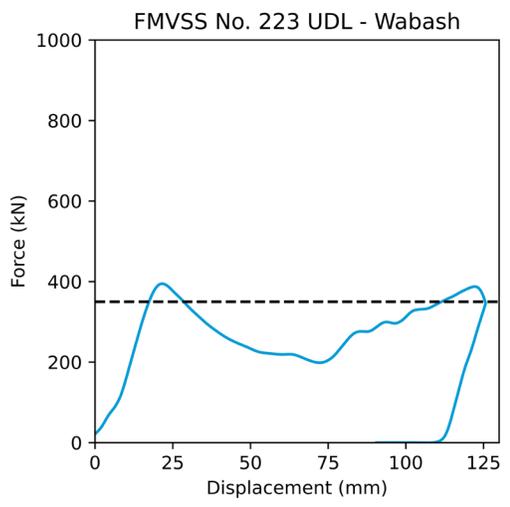
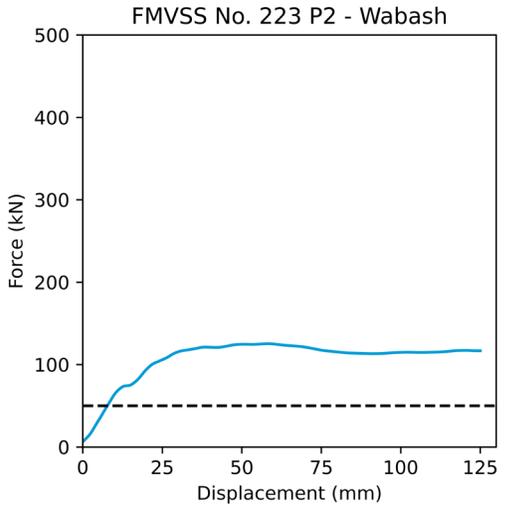
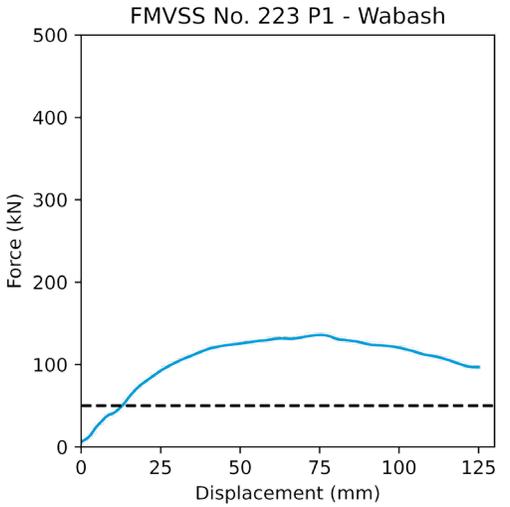
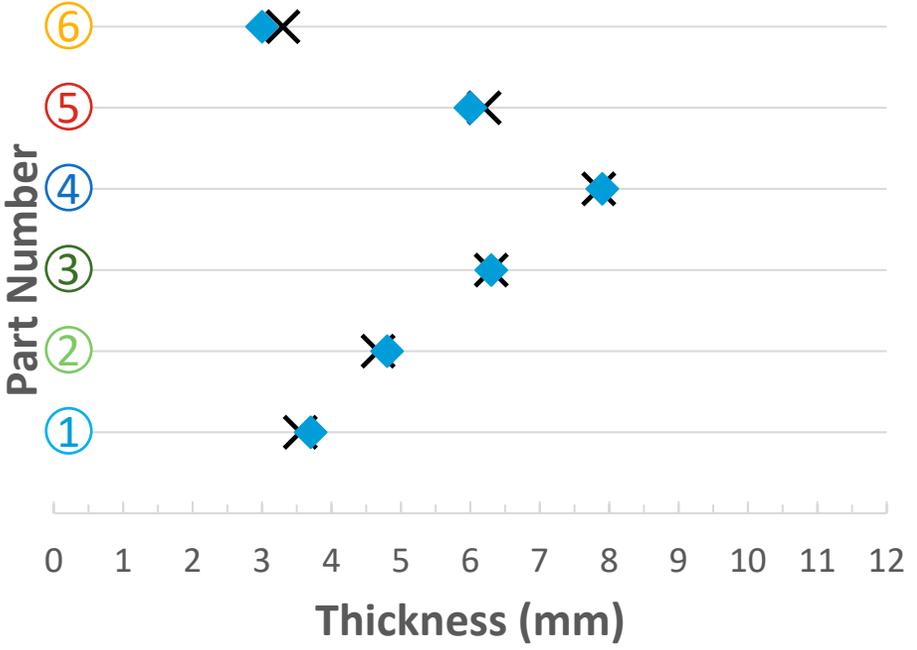




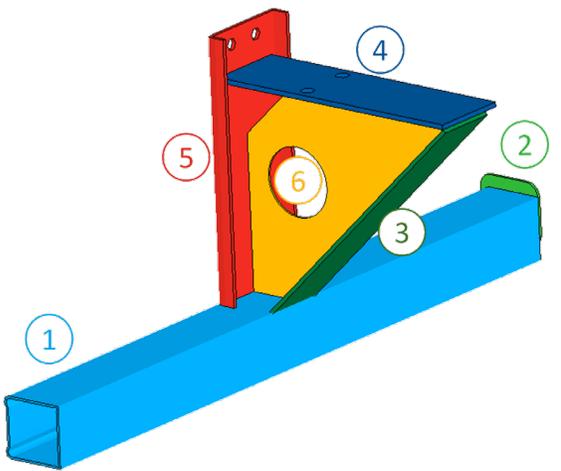
Wabash	Quasi-Static Response				Mass (kg)
	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Baseline					
Minimally Compliant					
FMVSS Req.	≥50	≥50	≥350	≥20	N/A



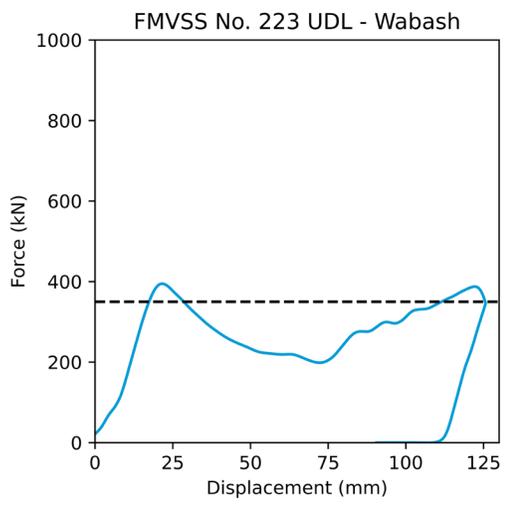
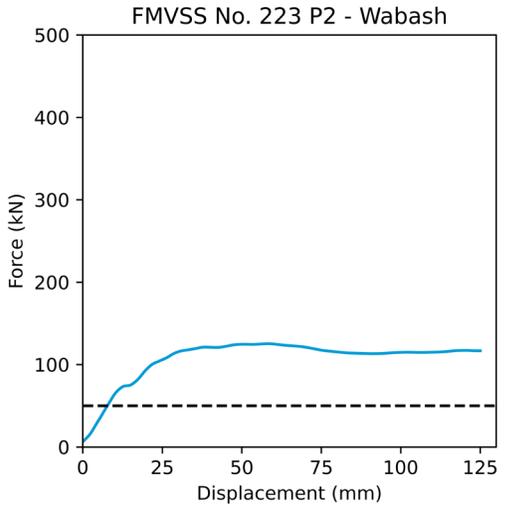
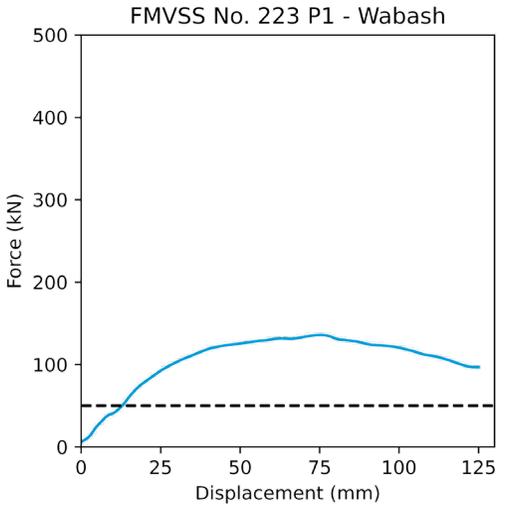
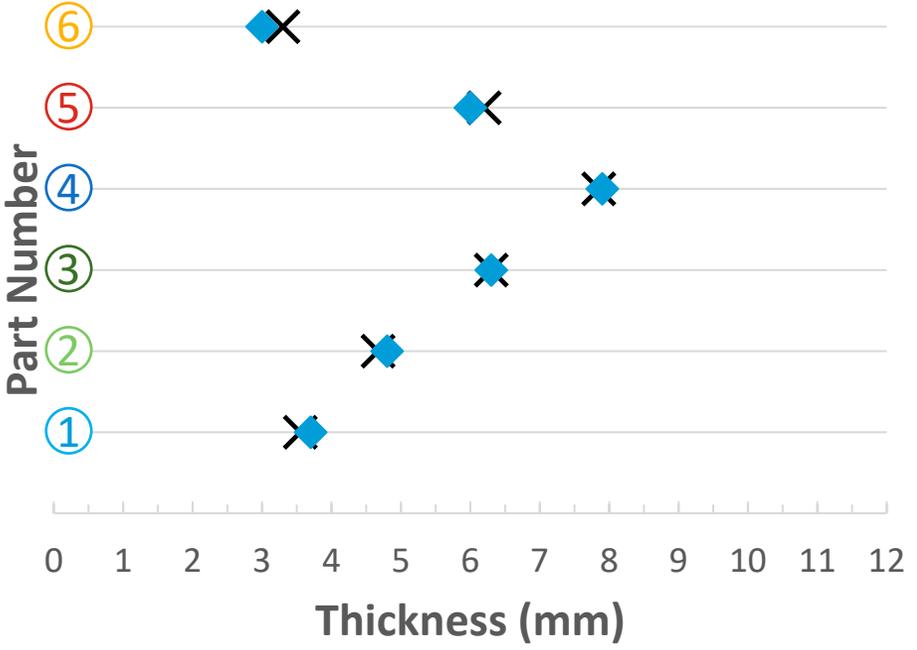
Wabash	Quasi-Static Response				Mass (kg)
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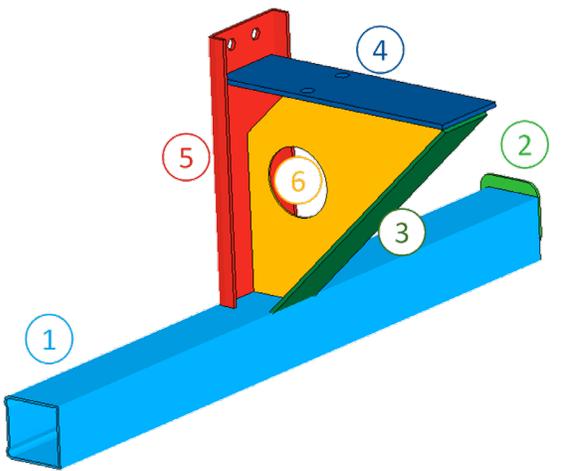
✕ Measured ♦ Tuned



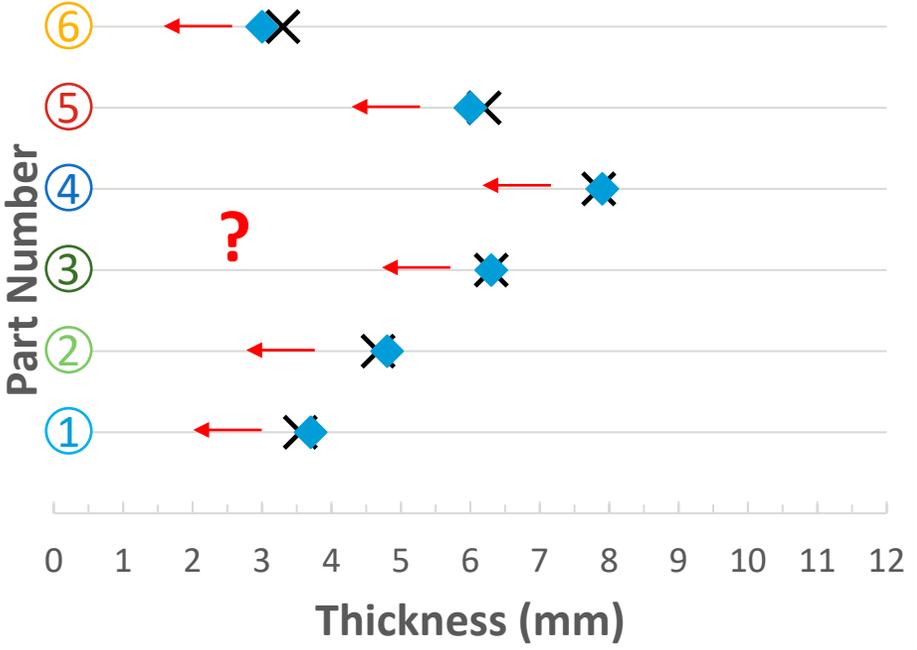
Wabash	Quasi-Static Response				Mass (kg)
	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Baseline	135.8	125.4	394.7	32.1	54.4
Minimally Compliant					
FMVSS Req.	≥50	≥50	≥350	≥20	N/A



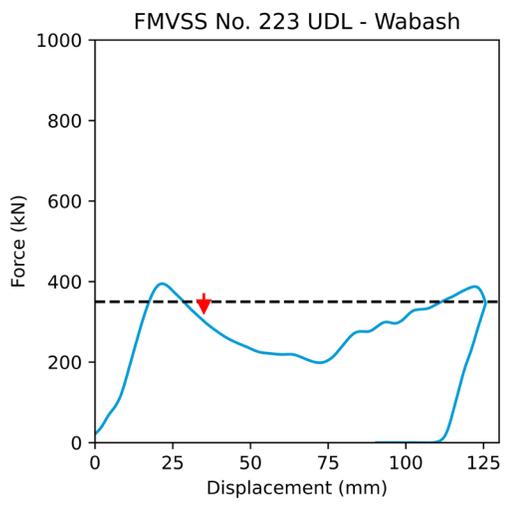
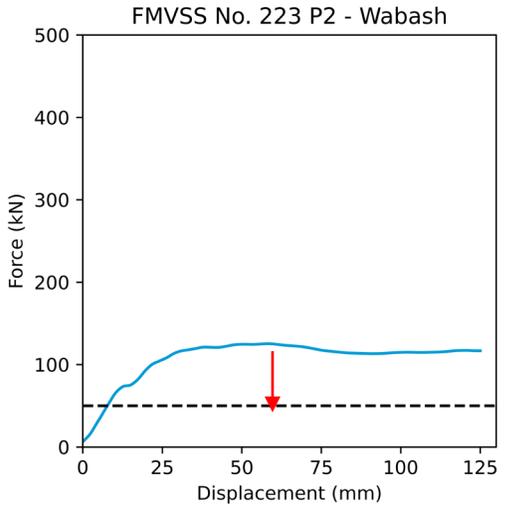
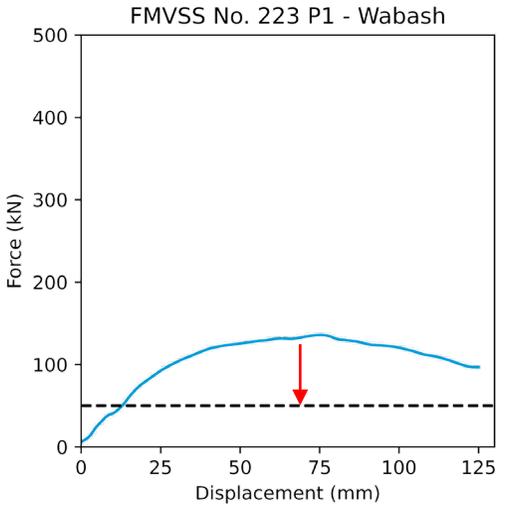
✕ Measured ◆ Tuned



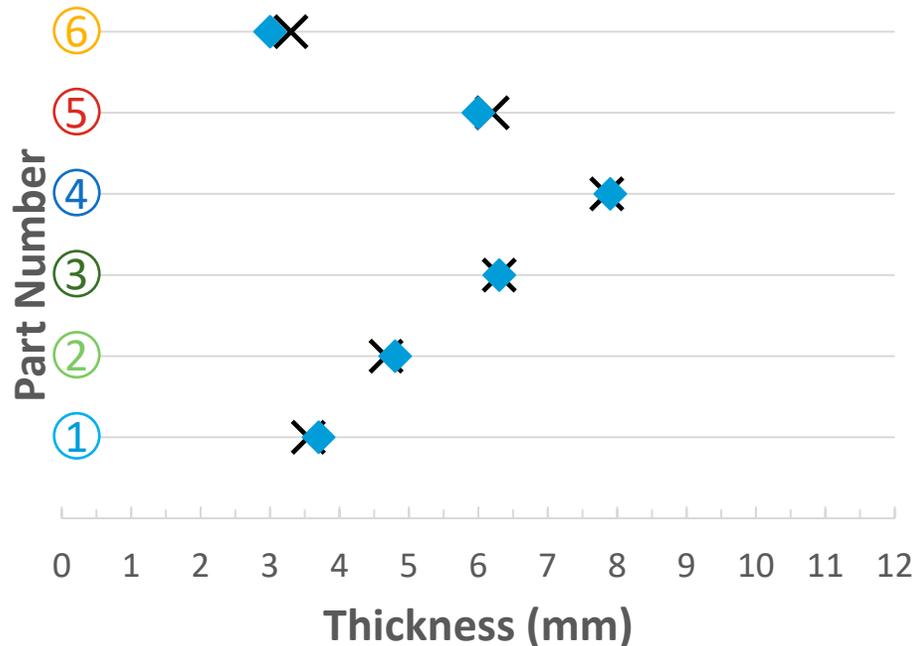
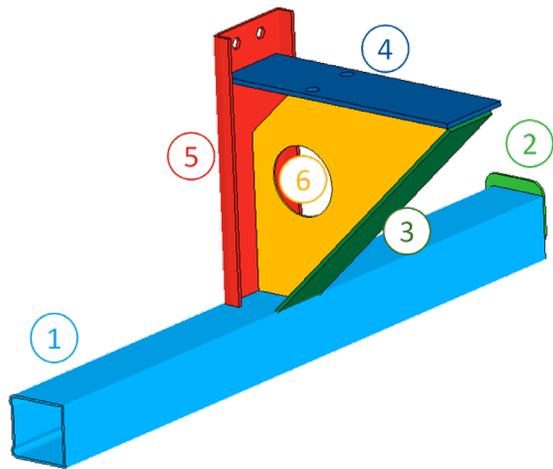
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Minimally Compliant					
FMVSS Req.	≥50	≥50	≥350	≥20	N/A



✕ Measured ◆ Tuned



What is the minimum thickness that still passes FMVSS No. 223?

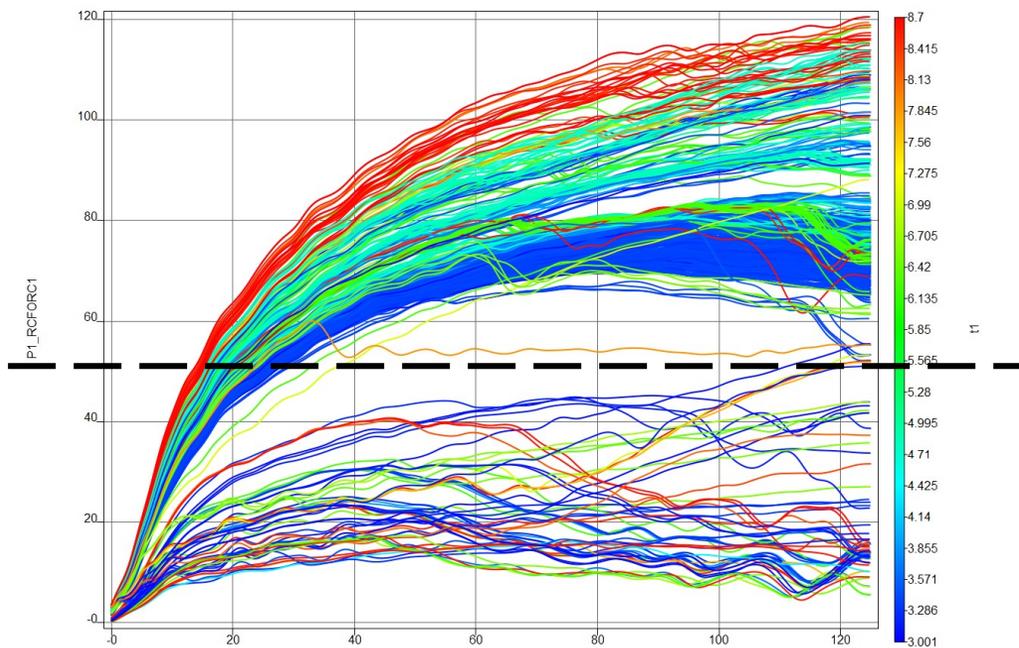


✕ Measured ♦ Tuned

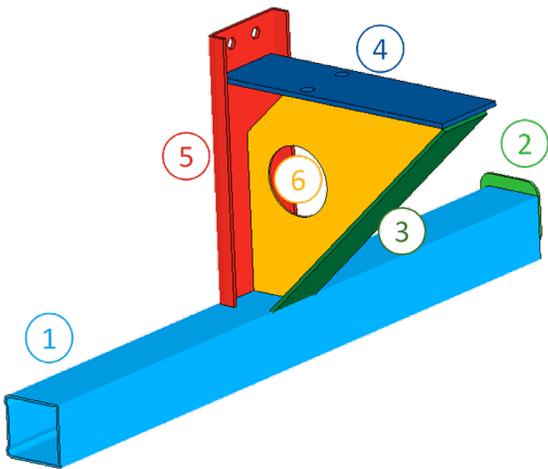
Modified guards using LS-OPT

- Each part thickness independently modified
- Considered P1, P2, UDL
- Small weighting factor on mass of guard

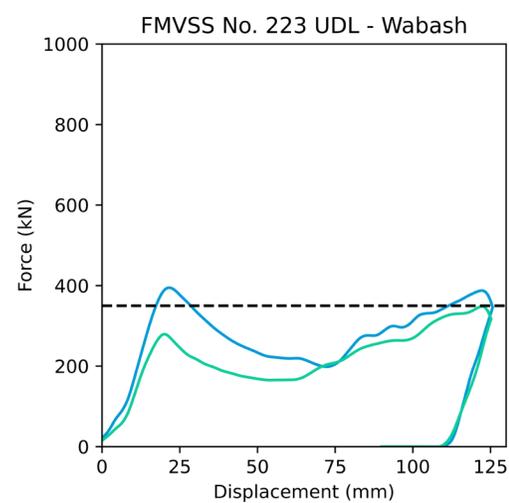
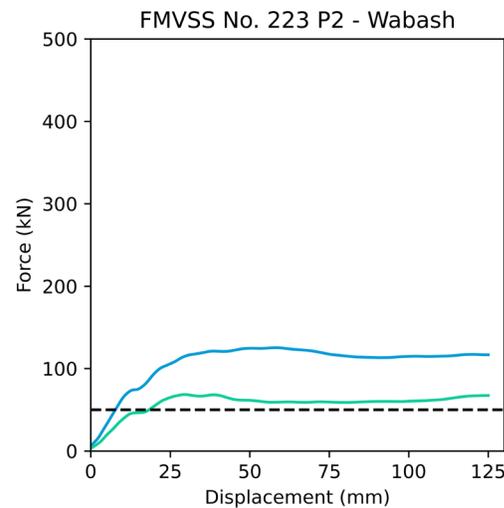
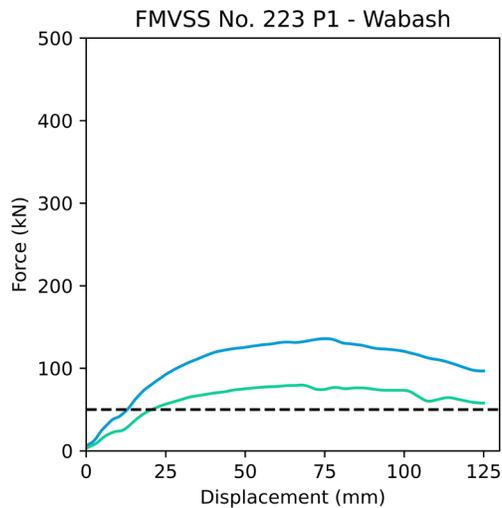
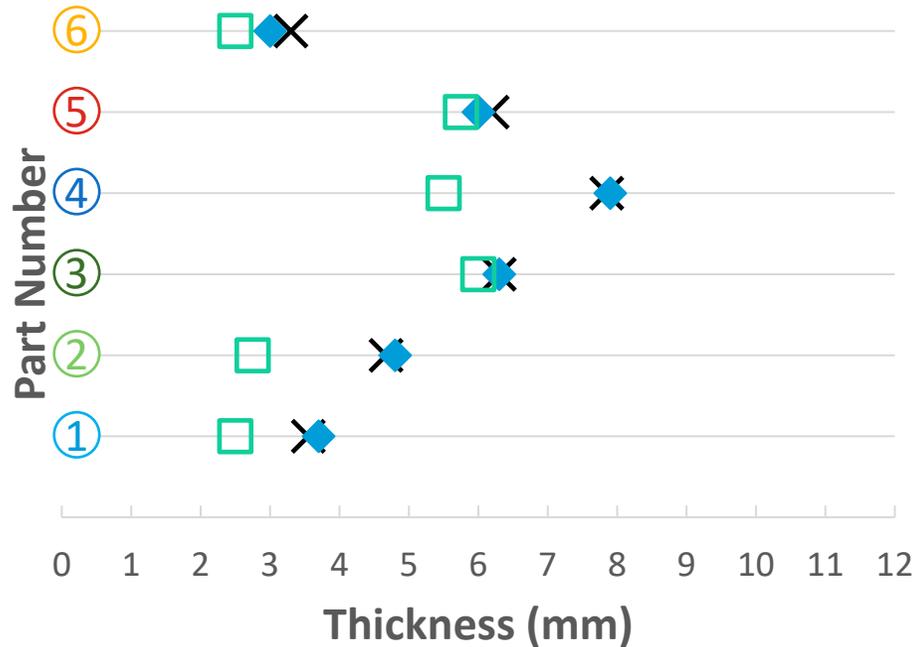
FMVSS Req.



What is the minimum thickness that still passes FMVSS No. 223?



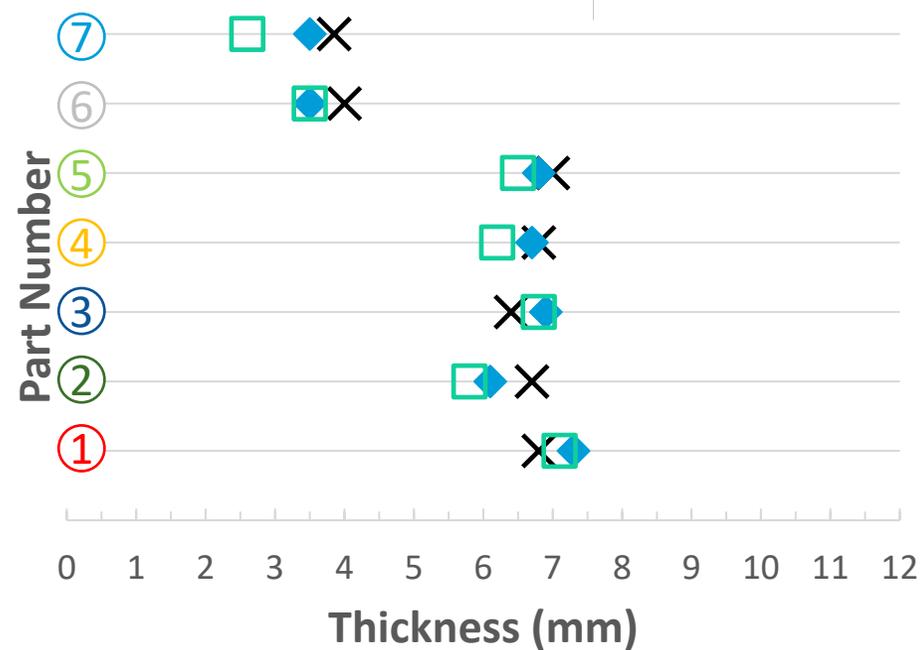
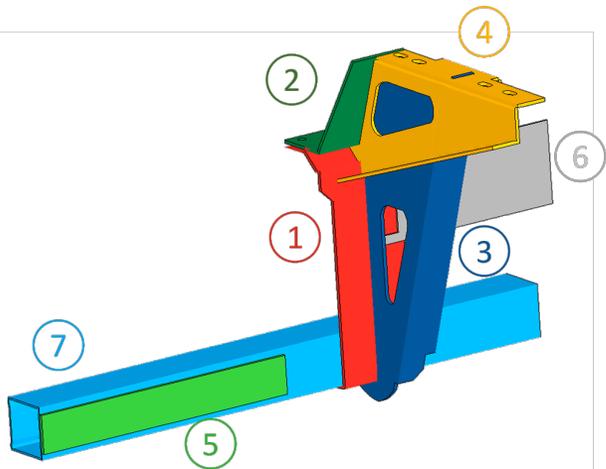
Wabash	Quasi-Static Response				Mass (kg)
	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Baseline	135.8	125.4	394.7	32.1	54.4
Minimally Compliant	79.6	68.5	350.4	25.6	38.9
FMVSS Req.	≥50	≥50	≥350	≥20	N/A



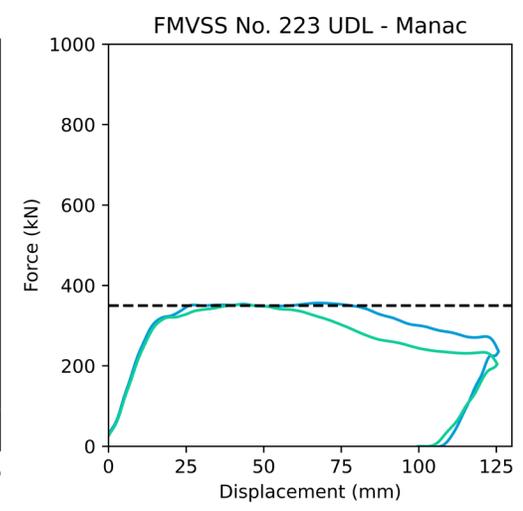
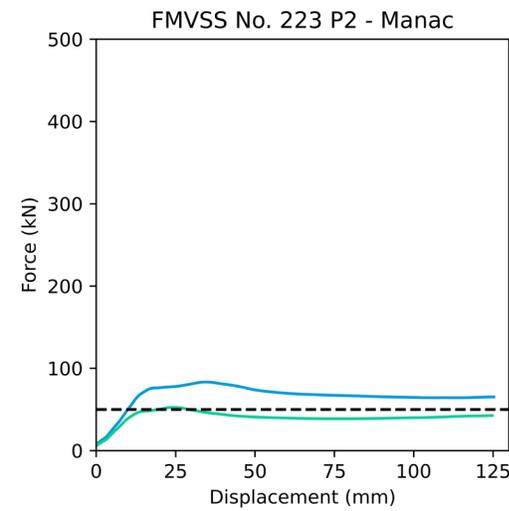
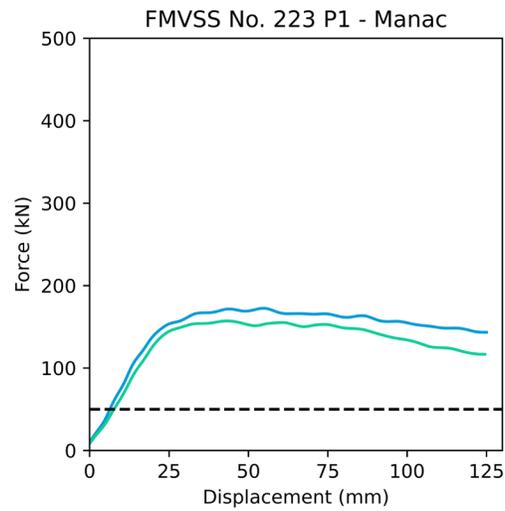
X Measured ♦ Tuned □ Minimally Compliant



Aim 2.2: Modify Guards to minimally comply with FMVSS 223 : Manac



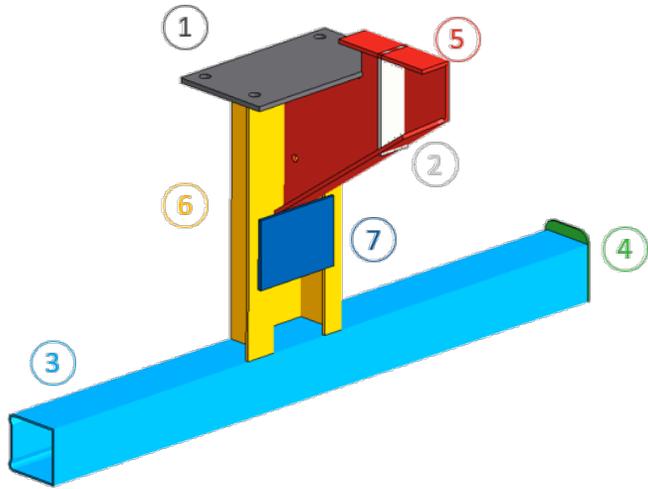
Wabash	Quasi-Static Response				Mass (kg)
	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Baseline	172.5	83.3	356.2	36.8	84.8
Minimally Compliant	157.1	52.5	351.9	33.3	75.7
FMVSS Req.	≥50	≥50	≥350	≥20	N/A



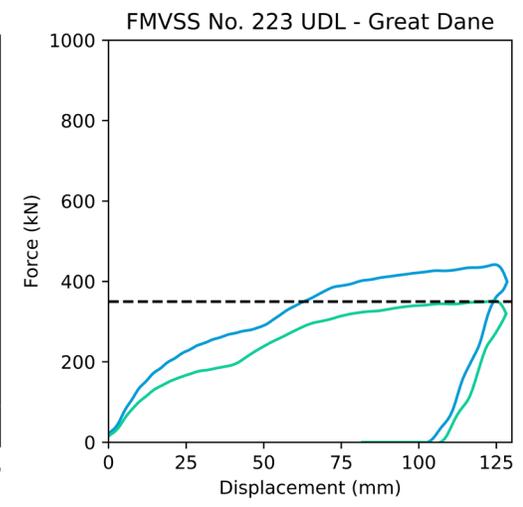
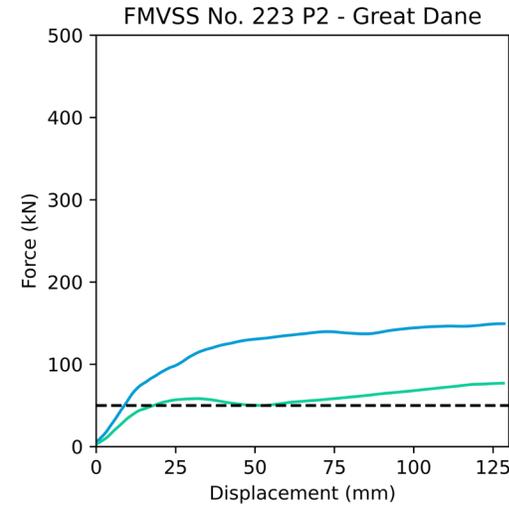
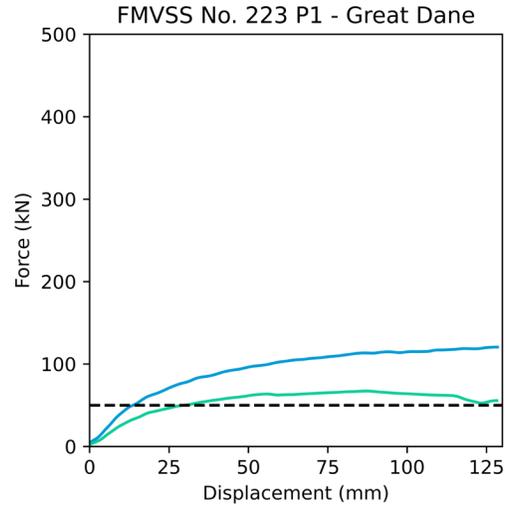
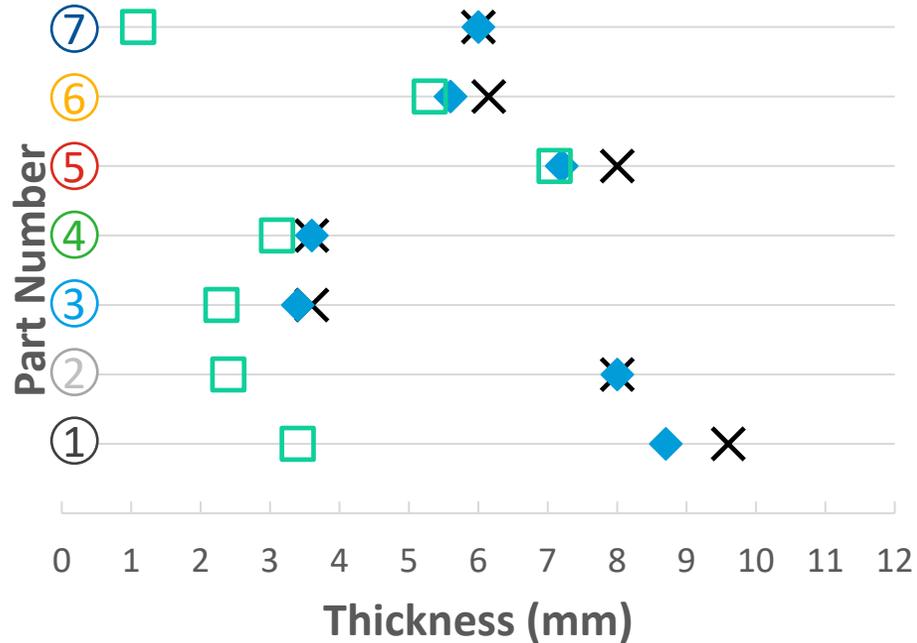
✕ Measured ◆ Tuned ◻ Minimally Compliant



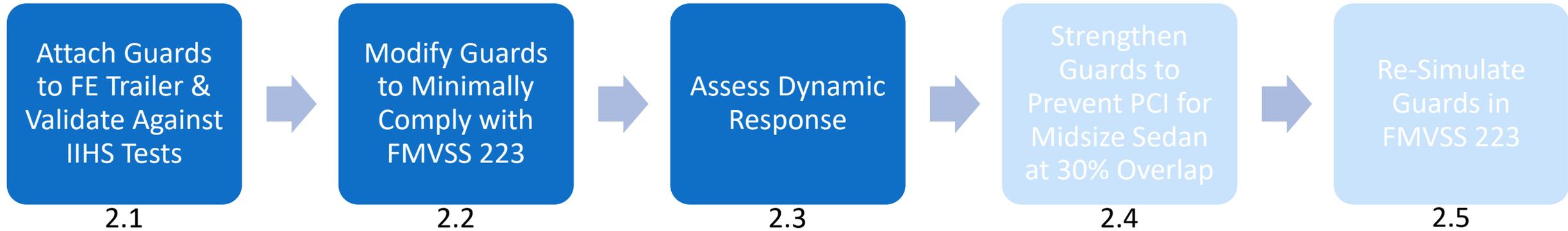
Aim 2.2: Modify Guards to minimally comply with FMVSS 223 : Great Dane



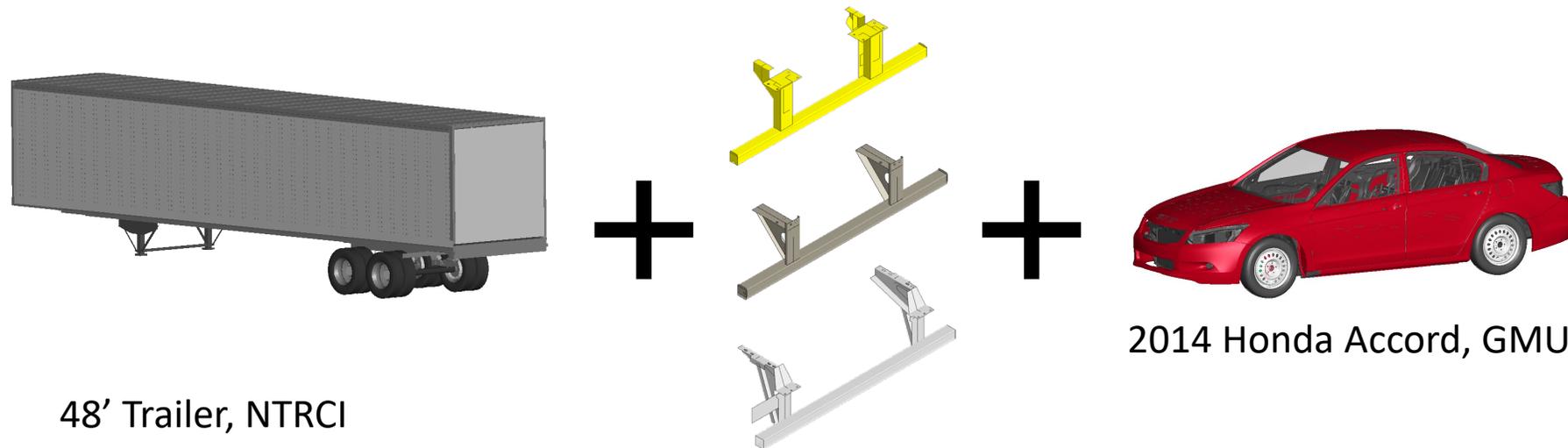
Wabash	Quasi-Static Response				Mass (kg)
	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Baseline	120.5	149.4	441.7	36.6	69.4
Minimally Compliant	67.2	77.0	350.4	29.4	52.5
FMVSS Req.	≥50	≥50	≥350	≥20	N/A



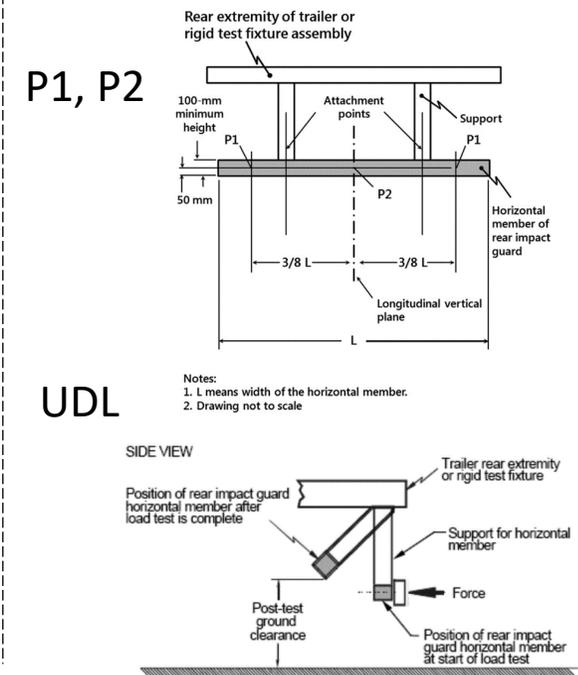
× Measured
 ◆ Tuned
 □ Minimally Compliant



Dynamic Simulations



Quasi-Static Simulations



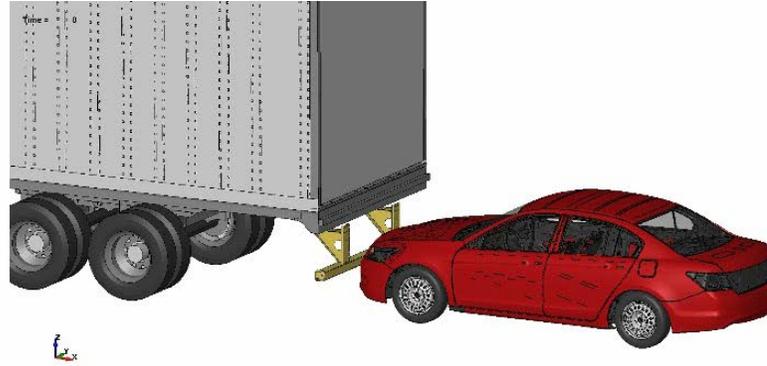
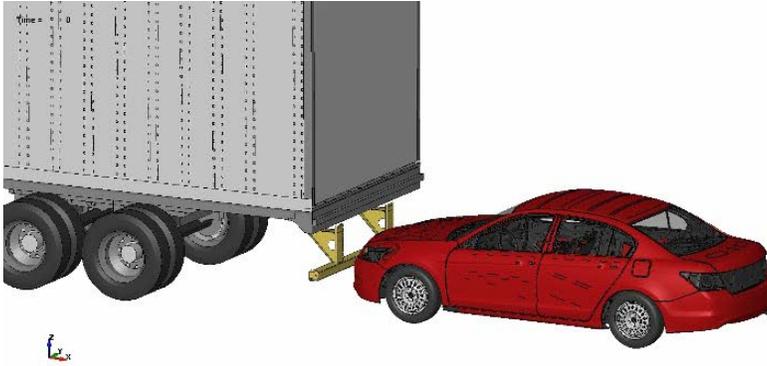


Aim 2.3: Assess Dynamic Response with Minimally Compliant Guards - Wabash

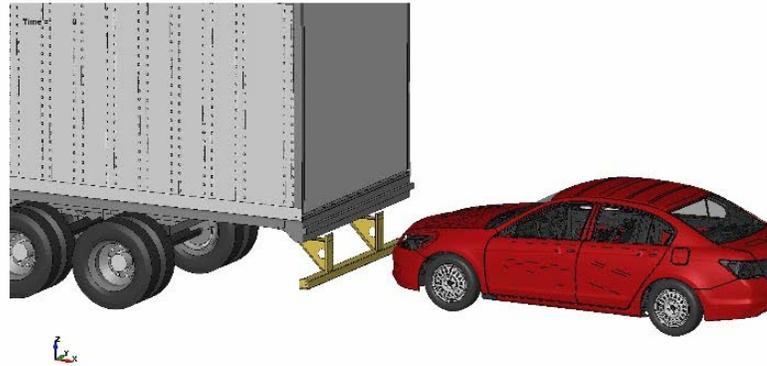
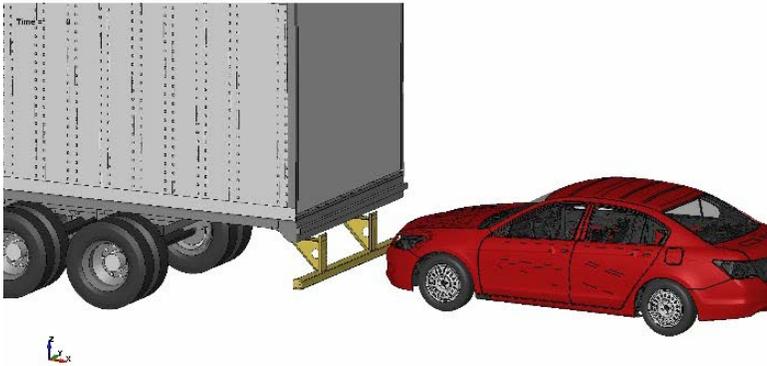
Baseline

Minimally Compliant

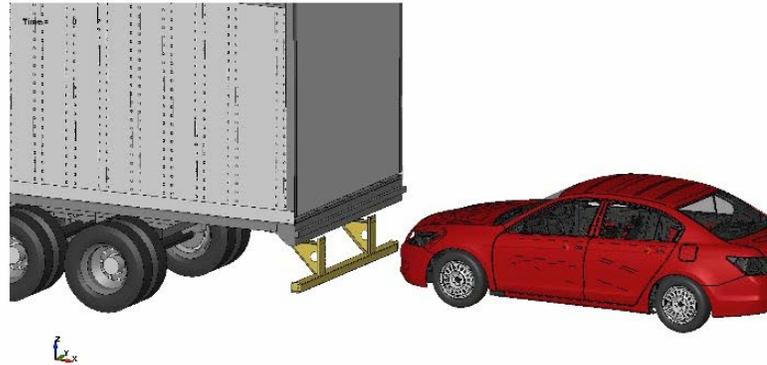
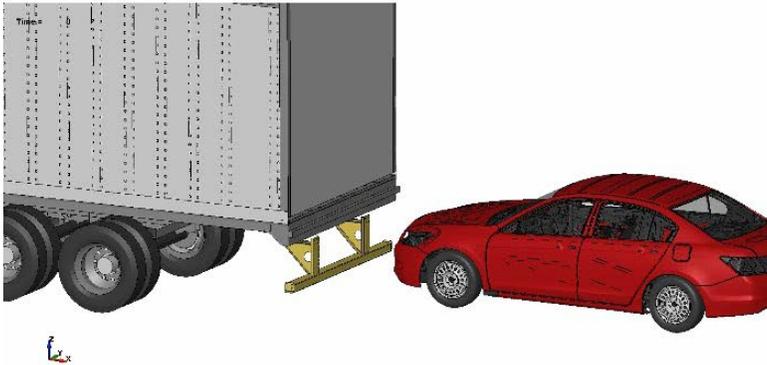
FW



50%



30%



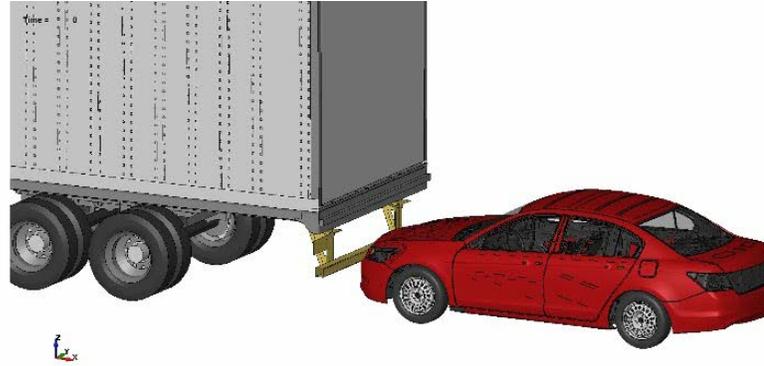
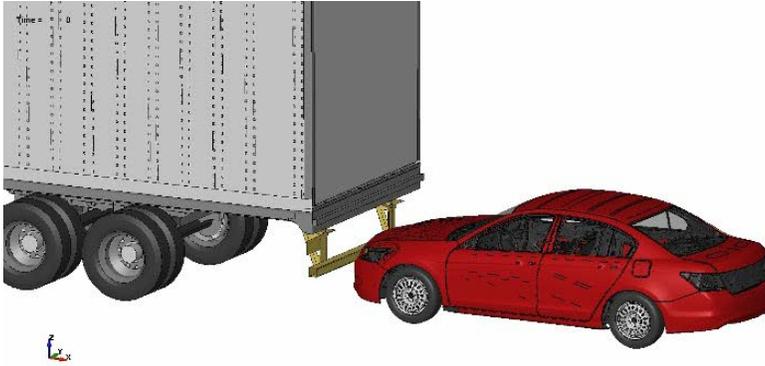
Wabash	Dynamic Response PCI Prevented?		
	FW	50%	30%
Baseline	Yes	Yes	No
Minimally Compliant	Yes	Yes	No



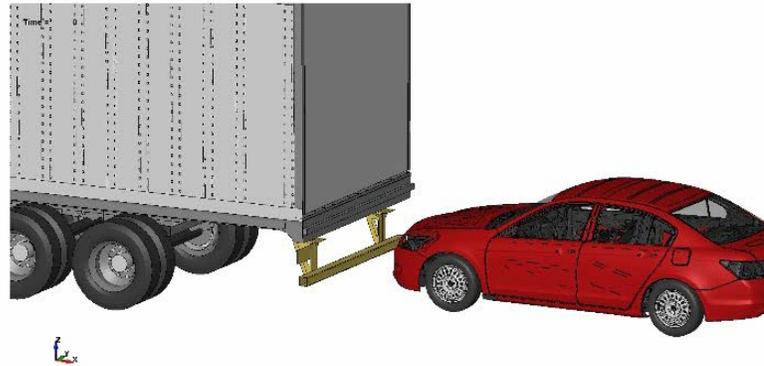
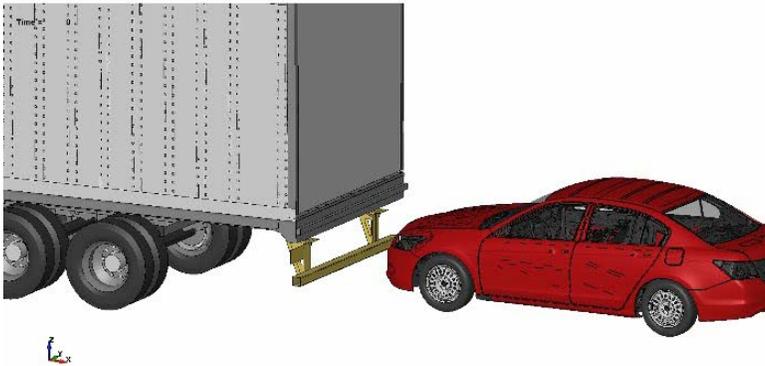
Baseline

Minimally Compliant

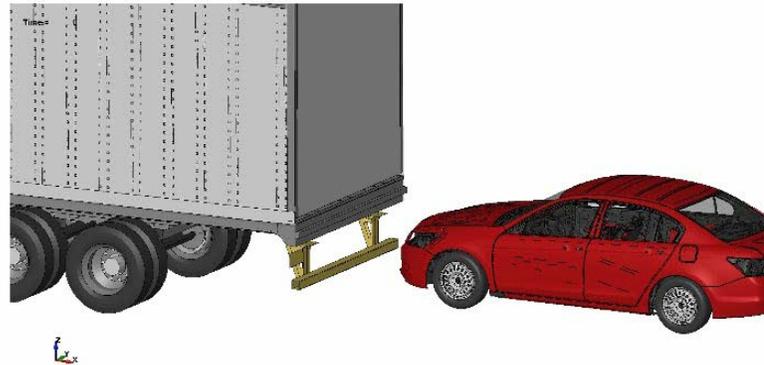
FW



50%



30%



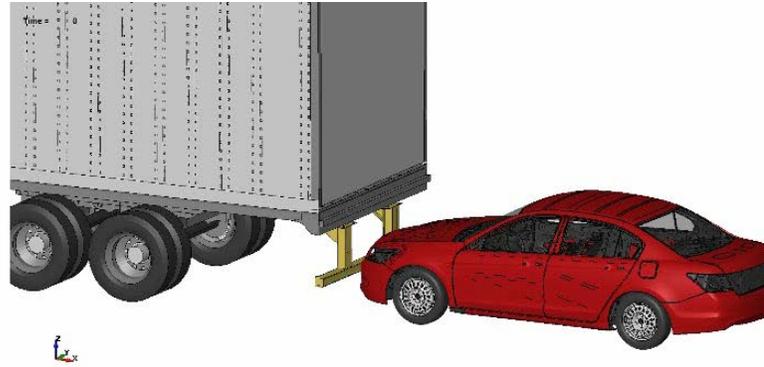
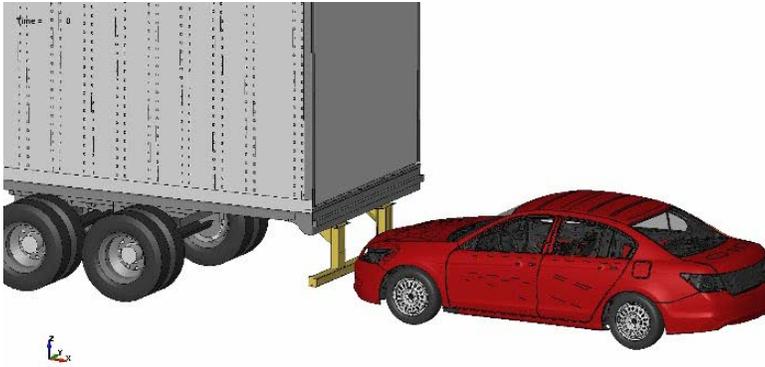
Manac	Dynamic Response PCI Prevented?		
	FW	50%	30%
Baseline	Yes	Yes	Yes
Minimally Compliant	Yes	Yes	Yes



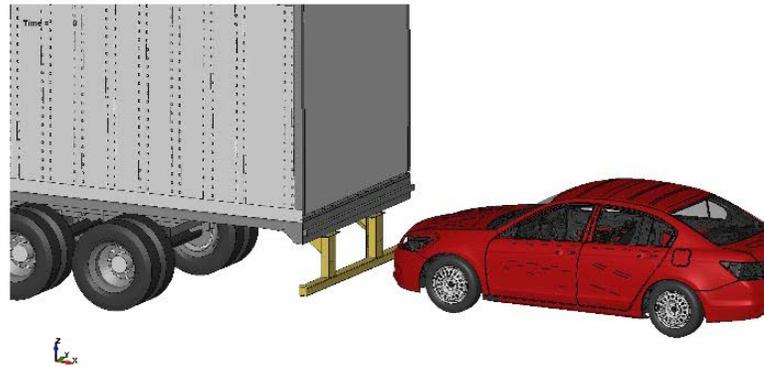
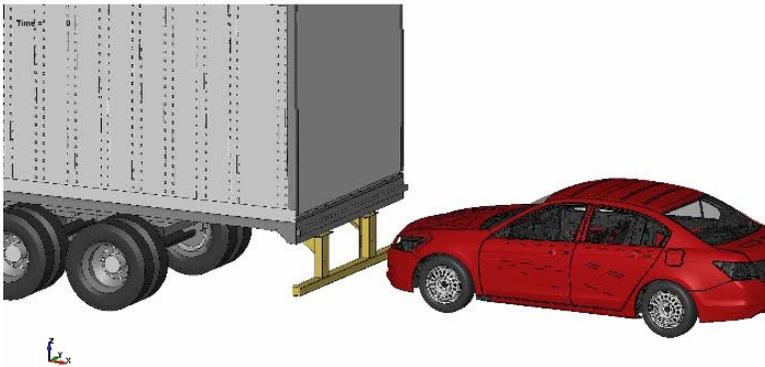
Baseline

Minimally Compliant

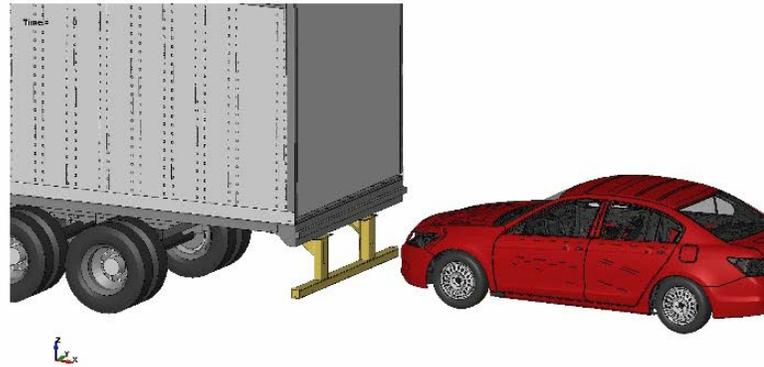
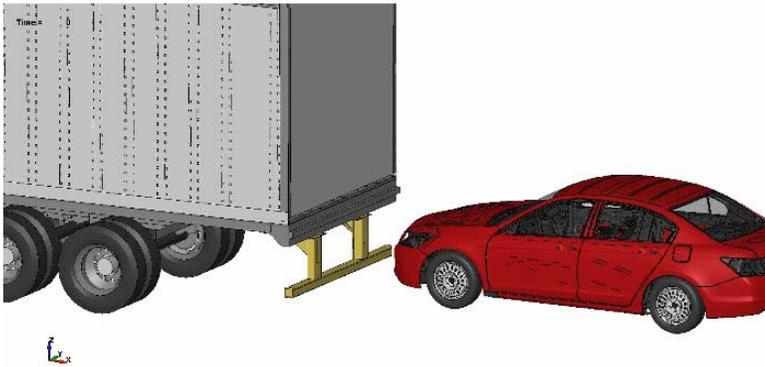
FW



50%



30%



Great Dane	Dynamic Response PCI Prevented?		
	FW	50%	30%
Baseline	Yes	Yes	No
Minimally Compliant	Yes	Yes	No

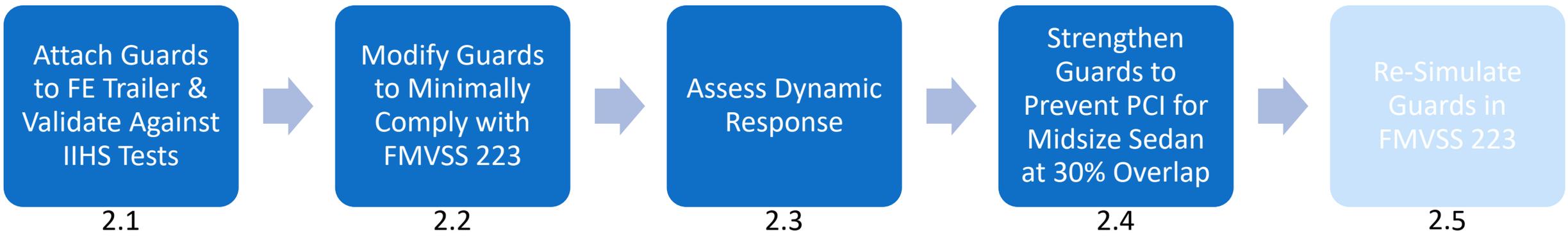
✓ PCI Prevented
 ✗ PCI Not Prevented

Guard Model		PCI Dynamic Response			Quasi-Static Response				Mass (kg)
		FW	50%	30%	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Manac	Baseline	✓	✓	✓	172.5	83.3	356.2	36.8	84.8
	Minimally Compliant	✓	✓	✓	157.1	52.5	351.9	33.3	75.7
	Strengthened– Midsize								
Wabash	Baseline	✓	✓	✗	135.8	125.4	394.7	32.1	54.4
	Minimally Compliant	✓	✓	✗	79.6	68.5	350.4	25.6	38.9
	Strengthened– Midsize	⊙	⊙	⊙	—————→ ?				
Great Dane	Baseline	✓	✓	✗	120.5	149.4	441.7	36.6	69.4
	Minimally Compliant	✓	✓	✗	67.2	77.0	350.4	29.4	52.5
	Strengthened– Midsize	⊙	⊙	⊙	—————→ ?				
FMVSS No. 223 Requirement					≥50	≥50	≥350	≥20	N/A

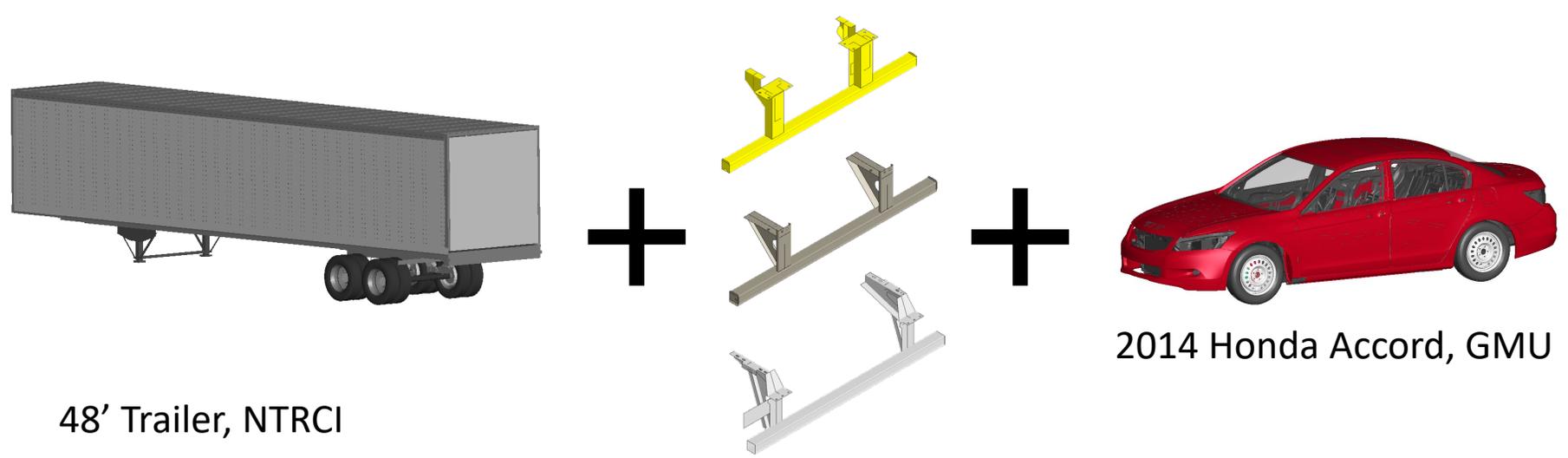
✓ PCI Prevented

✗ PCI Not Prevented

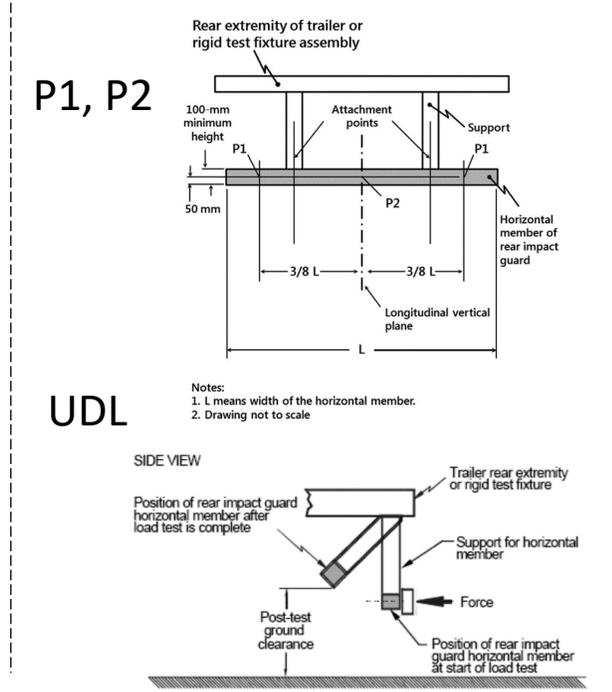
Guard Model		PCI Dynamic Response			Quasi-Static Response				Mass (kg)
		FW	50%	30%	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Manac	Baseline	✓	✓	✓	172.5	83.3	356.2	36.8	84.8
	Minimally Compliant	✓	✓	✓	157.1	52.5	351.9	33.3	75.7
	Strengthened– Midsize								
Wabash	Baseline	✓	✓	✗	135.8	125.4	394.7	32.1	54.4
	Minimally Compliant	✓	✓	✗	79.6	68.5	350.4	25.6	38.9
	Strengthened– Midsize								
Great Dane	Baseline	✓	✓	✗	120.5	149.4	441.7	36.6	69.4
	Minimally Compliant	✓	✓	✗	67.2	77.0	350.4	29.4	52.5
	Strengthened– Midsize								
FMVSS No. 223 Requirement					≥50	≥50	≥350	≥20	N/A



Dynamic Simulations



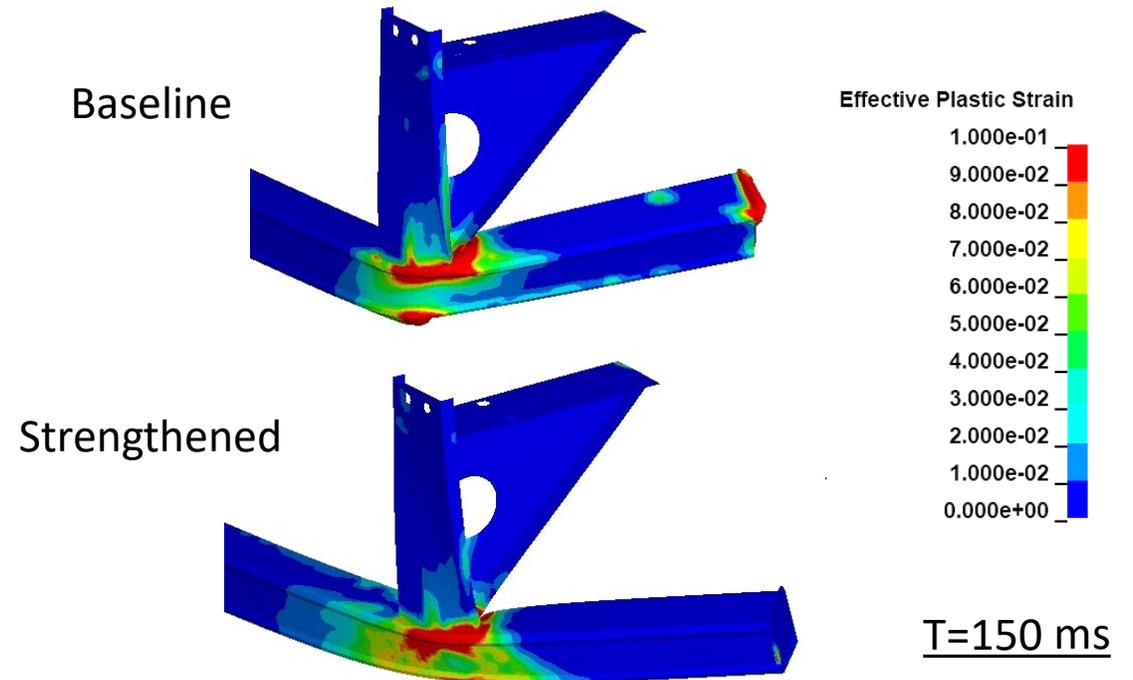
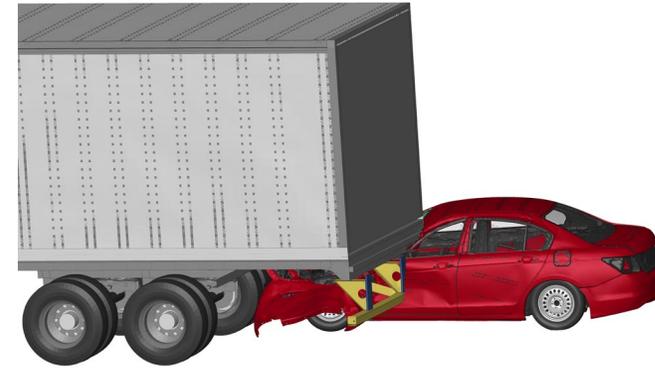
Quasi-Static Simulations





Strengthening Guards:

- Identified parts that were carrying majority of load
- Increase thicknesses of parts in build-simulate-build iterative manner
- Goal: Find minimum thicknesses that still prevent PCI

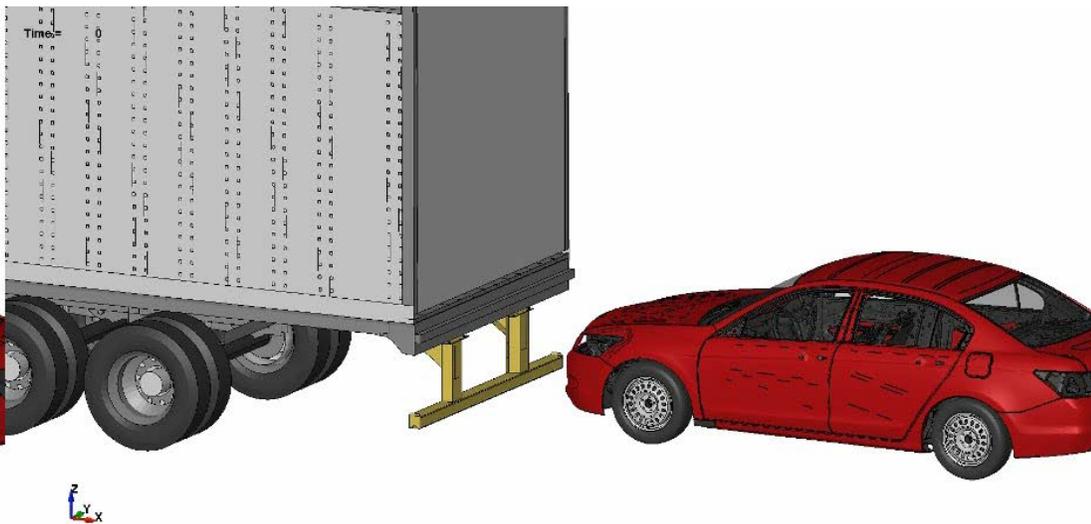
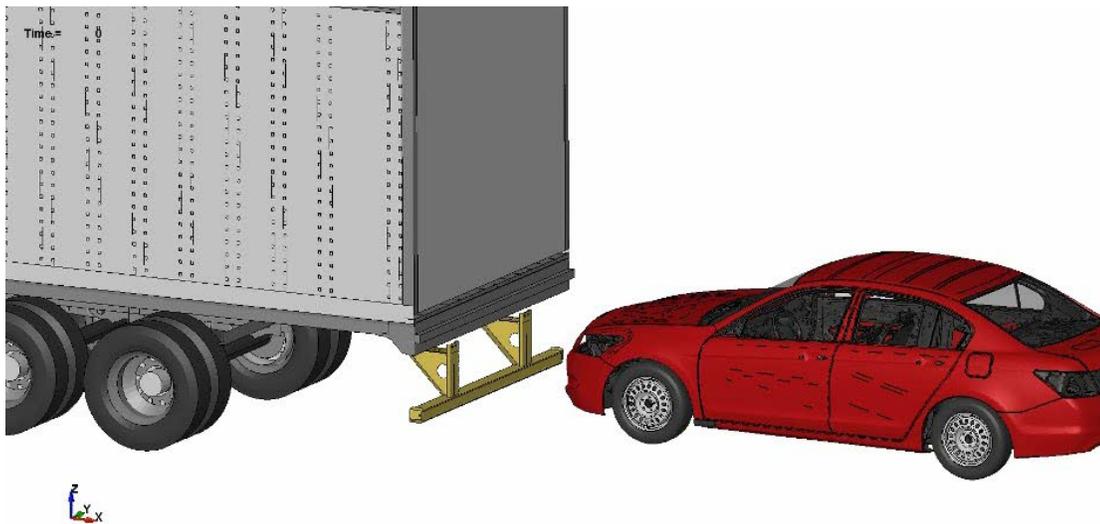




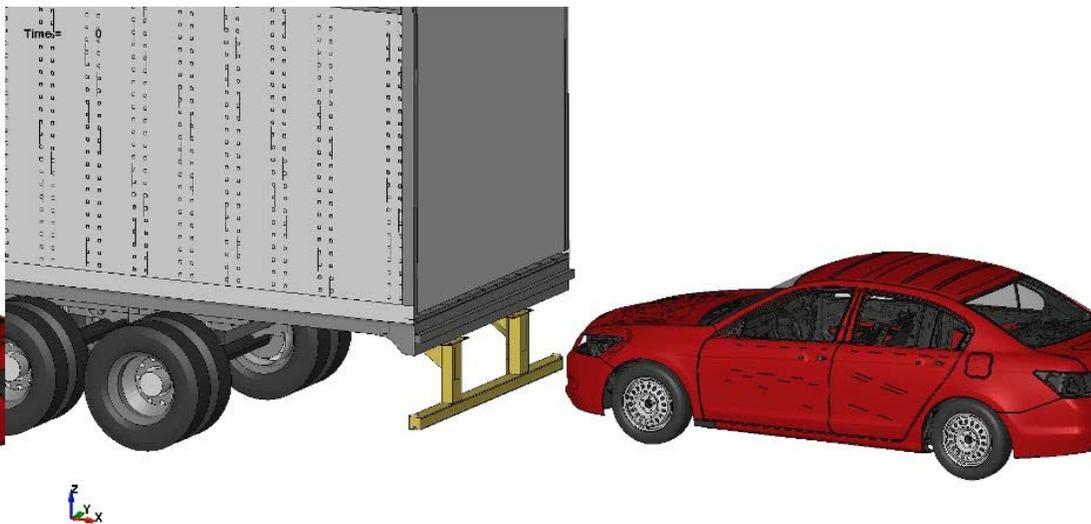
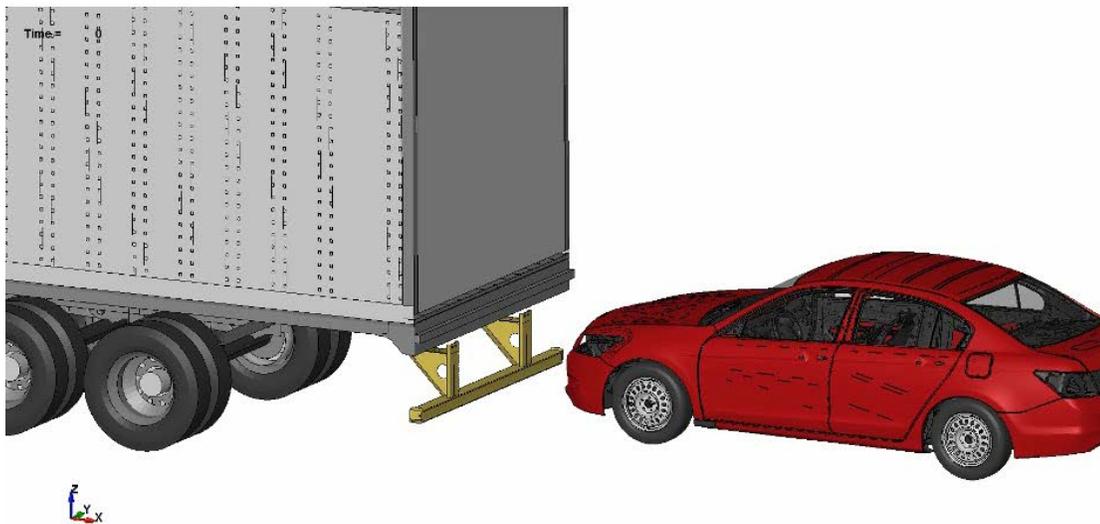
Wabash

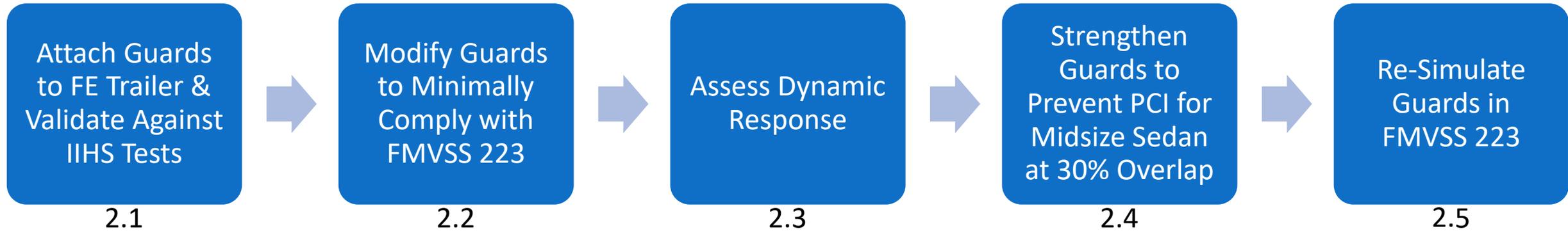
Great Dane

Baseline

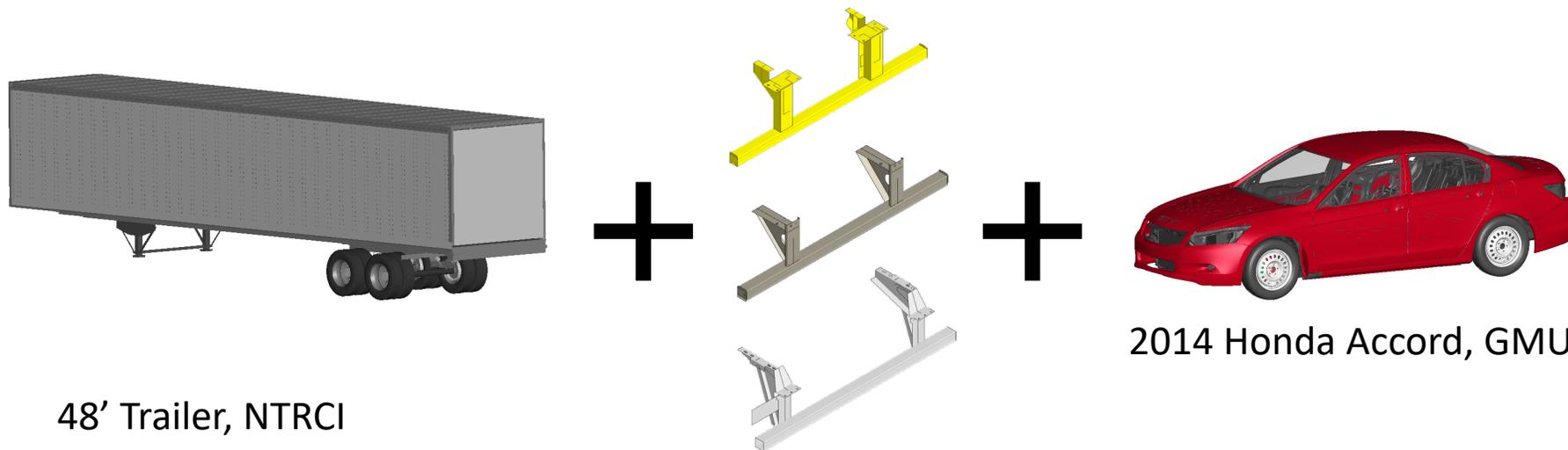


Strengthened

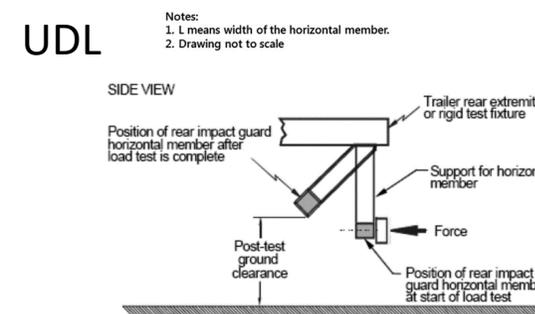
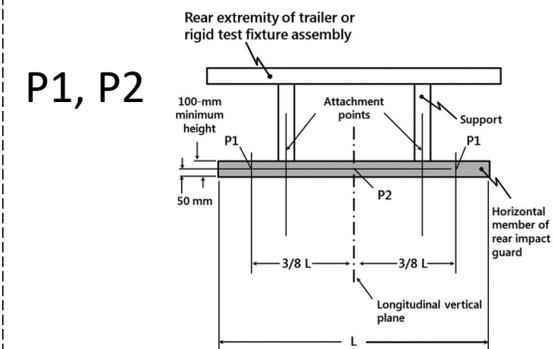


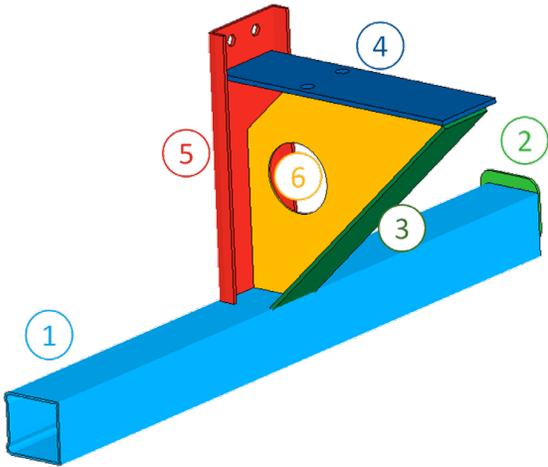


Dynamic Simulations

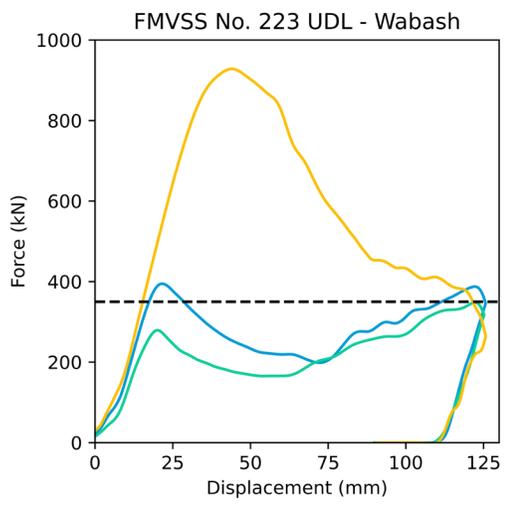
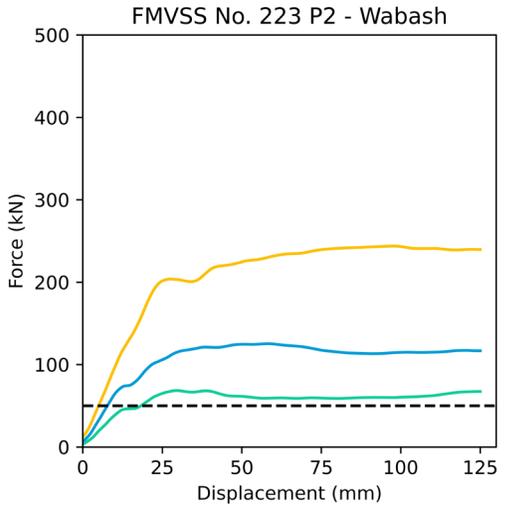
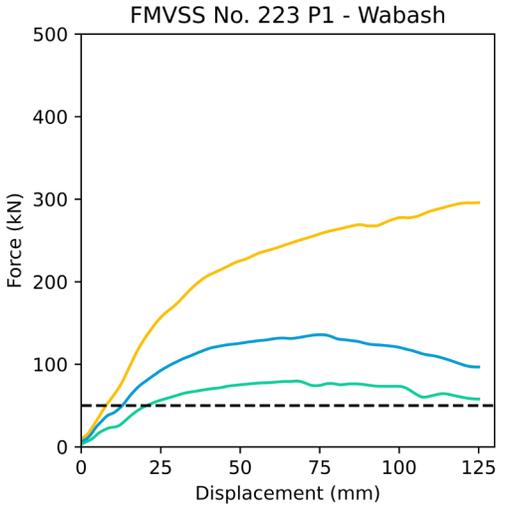
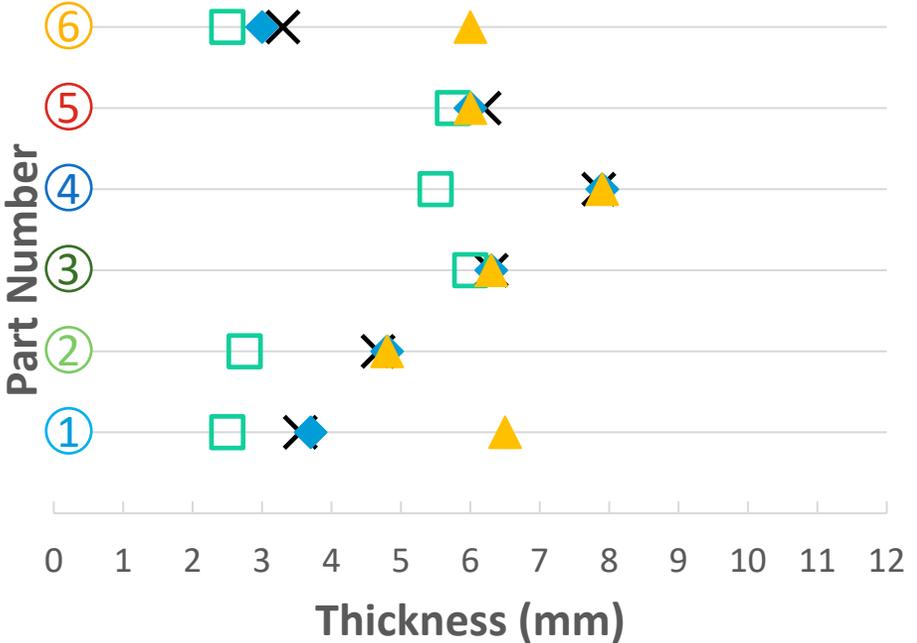


Quasi-Static Simulations

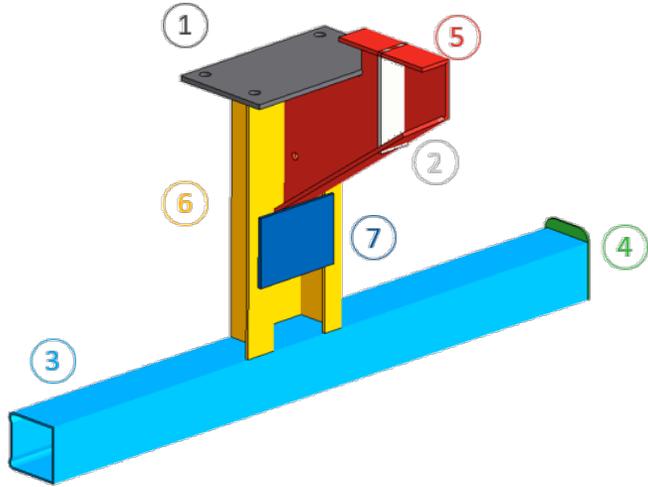




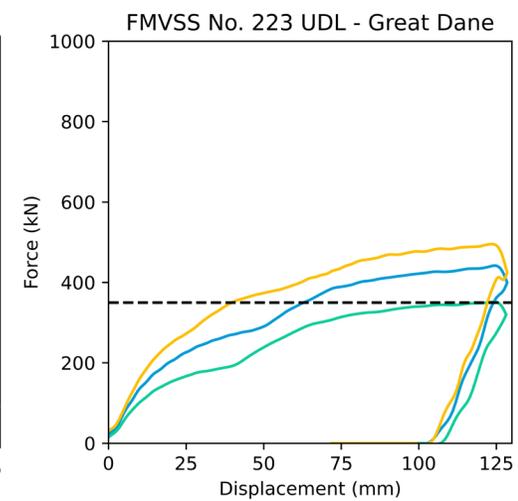
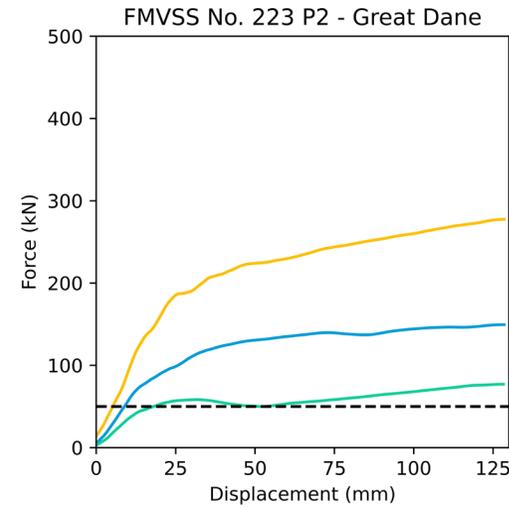
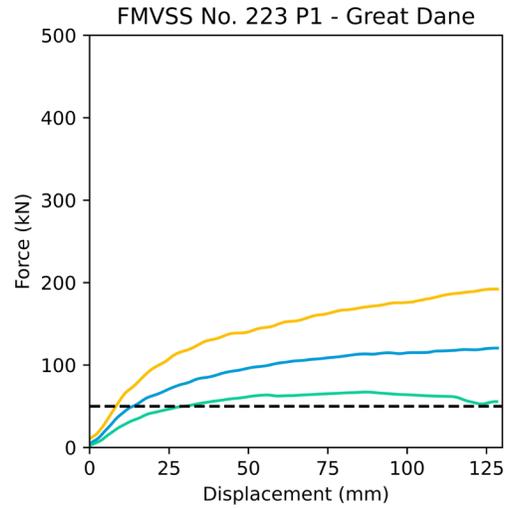
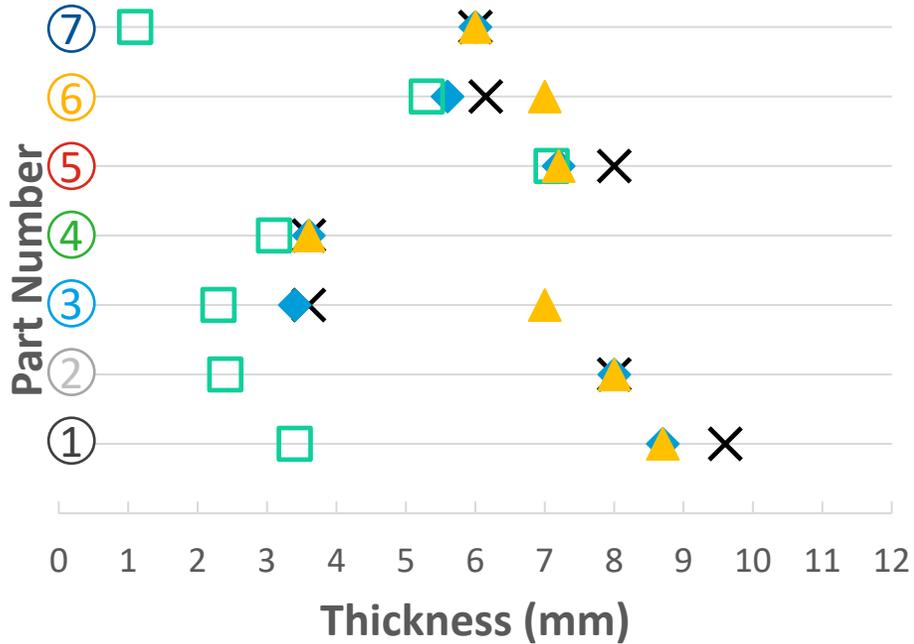
Wabash	Quasi-Static Response				Mass (kg)
	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Baseline	135.8	125.4	394.7	32.1	54.4
Minimally Compliant	79.6	68.5	350.4	25.6	38.9
Strengthened	295.7	243.8	928.1	68.0	75.8
FMVSS Req.	≥50	≥50	≥350	≥20	N/A



X Measured ♦ Tuned □ Minimally Compliant ▲ Strengthened

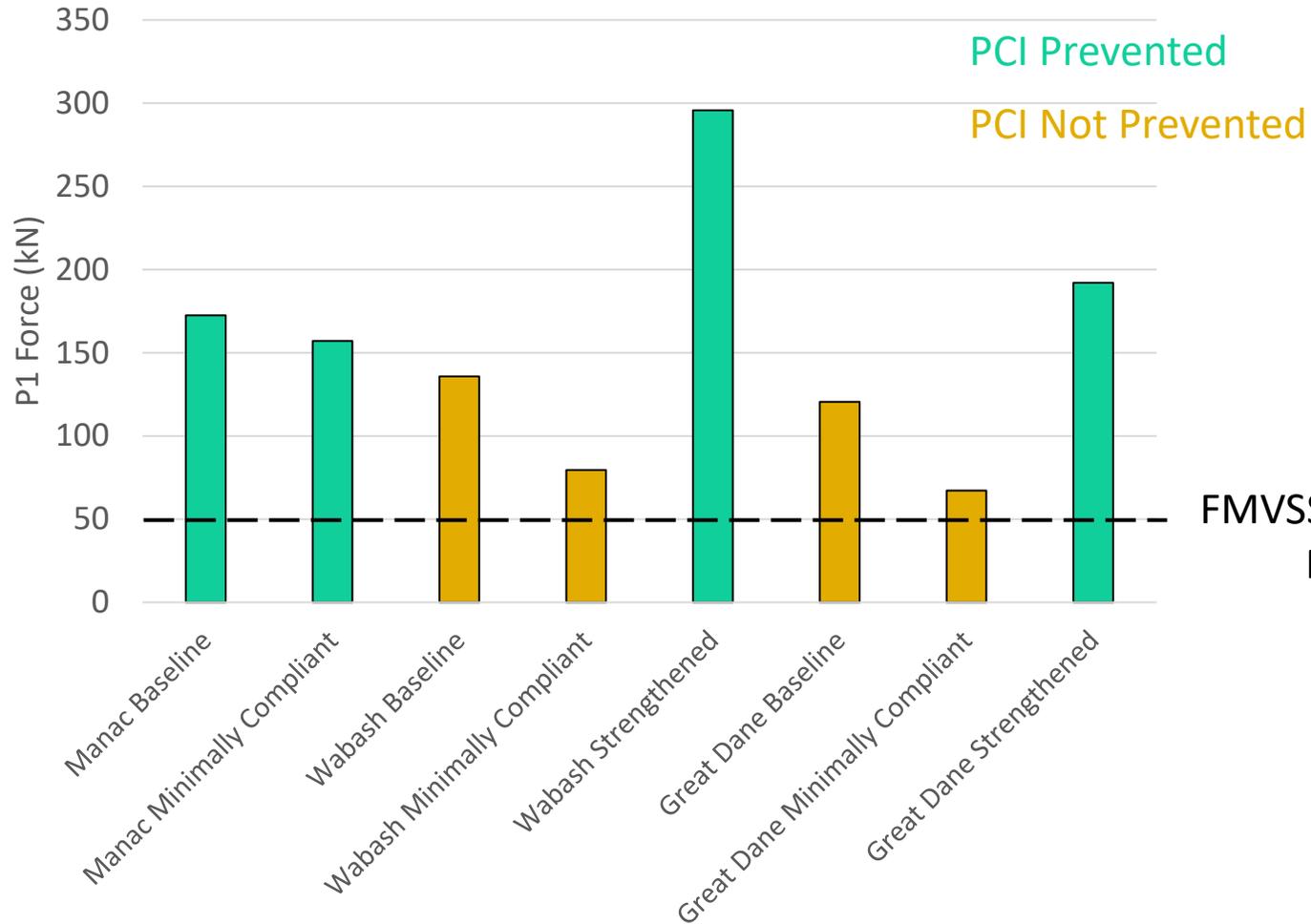


Wabash	Quasi-Static Response				Mass (kg)
	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Baseline	120.5	149.4	441.7	36.6	69.4
Minimally Compliant	67.2	77.0	350.4	29.4	52.5
Strengthened	192.1	277.3	495.4	42.8	101.1
FMVSS Req.	≥50	≥50	≥350	≥20	N/A

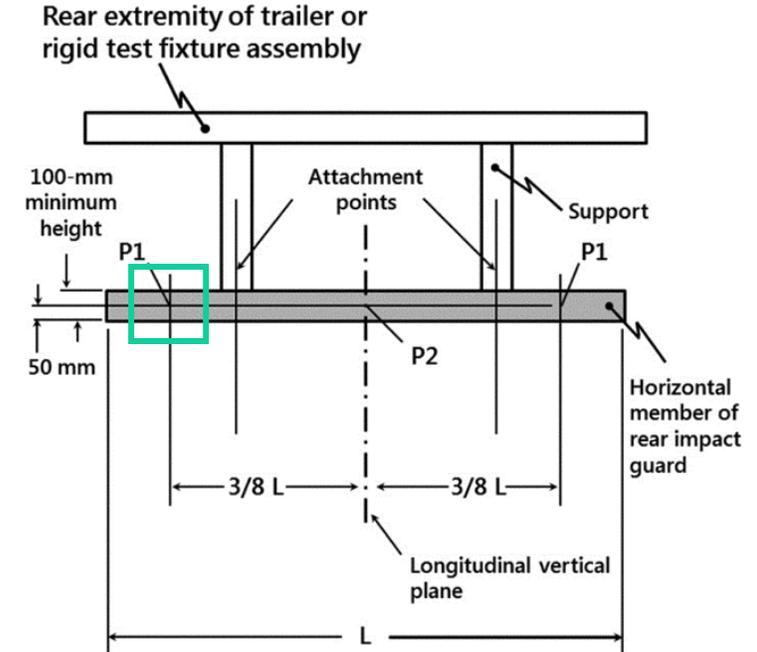


X Measured ♦ Tuned □ Minimally Compliant ▲ Strengthened

P1 Force & 30% PCI Prevention



FMVSS No. 223
Req.

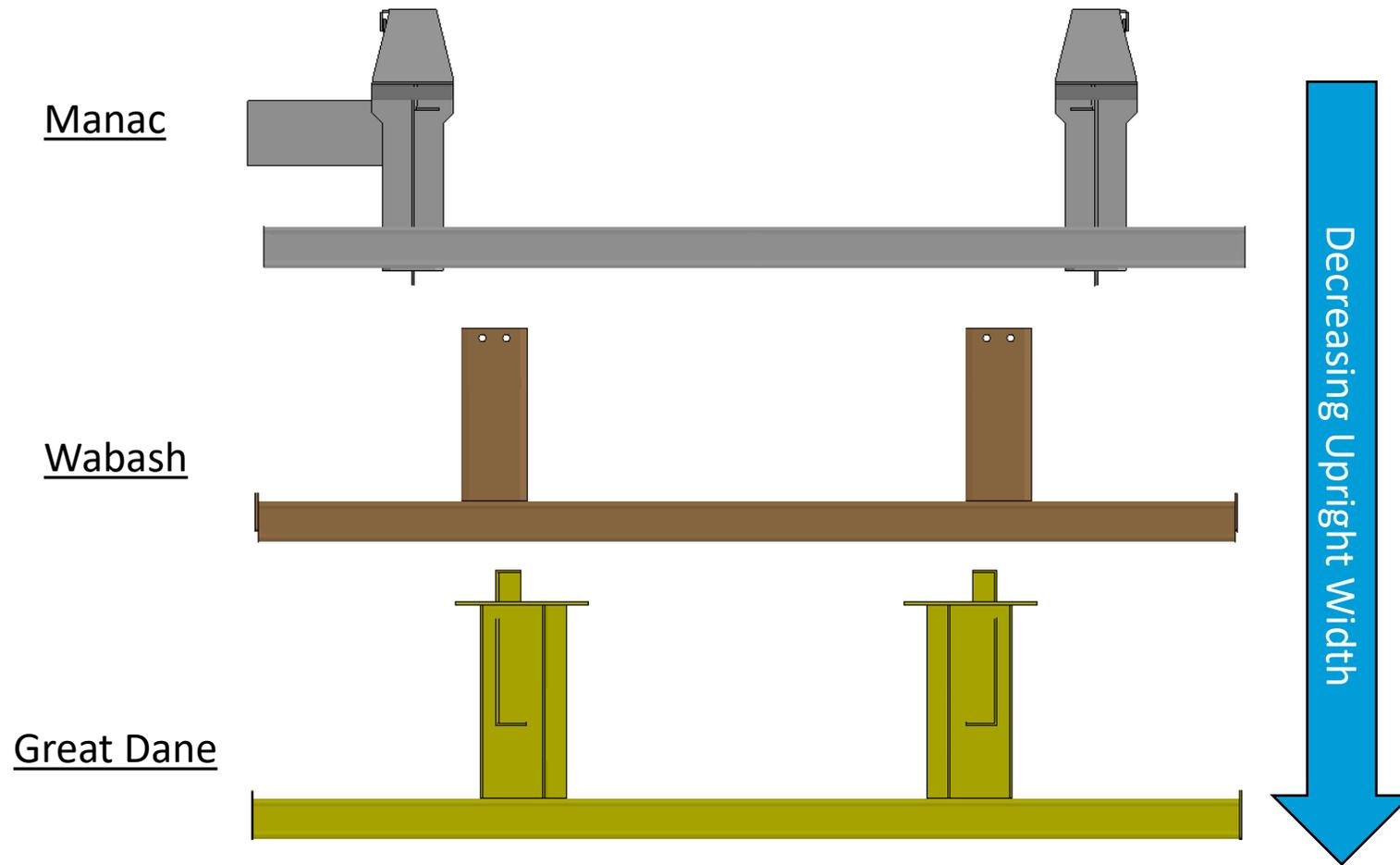


- Notes:
1. L means width of the horizontal member.
 2. Drawing not to scale

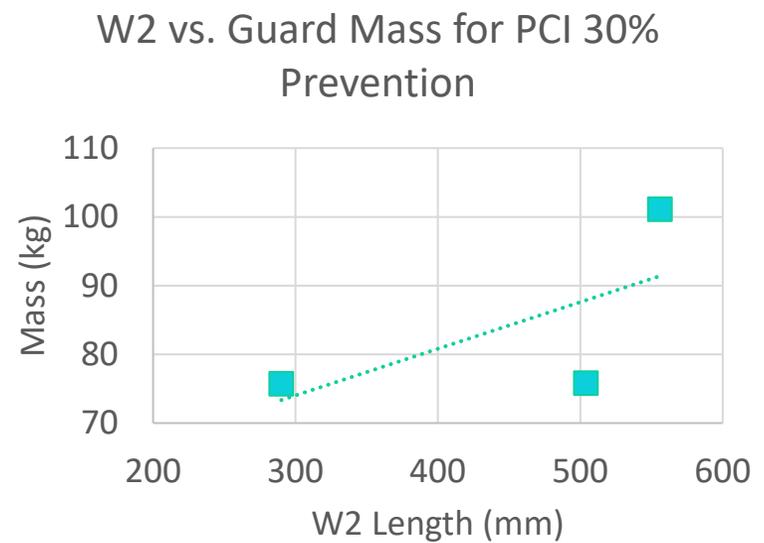
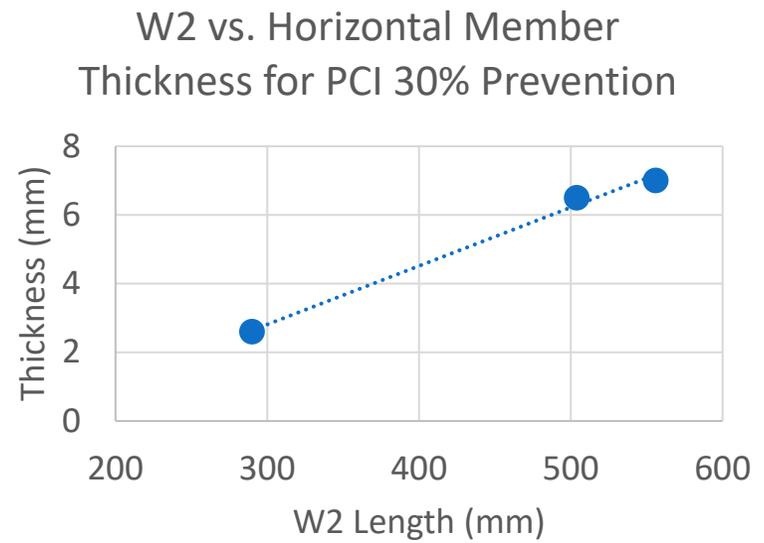
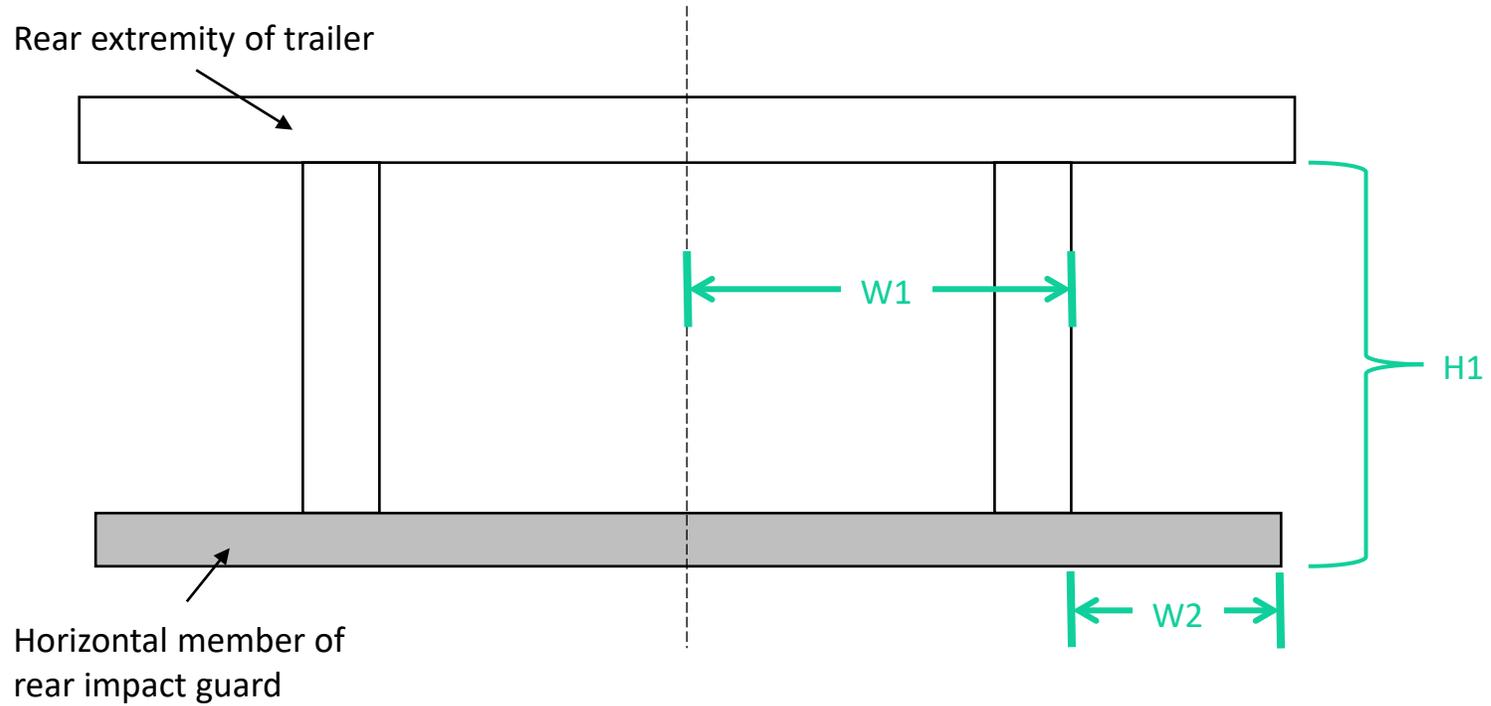
✓ PCI Prevented

✗ PCI Not Prevented

Guard Model		PCI Dynamic Response			Quasi-Static Response				Mass (kg)
		FW	50%	30%	P1 Force (kN)	P2 Force (kN)	UDL Force (kN)	UDL Energy (kJ)	
Manac	Baseline	✓	✓	✓	172.5	83.3	356.2	36.8	84.8
	Minimally Compliant	✓	✓	✓	157.1	52.5	351.9	33.3	75.7
	Strengthened– Midsize								
Wabash	Baseline	✓	✓	✗	135.8	125.4	394.7	32.1	54.4
	Minimally Compliant	✓	✓	✗	79.6	68.5	350.4	25.6	38.9
	Strengthened– Midsize	✓	✓	✓	295.7	243.8	928.1	68.0	75.8
Great Dane	Baseline	✓	✓	✗	120.5	149.4	441.7	36.6	69.4
	Minimally Compliant	✓	✓	✗	67.2	77.0	350.4	29.4	52.5
	Strengthened– Midsize	✓	✓	✓	192.1	277.3	495.4	42.8	101.1
FMVSS No. 223 Requirement					≥50	≥50	≥350	≥20	N/A



Model Version Preventing PCI @ 30% Overlap	
Horizontal Member Thickness (mm)	Guard Mass (kg)
2.6	75.7
6.5	75.8
7.0	101.1



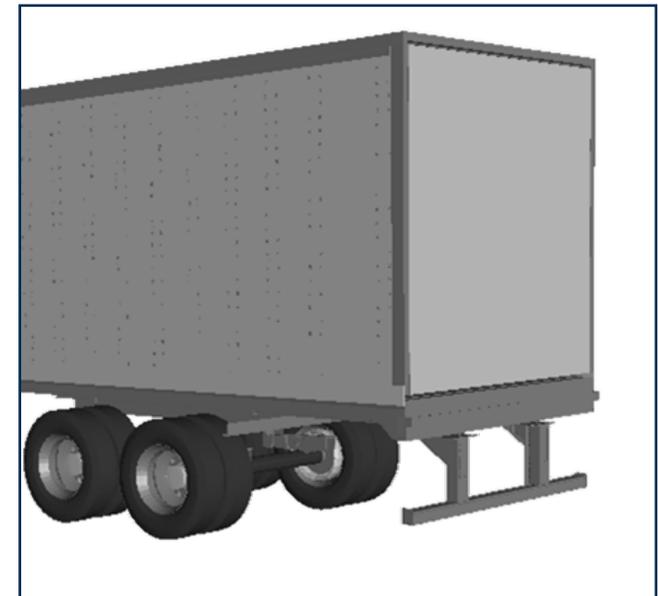
Guard	H1	W1	W2
Manac	450	910	290
Wabash	525	690	504
Great Dane	575	650	556



- Bolt connections not explicitly modeled. Instead, rigid constraints at bolt holes
- Trailer model generic, not modified to replicate each manufacturer's trailer
- Trailer ride height not adjusted between guards
- Preliminary validation only possible between physical Chevrolet Malibu and simulation Honda Accord

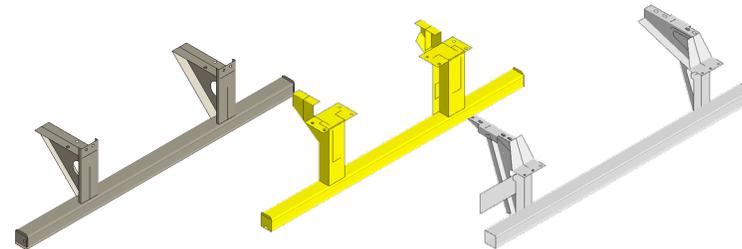
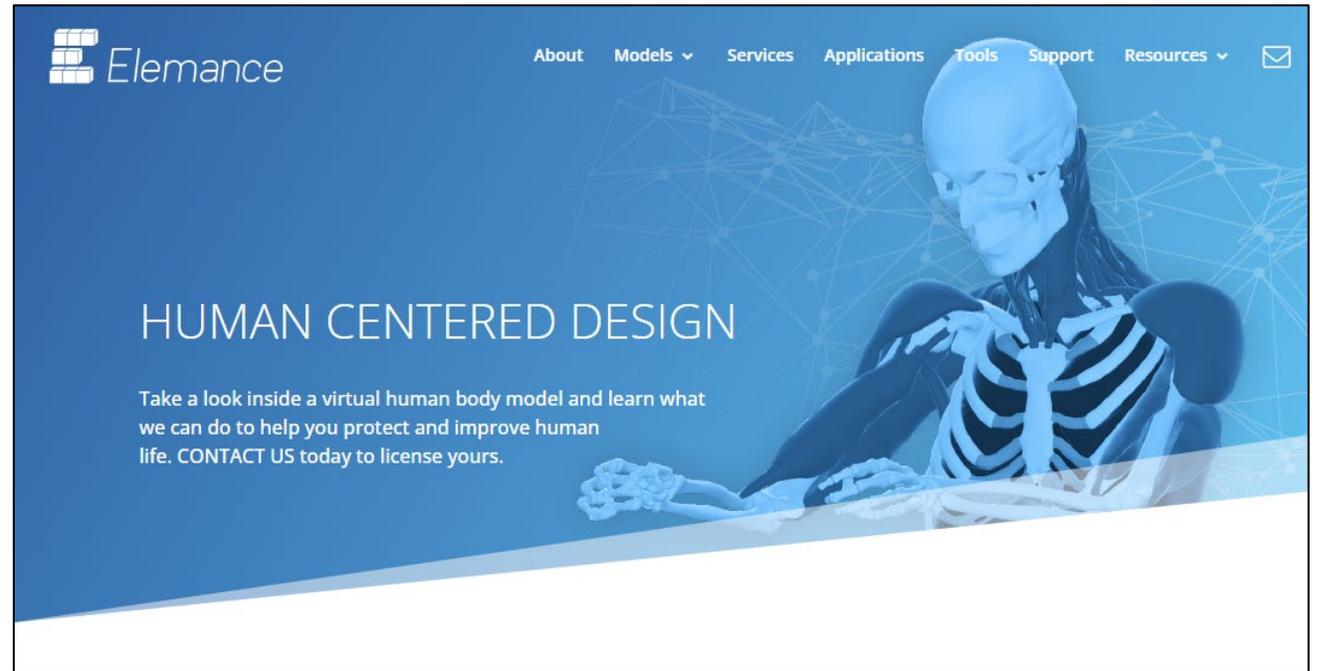


- PCI prevented in both baseline and minimally compliant conditions, 50% and Full Width 35 mph cases across all models
- 30% Overlap PCI prevention is particularly challenging; selectively increasing guard metal thicknesses can prevent PCI, but comes with large mass increases
- As width between the uprights decreases, required horizontal member strength increases



Thank you!

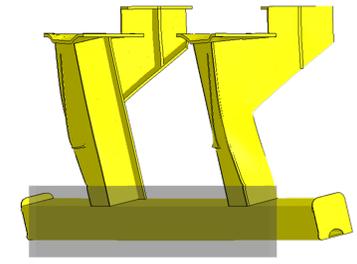
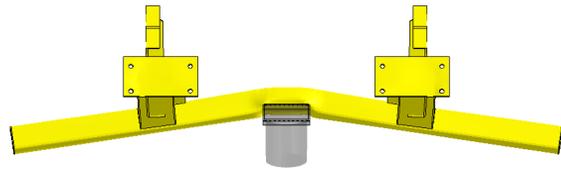
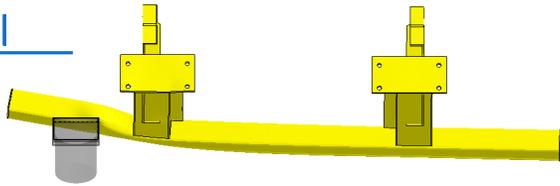
NHTSA Contract Number: 693JJ921D000042



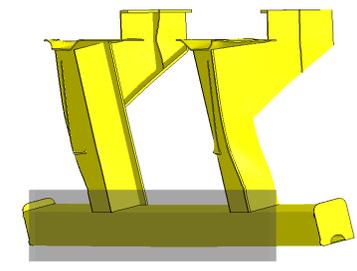
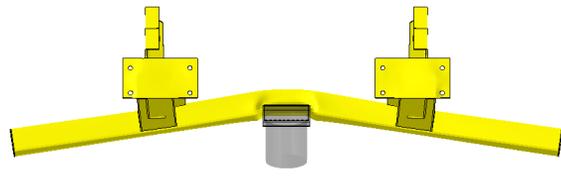
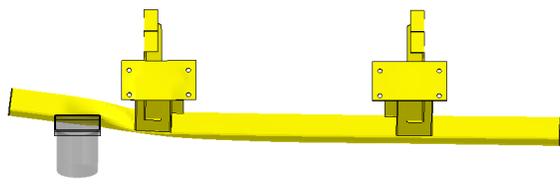
**Models freely available at
[Elemance.com](https://www.elemance.com)**



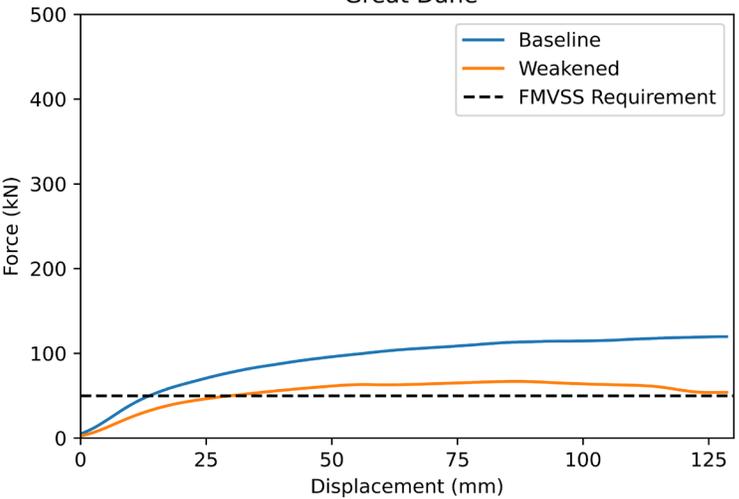
Basel



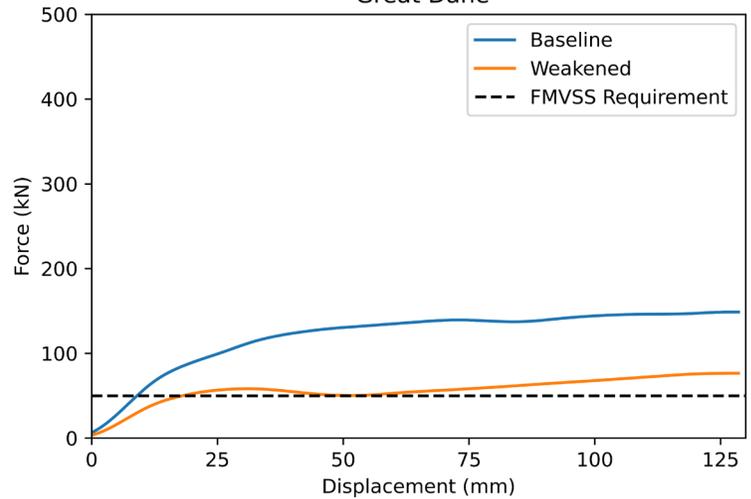
Minimally Compliant



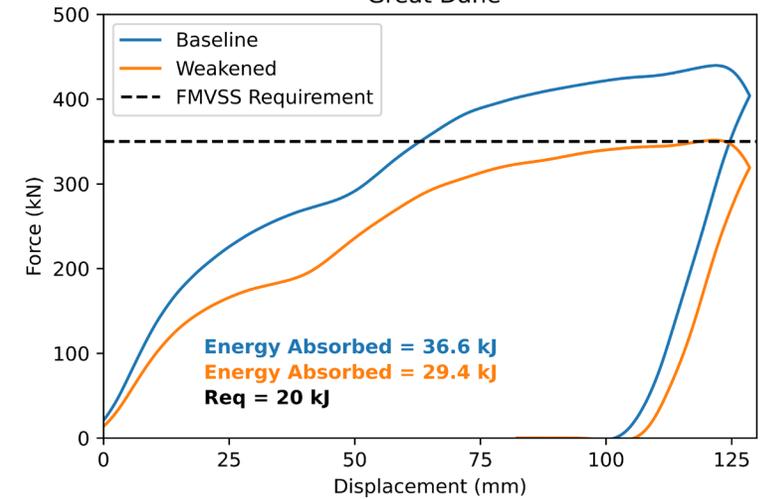
FMVSS 223 Minimal Requirements P1
Great Dane



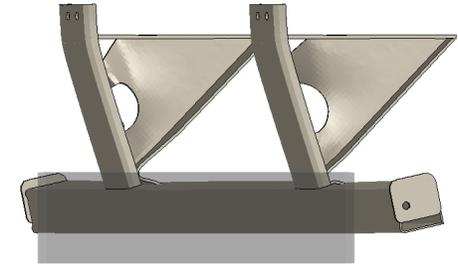
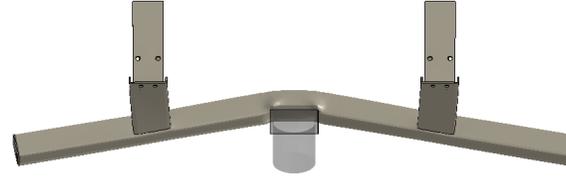
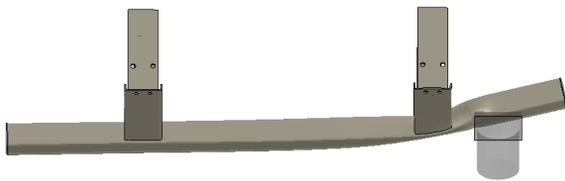
FMVSS 223 Minimal Requirements P2
Great Dane



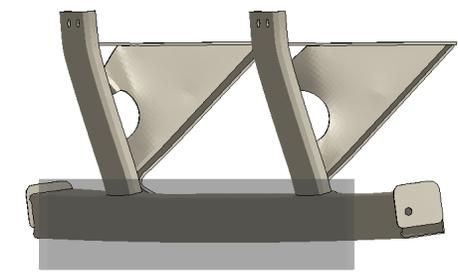
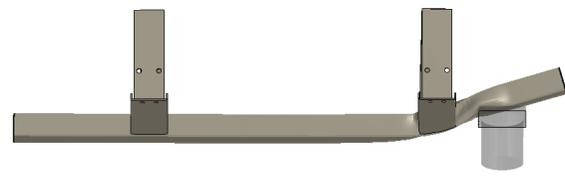
FMVSS 223 Minimal Requirements UDL
Great Dane



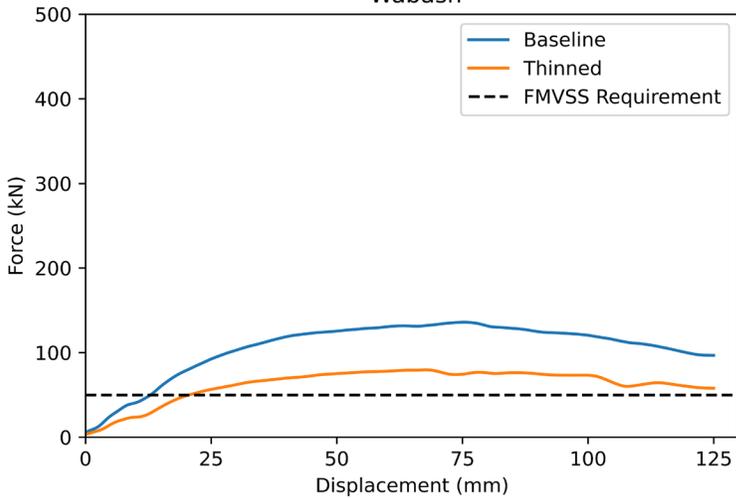
Baseline



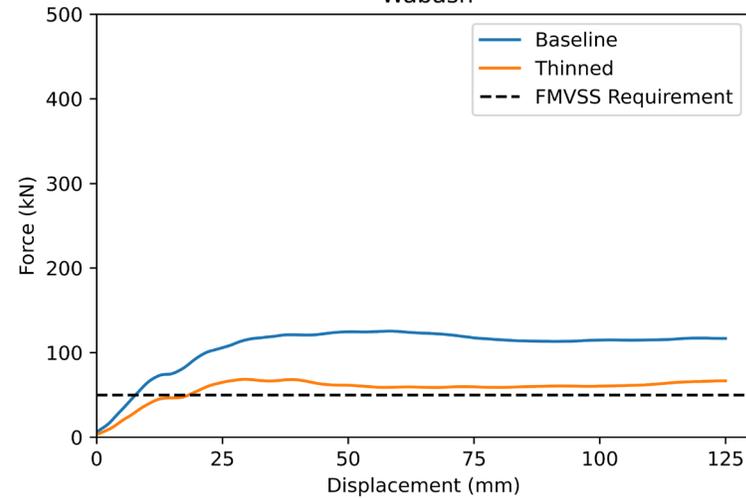
Minimally Compliant



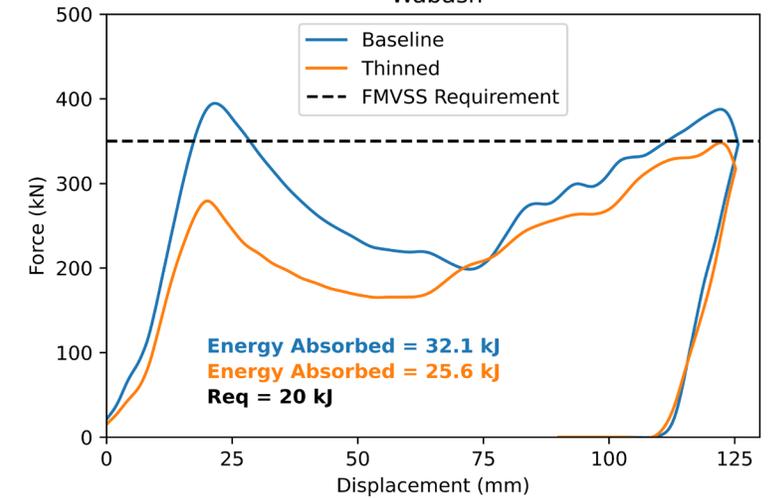
FMVSS 223 Minimal Requirements P1
Wabash



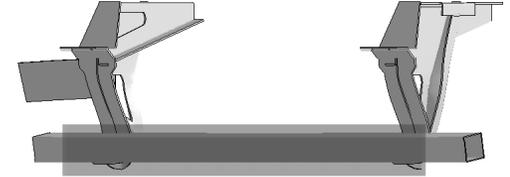
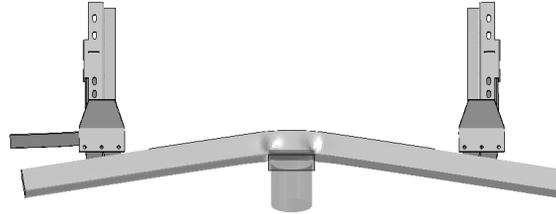
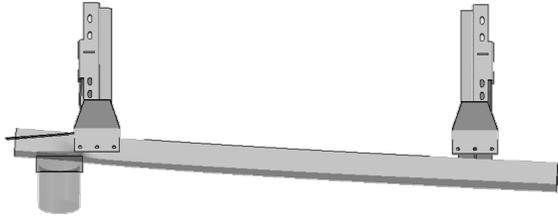
FMVSS 223 Minimal Requirements P2
Wabash



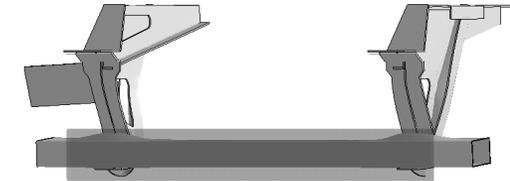
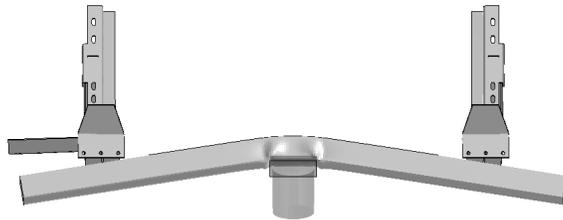
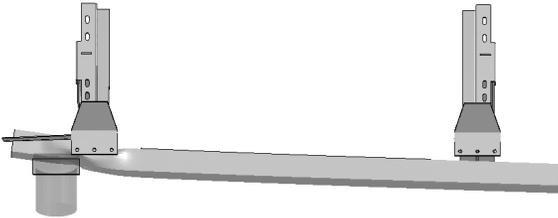
FMVSS 223 Minimal Requirements UDL
Wabash



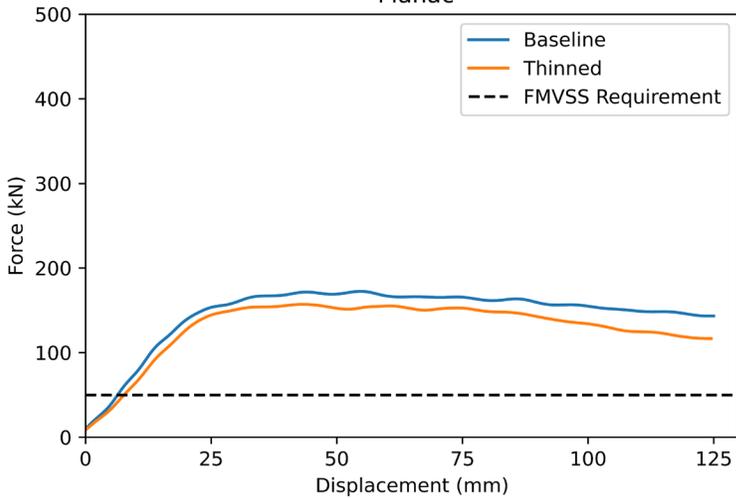
Baseline



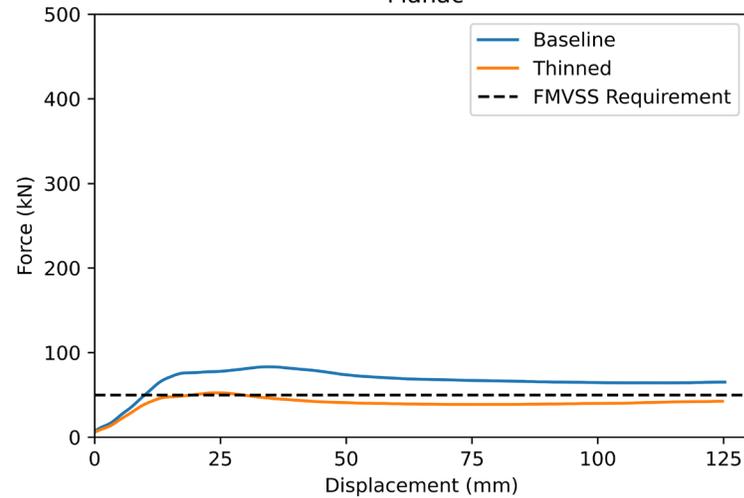
Minimally Compliant



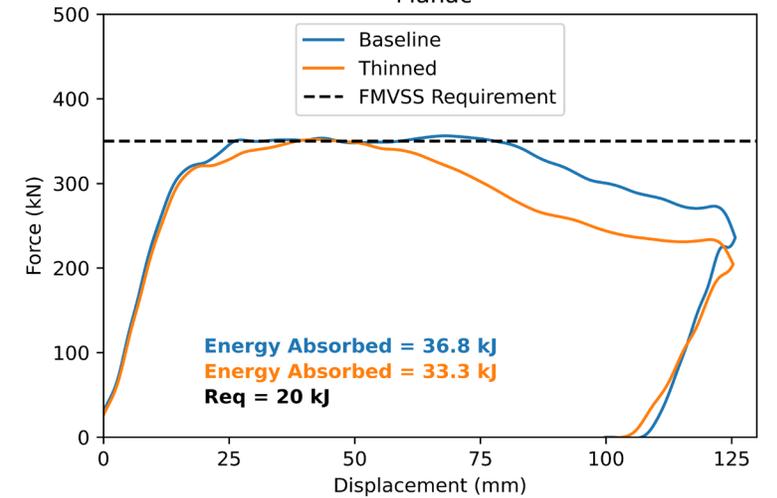
FMVSS 223 Minimal Requirements P1
Manac



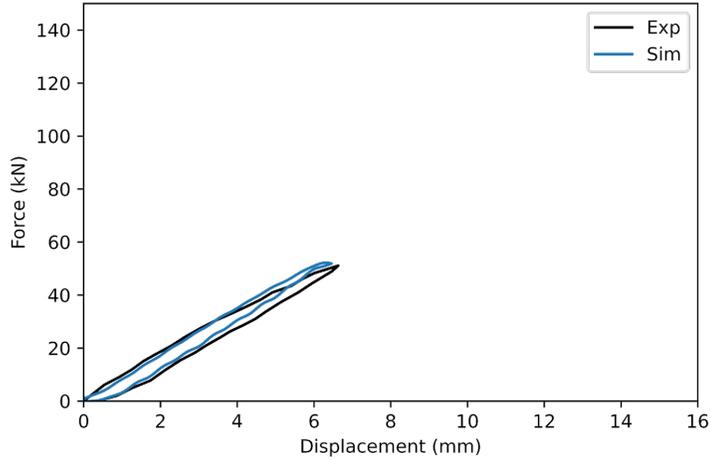
FMVSS 223 Minimal Requirements P2
Manac



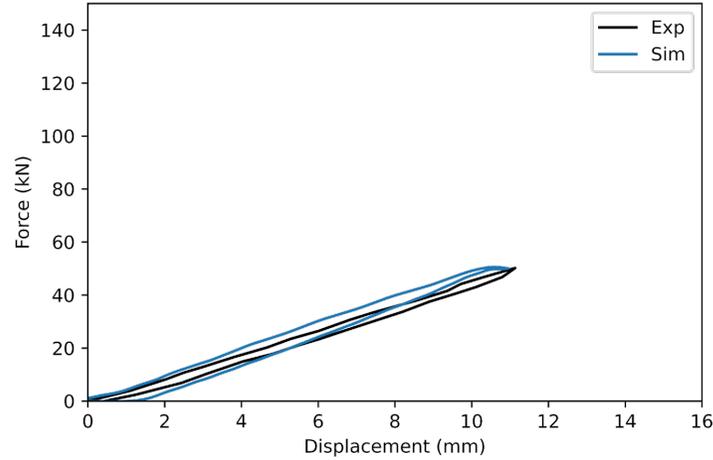
FMVSS 223 Minimal Requirements UDL
Manac



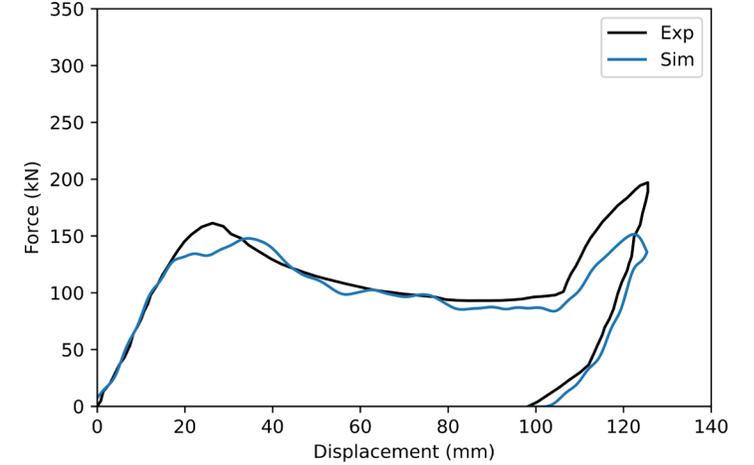
Manac P1 - Baseline



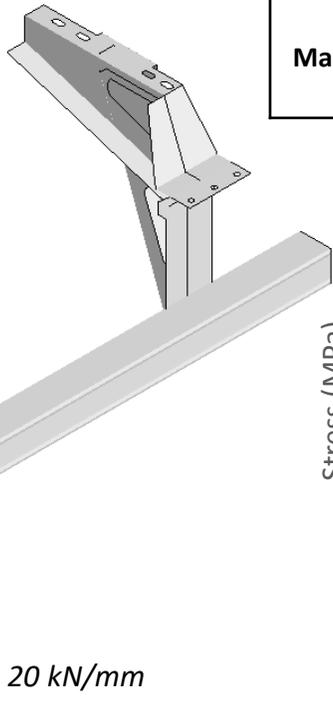
Manac P2 - Baseline



Manac P3 - Baseline

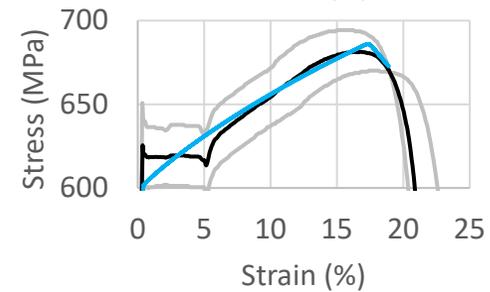
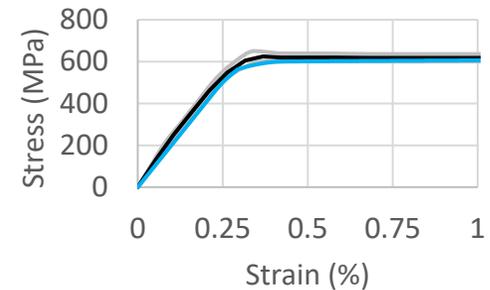
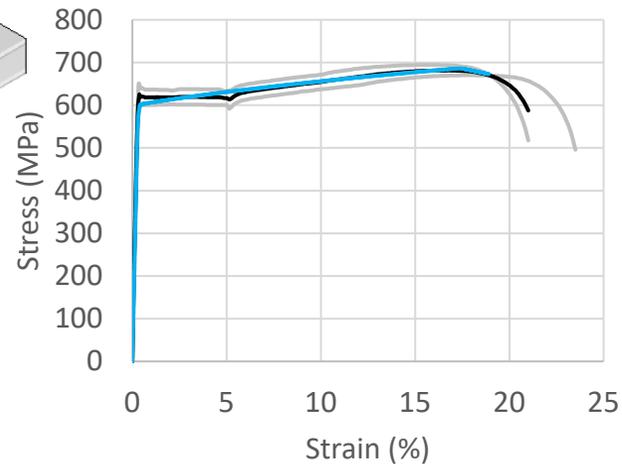


Element Type	Count (%)
Quad	21,224 (99.5%)
Tria	114 (0.5%)
Total	21,338



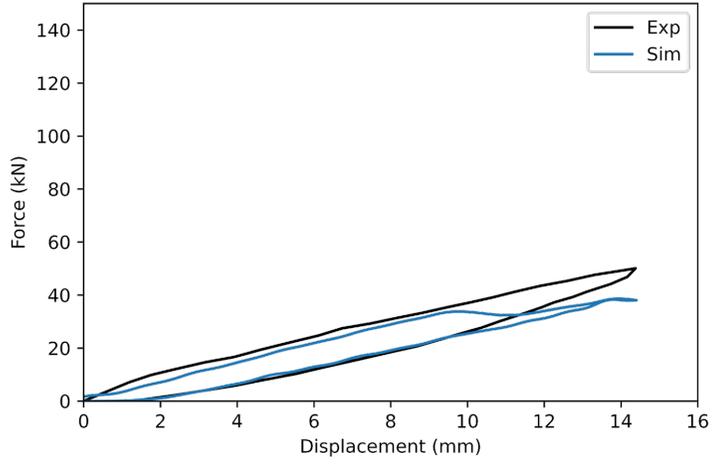
Fixture Stiffness: 20 kN/mm

CORA Scores						
		Phase	Size	Shape	Total	Avg
Manac	P1	1.000	1.000	0.981	0.994	0.954
	P2	1.000	0.889	0.994	0.961	
	P3	1.000	0.780	0.943	0.908	

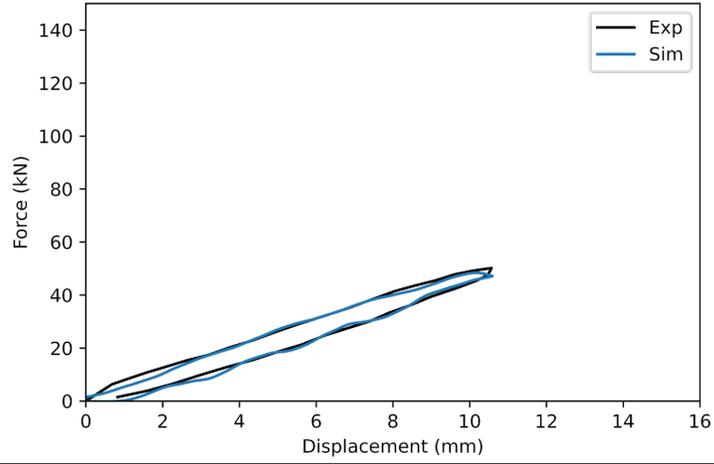


*MAT_098 (GPa) Manac	
E	209.91
A	0.6007
B	0.7271
N	0.8944
SIGMAX	0.7402

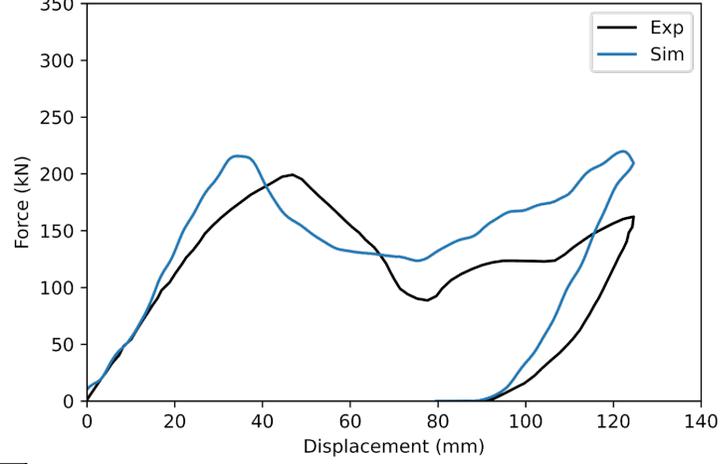
Wabash P1 - Baseline



Wabash P2 - Baseline

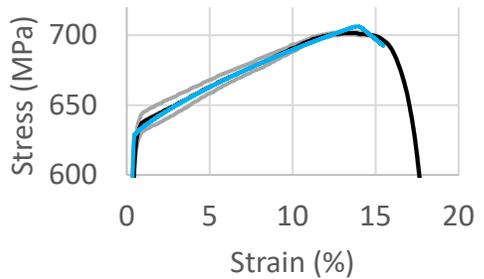
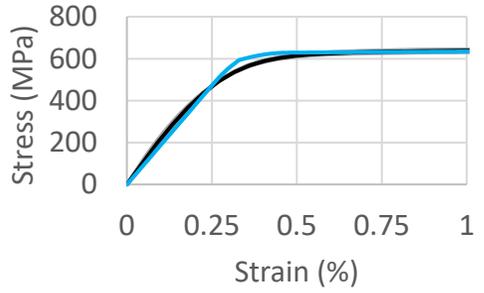
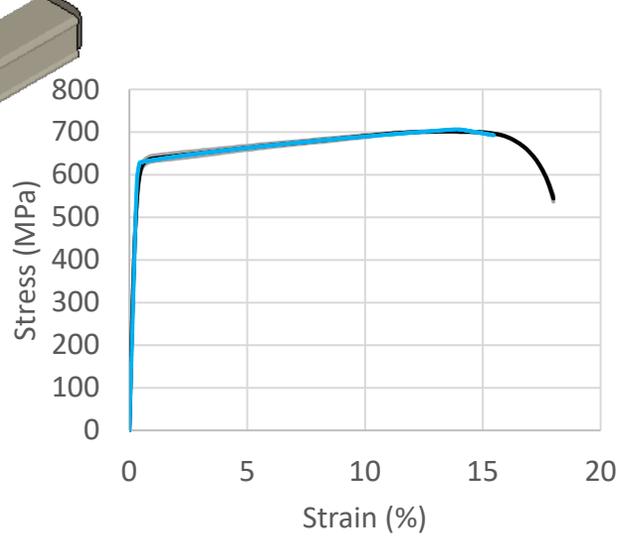
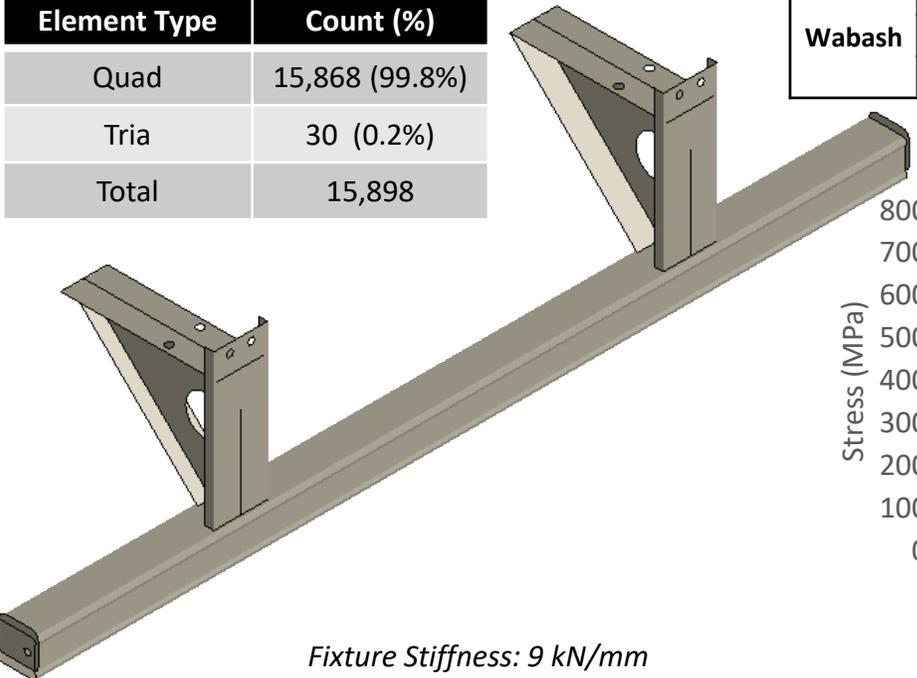


Wabash P3 - Baseline



Element Type	Count (%)
Quad	15,868 (99.8%)
Tria	30 (0.2%)
Total	15,898

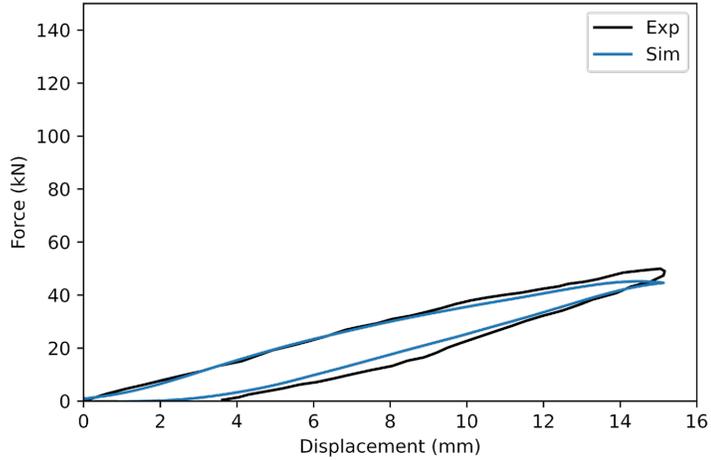
CORA Scores						
		Phase	Size	Shape	Total	Avg
Wabash	P1	1.000	0.734	0.976	0.903	0.921
	P2	1.000	0.985	0.995	0.993	
	P3	1.000	0.712	0.89	0.867	



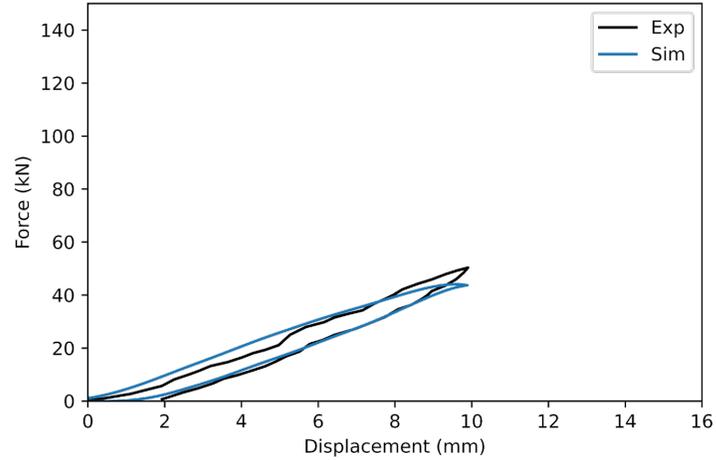
*MAT_098 (GPa) Wabash	
E	189.93
A	0.6274
B	0.7788
N	0.8780
SIGMAX	0.7057



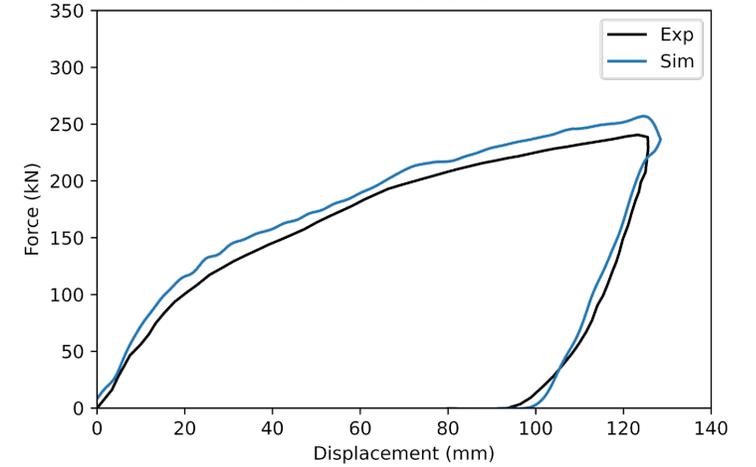
Great Dane P1 - Baseline



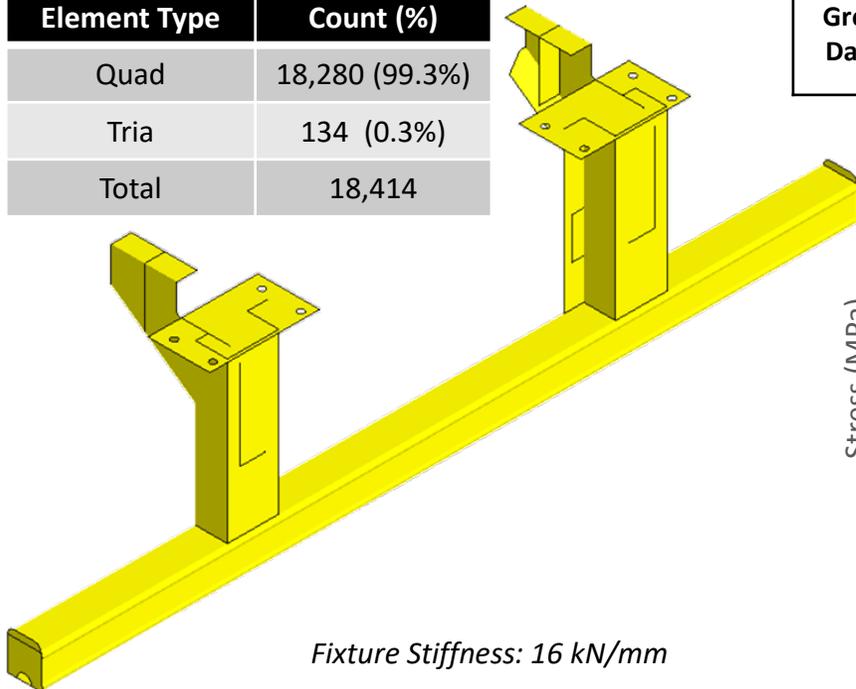
Great Dane P2 - Baseline



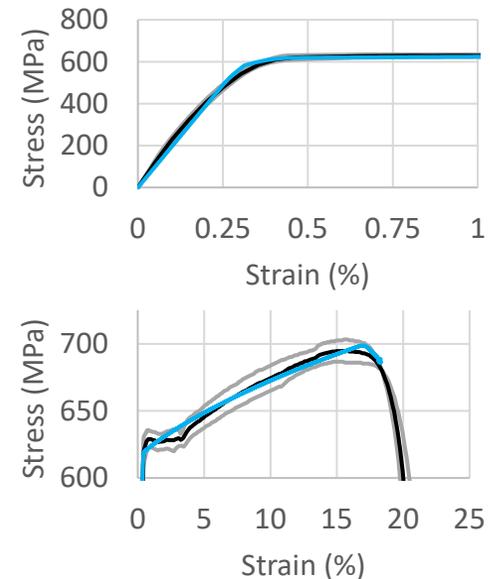
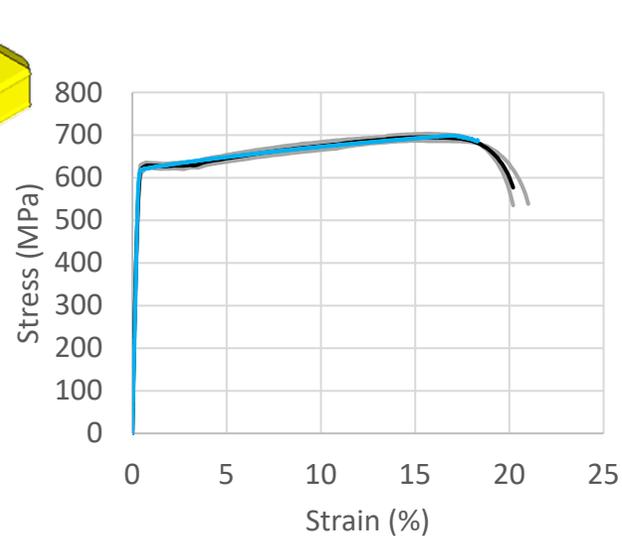
Great Dane P3 - Baseline



Element Type	Count (%)
Quad	18,280 (99.3%)
Tria	134 (0.3%)
Total	18,414



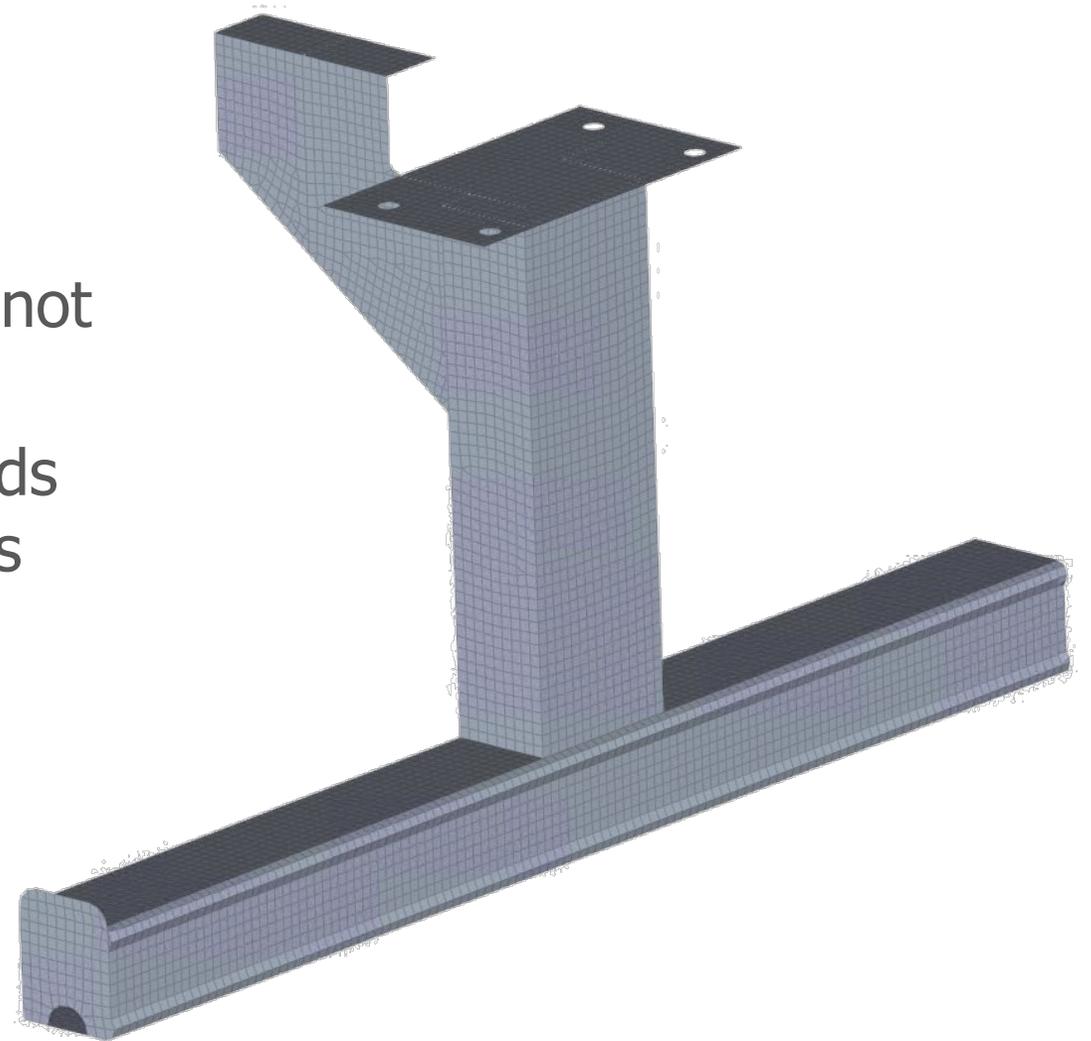
CORA Scores						
		Phase	Size	Shape	Total	Avg
Great Dane	P1	1.000	0.946	0.989	0.978	0.951
	P2	1.000	0.810	0.989	0.933	
	P3	1.000	0.836	0.989	0.942	

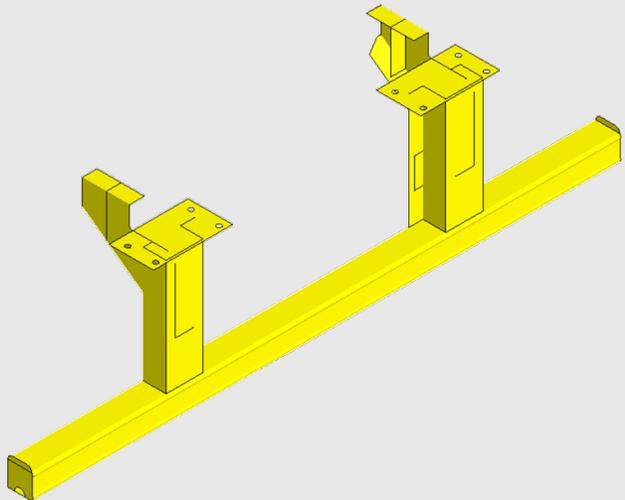
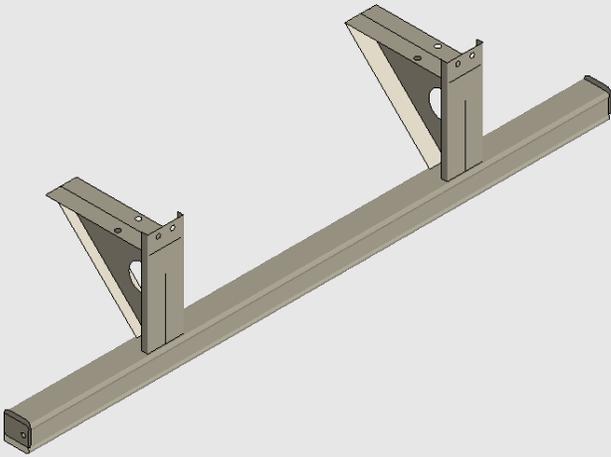
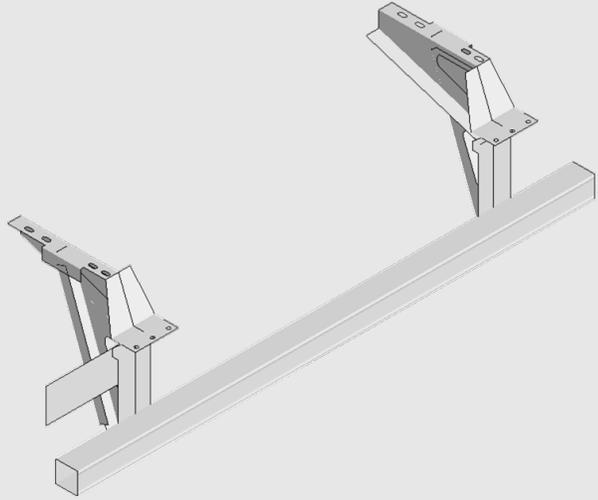


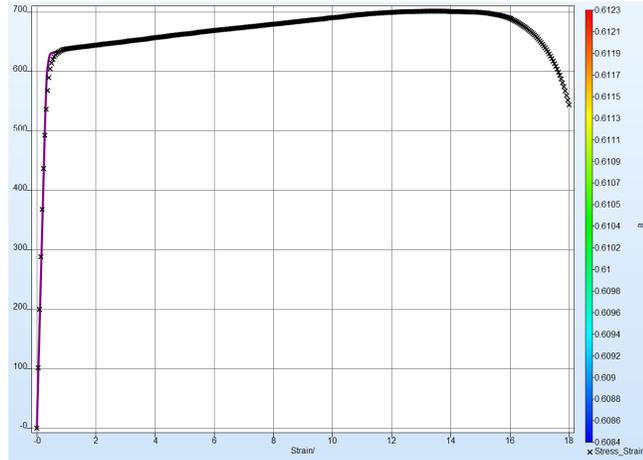
*MAT_098 (GPa) Great Dane	
E	196.84
A	0.6177
B	0.7432
N	0.8963
SIGMAX	0.7565



- Meshed in Beta ANSA:
 - Primarily quad shell elements
 - Target element length 10mm
 - Welds modeled as node-to-node connections or tied contacts where not possible
 - Thicknesses assigned in section cards according to physical measurements



Element Type	Great Dane	Wabash	Manac
Quad	18,280 (99.3%)	15,868 (99.8%)	21,224 (99.5%)
Tria	134 (0.3%)	30 (0.2%)	114 (0.5%)
Total	18,414	15,898	21,338
			

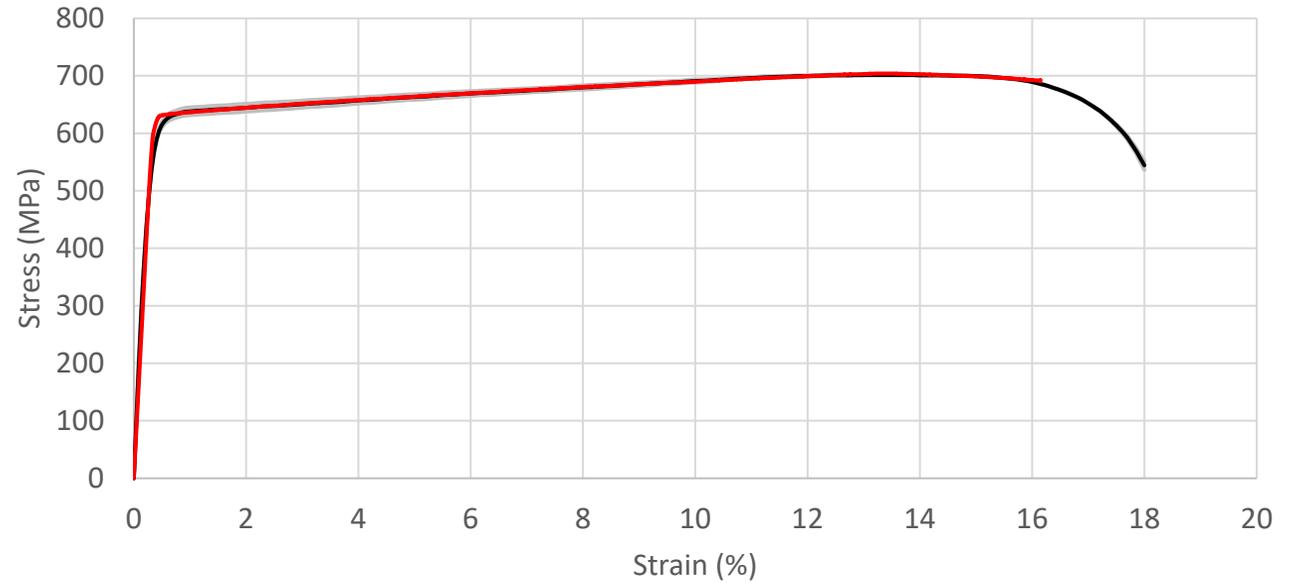


*MAT_98 Simplified Johnson Cook

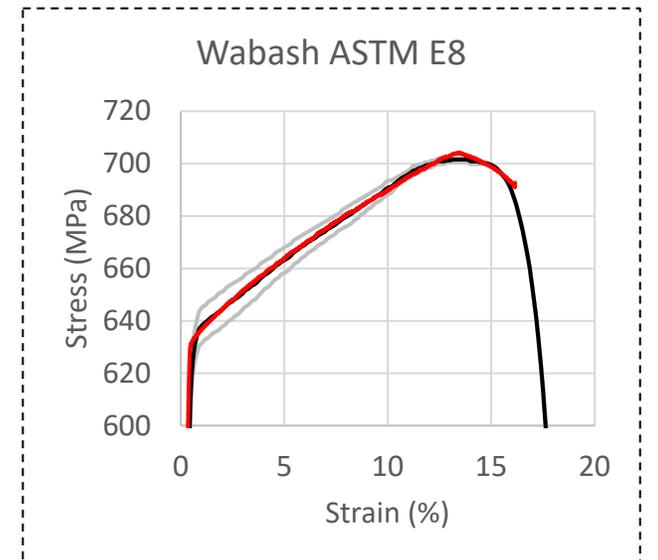
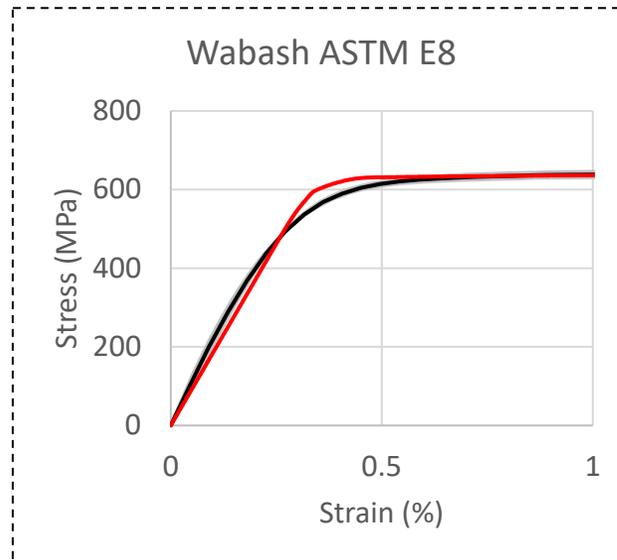
$$\sigma_y = \left(A + B\bar{\epsilon}^{p^n} \right)$$

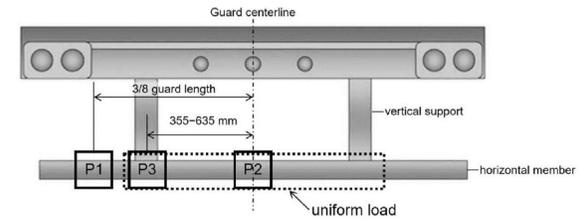
*MAT_098 (GPa) Wabash	
E	189.93
A	0.6274
B	0.7788
N	0.8780
SIGMAX	0.7057

Wabash ASTM E8



— Sample 1 — Sample 2 — Characteristic Curve — Simulation





Minimize y :

$$y = \frac{P_{UDL} - 350 \text{ kN}}{350 \text{ kN}} + \frac{P_{P2} - 50 \text{ kN}}{50 \text{ kN}} + \frac{P_{P1} - 50 \text{ kN}}{50 \text{ kN}} + \frac{U_{UDL} - 20 \text{ kJ}}{20 \text{ kJ}} + 0.25 \frac{M_{Sim}}{M_0}$$

Where:

- P_{UDL} , P_{P2} , and P_{P1} are the peak force from the UDL, P2, and P1 test locations
- U_{UDL} is the plastic energy absorbed during the UDL test
- M_{Sim} and M_0 are the current bumper mass and the baseline bumper mass, respectively

Constraints:

- $P_{UDL} \geq 350 \text{ kN}$
- $U_{UDL} \geq 20 \text{ kJ}$
- $P_{P2}, P_{P1} \geq 50 \text{ kN}$
- Ground Clearance $\leq 22 \text{ in}$